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ELES-1984

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EXPANDED LIQUID ENGINE SIMULATION COMPUTER PROGRAM

PROGRAMMERS MANUAL

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TABLE OF CONTENTS

	<u>Page</u>
1.0 Introduction	1
2.0 Liquid Stage Design Procedure	3
3.0 ELES Flowchart	5
4.0 Numerical Techniques	31
4.1 Warning Flags	35
5.0 Common Block Variables	36
6.0 Propellant Library	83

LIST OF FIGURES

<u>Figure No.</u>	<u>Page</u>
2.1 Liquid Stage Design Procedure	4
3.1 ELES Flowchart	6
3.2 ELES Subroutine List	16
5.1 Common Block Variables	37
6.1 Beginning of Propellant Library (PROPLIB)	85
6.2 Propellant Data Structure	86
6.3 Propellant Library (PROPLIB)	87

1.0 INTRODUCTION

The ELES-1984 computer code is a landmark development in the preliminary systems analysis of liquid rocket vehicles. It is capable of revealing subsystem interactions and design choice impacts on total vehicle performance. Its use enables very rapid determinations of optimum vehicle designs.

The liquid propulsion system models in ELES have been developed by Aerojet TechSystems Company under the auspices of AFRPL during the past few years (1980-1984). The main purpose of ELES is to find optimum vehicle designs for specified mission requirements. Toward that end it is capable of evaluating the size, weight, and performance of system components over a range of design configurations, materials of construction, and operating points. These capabilities allow the code to act as an excellent propulsion system preliminary design training tool.

The objective of this manual is to explain the internal structure of the ELES-1984 computer code. Main topics to be covered are the logic flowchart, internal variable definitions, data files, and numerical techniques used.

The non-liquid portions of ELES (solid stage design, trajectory simulation, method of multipliers optimization, etc.) are documented by other sources available through AFRPL.

There are four manuals which describe the operation of the ELES-1984 Computer Program.

Taylor, C. E.
Expanded Liquid Engine Simulation Computer Program
New Users Guide, Aerojet TechSystems Company, 1984

Taylor, C. E.
Expanded Liquid Engine Simulation Computer Program
Technical Information Manual, Aerojet TechSystems Company, 1984

Taylor, C. E.
Expanded Liquid Engine Simulation Computer Program
Programmers Manual, Aerojet TechSystems Company, 1984

Taylor, C. E.
Expanded Liquid Engine Simulation Computer Program
Advanced Users Manual, Aerojet TechSystems Company, 1984

Introduction (cont.)

Both users guides are concerned with proper formulation and input of a problem statement. The new users guide does so in a more basic manner than the advanced users guide. The technical information manual describes the mathematical algorithms used in ELES to model the various propulsion subsystems. The programmers manual deals with the internal structure of the FORTRAN code, its file structure, and internal communication.

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2.0 LIQUID STAGE DESIGN PROCEDURE

The general procedure used for calculating the size/weight/performance of liquid stages is described in Figure 2.1. It begins with the initialization of propellant feed circuit parameters (temperature, pressure, flowrate). The remainder of the procedure refines those initial estimates.

Refinements to the feed schedules include calculating the engine's barrier mixture ratio, engine performance, regenerative cooling jacket properties, turbo pump assembly (TPA) design, propellant tank pressurization requirements, and tankage heat transfer. Iterative procedures are used for some of the parameters.

When the propellant feed schedules are finalized, the final calculations of size, weight, and performance of the TPA, engine, and tankage can take place. A stage summary of those parameters and related parameters can then be made.

- 1) Initialize temperature schedule
- 2) Calculate engine barrier mixture ratio
- 3) Initialize flowrate schedule (using some rough estimates)
 - 3.1) Estimate tank sizes
 - 3.1.1 Estimate tank heat transfer
 - 3.1.2 Estimate pressurization requirements
 - 4) Calculate feed system pressure schedule
 - 4.1) Calculate engine performance
 - 4.2) Perform regen cooling analysis (if required)
 - 5) Perform non-conventional nozzle modifications
 - 6) Calculate flowrate schedule (using improved estimates)
 - 6.1) Calculate tank sizes
 - 6.1.1 Calculate tank heat transfer
 - 6.1.2 Calculate pressurization requirements.
 - 7) Design TPA (if required)
(iterate, if not power balanced)
 - 8) Update propellant temperature schedule
(iterate on temperature schedule, if required)
 - 9) Calculate TPA size/weight (if required)
 - 10) Calculate engine size/weight
 - 11) Calculate tankage size/weight
 - 12) Calculate stage summary size/weight/performance

Figure 2.1. Liquid Stage Design Procedure

3.0 ELES FLOW CHART

The overall flowchart of ELES is shown in Figure 3.1. The main program is named MODEC. The column to the right of MODEC shows each subroutine called by MODEC. The column below and to the right of each subroutine shows the subroutines which it calls.

In the interest of reducing the overall length of the flowchart, some entries have been abbreviated (FLUCON, FLUCP, FLUDEN, FLUPRO, FLUVIS, and RUNIT). The fluid property routines are abbreviated in all instances. The major subroutine RUNIT is abbreviated where it is called by the optimizer. The flowchart indicates abbreviated listings by parentheses following the subroutine name.

A brief description of each subroutine in ELES appears in Figure 3.2. The flowchart and subroutine description list should be used together.

```

Main
Program
MODEC
    FILOPN
    NEWNLP
        : READ3
        ! NLPIN
    FILCLS
    INITLG
        : MAKCAS
        : PROLIB
        : HXLIB
        : INPROP
            : FLUCON(conductivity)
            : LVPRES
            : FLUCP(heat capacity)
            : FLUDEN(density)
            : FLUVIS(viscosity)
    INTSAT
        ! LVPRES
    LVPRES
    INITER
        : MAKODE
        " DBINT
        : MAKCSR
        " DBINT
INTERM
    FILCLS
THRUST
    NOZZEX
CFVAC
PARSEL
RUNIT
    PARSEL
    SSTAGE
        : GRAPH
        " PARCOE
        CFVAC
    LSTAGE
        : INITMP
        " MAKODE
        " DBINT
        : BARMIX
        " ERISP
        " MAKODE
        " DBINT
        " ERCSR
        " MAKCSR
        " DBINT
        " MAKODE
        " DBINT
        " MAKCSR
        " DBINT
        TBVSMR
        " ERISP
        " MAKODE
        " DBINT
        " MAKODE
        " DBINT

```

Figure 3.1. ELES Flowchart (Sheet 1 of 10)

```

    " CMBGPR
    " GASH
    " RADENG
    " QUART
    " : CUBROT
    " MACH
INITWD
    " ERISP
    " MAKODE
    " : DBINT
    " MAKODE
    " DBINT
    " LVPRES
    " FLUDEN(density)
    " WSCHED
    " TNKEST
    " : THWALL
    " ! MPROP
    " TNDVOL
    " : FLUPRO(fluid properties)
    " ACQUID
    " " BLADR
    " " GOTOER
    " " BLADWT
    " TSAT
    " HVAPVT
    " FLUCP(heat capacity)
    " TANKHX
    " " MPROP
    " COMPHX
    " CNSTBT
    " : FLUPRO(fluid properties)
    " : FLUDEN(density)
    " : FLUCP(heat capacity)
    " FREECN
    " CALCON
    " COMPHX
    " ORBHX
    " PSYCHO
    " DBINT
PRESS
    " AUTOGN
    " TSAT
    " FLUDEN(density)
    " FLUPRO(fluid properties)
    " FLUCP(heat capacity)
    " FREECN
    " MPROP
    " EPSTN
    " SOLGG
    " CGPRES
    " TSAT
    " MPROP
    " HEDATA
    " DBINT
    " FREECN
    " EPSTN
NCTVOL
    " : FLUPRO(fluid properties)
    " ACQUID

```

Figure 3.1. ELES Flowchart (Sheet 2 of 10)

```

          "     BLADR
          "     GOTOER
          "     BLADWT
TSAT
HVAPVT
FLUCP(heat capacity)
SAT4HX
      "     MPROP
TANKHX
      "     MPROP
      "     COMPHX
      "     CNSTBT
      "     FLUPRO(fluid properties)
      "     FLUDEN(density)
      "     FLUCP(heat capacity)
      "     FREECN
      "     CALCON
      "     COMPHX
      "     ORBHX
      "     PSYCHO
      "     DBINT
PRESS
      "     AUTOGN
      "     TSAT
      "     FLUDEN(density)
      "     FLUPRO(fluid properties)
      "     FLUCP(heat capacity)
      "     FREECN
      "     MPROP
      "     EPSTN
      "     SOLGG
      "     CGPRES
      "     TSAT
      "     MPROP
      "     HEDATA
      "     DBINT
      "     FREECN
      "     EPSTN
PSCHED
      "     LPERF
ANNEPS
      "     MAKODE
      "         !     DBINT
      "     MAKCSR
      "         !     DBINT
      "     ERISP
      "         !     MAKODE
      "             "     DBINT
      "     ERCSR
      "         !     MAKCSR
      "             "     DBINT
      "         RADCON
      "     ERISP
      "         !     MAKODE
      "             "     DBINT
      "     MAKODE
      "         !     DBINT
      "     MAKCSR
      "         !     DBINT
      "     ERCSR

```

Figure 3.1. ELES Flowchart (Sheet 3 of 10)

```

    "      MAKCSR
    "      ! DBINT
VAPCON
    "      FLUPRO(fluid properties)
    "      SURTEN
    "      ! LVPRES
    "      DBINT
    "      GOTOER
    "      MAKODK
    "      ! DBINT
CMBGPR
REGEN
    "      MACH
    "      GASH
    "      FLUCP(heat capacity)
    "      FLUCON(conductivity)
    "      TRANSP
    "      FLUPRO(fluid properties)
    "      TSAT
    "      FFACTR
    "      HXHCV
    "      ! FLUPRO(fluid properties)
    "      ! FLUCP(heat capacity)
    "      LVPRES
PLUG
    "      TLTANG
    "      NOZZEX
    "      NOZZEX
ANULAR
    "      NOZZEX
WSCHED
    "      TNKEST
    "      THWALL
    "      ! MPROP
    "      TNDVOL
    "      ! FLUPRO(fluid properties)
    "      ACQUID
    "      ! BLADR
    "      " GOTOER
    "      BLADWT
    "      TSAT
    "      HVAPVT
    "      FLUCP(heat capacity)
    "      TANKHX
    "      ! MPROP
    "      COMPHX
    "      CNSTBT
    "      ! FLUPRO(fluid properties)
    "      ! FLUDEN(density)
    "      ! FLUCP(heat capacity)
    "      ! FREECN
    "      ! CALCON
    "      ! COMPHX
    "      ORBHX
    "      PSYCHO
    "      ! DBINT
PRESS
    "      ! AUTOGN
    "      ! TSAT
    "      ! FLUDEN(density)

```

Figure 3.1. ELES Flowchart (Sheet 4 of 10)

```

    "      " FLUPRO(fluid properties)
    "      " FLUCP(heat capacity)
    "      " FREECN
    "      " MPROP
    "      " EPSTN
    SOLGG
    CGPRES
    TSAT
    MPROP
    HEDATA
    "      DBINT
    FREECN
    EPSTN
NCTVOL
    FLUPRO(fluid properties)
    ACQUID
        BLADR
            "      GOTOER
        BLADWT
    TSAT
    HVAPVT
    FLUCP(heat capacity)
    SAT4HX
        MPROP
    TANKHX
        MPROP
        COMPHX
        CNSTBT
            "      FLUPRO(fluid properties)
            "      FLUDEN(density)
            "      FLUCP(heat capacity)
            "      FREECN
            "      CALCON
            "      COMPHX
        ORBHX
        PSYCHO
            "      DBINT
PRESS
    AUTOGN
        "      TSAT
        "      FLUDEN(density)
        "      FLUPRO(fluid properties)
        "      FLUCP(heat capacity)
        "      FREECN
        "      MPROP
        "      EPSTN
        SOLGG
        CGPRES
        TSAT
        MPROP
        HEDATA
            "      DBINT
        FREECN
        EPSTN
TSCHED
    "      FLUCP(heat capacity)
    "      FLUPRO(fluid properties)
    "      MAKODE
    "      DBINT
TPASYS

```

Figure 3.1. ELES Flowchart (Sheet 5 of 10)

```

" LVPRES
" FLUPRO(fluid properties)
" TPAGG
" PUMP
" : HEADCO
" : PMPEFF
" : BPHDCO
" : BPEFF
" TRBEFF
" SPOUT
" TURBIN
" BLADE
" PARTAD
" : TRBEFF
" ALLOW
" MAXRPM
" : TURBIN
" : BLADE
" : PARTAD
" : ! TRBEFF
" PUMP
" : HEADCO
" : PMPEFF
" : BPHDCO
" : BPEFF
TPAOTH
" PUMP
" : HEADCO
" : PMPEFF
" : BPHDCO
" : BPEFF
" HEADCO
" PMPEFF
" TRBEFF
" SPOUT
" TURBIN
" BLADE
" PARTAD
" : ! TRBEFF
" ALLOW
" MAXRPM
" : TURBIN
" : BLADE
" : PARTAD
" : ! TRBEFF
" PUMP
" : HEADCO
" : PMPEFF
" : BPHDCO
" : BPEFF
" MAKODE
" DBINT
WTPA
" FLUDEN(density)
" MAKODE
" DBINT
" MAKCSR
" DBINT
" FLUCP(heat capacity)
" TSAT

```

Figure 3.1. ELES Flowchart (Sheet 6 of 10)

```

    " HVAPVT
BURNTM
    " BTINT
    " LINI
    " MAKCSR
    " : DBINT
    " ERCSR
    " : MAKCSR
    " : ! DBINT
    " THROTT
    " LINI
MAKODE
    " DBINT
MAKCSR
    " DBINT
ERISP
    " MAKODE
    " : DBINT
ERCSR
    " MAKCSR
    " : DBINT
WTCA
    " FLUPRO(fluid properties)
    " WTRANZ
    " RADCON
    " FLUDEN(density)
TNKAGE
    " LQTANK
    " FLUPRO(fluid properties)
    " MPROP
    " THWALL
    " : MPROP
    " TNDVOL
    " : FLUPRO(fluid properties)
    " ACQUID
    " : BLADR
    " : ! GOTDER
    " : BLADWT
    " TSAT
    " HVAPVT
    " : FLUCP(heat capacity)
    " TANKHX
    " : MPROP
    " : COMPHX
    " : CNSTBT
    " : " FLUPRO(fluid properties)
    " : " FLUDEN(density)
    " : " FLUCP(heat capacity)
    " : " FREECN
    " : " CALCON
    " : " CDMPHX
    " : ORBHX
    " : PSYCHO
    " : " DBINT
    " PRESS
    " : AUTOGN
    " : " TSAT
    " : " FLUDEN(density)
    " : " FLUPRO(fluid properties)
    " : " FLUCP(heat capacity)

```

Figure 3.1. ELES Flowchart (Sheet 7 of 10)

```

    "      FREECN
    "      MPROP
    "      EPSTN
    SOLG
    CGPRES
    TSAT
    MPROP
    HEDATA
    "      DBINT
    FREECN
    EPSTN
GOTOER
BLADR
    GOTOER
BLADWT
LAYERV
MPROP
SHRTLD
NCTVOL
    FLUPRD(fluid properties)
    ACQUID
        ! BLADR
        " GOTOER
        BLADWT
    TSAT
    HVAPVT
    FLUCP(heat capacity)
    SAT4HX
        ! MPROP
    TANKHX
        MPROP
        COMPHX
        CNSTBT
            " FLUPRD(fluid properties)
            " FLUDEN(density)
            " FLUCP(heat capacity)
            " FREECN
            " CALCON
            " COMPHX
    ORBHX
    PSYCHO
        " DBINT
PRESS
    AUTOQN
        " TSAT
        " FLUDEN(density)
        " FLUPRD(fluid properties)
        " FLUCP(heat capacity)
        " FREECN
        " MPROP
        " EPSTN
    SOLGG
    CGPRES
    TSAT
    MPROP
    HEDATA
    " DBINT
    FREECN
    EPSTN
CSETNK

```

Figure 3.1. ELES Flowchart (Sheet 8 of 10)

```

    "          : MPROP
    "          : ACQUID
    "          :   ! BLADR
    "          :   " GOTOER
    "          :   ! BLADWT
TORUS      : TORUS
    "          : ACQUID
    "          :   ! BLADR
    "          :   " GOTOER
    "          :   ! BLADWT
    "          : MPROP
ELLELL     : ELLELL
    "          : QUART
    "          :   ! CUBROT
    "          : TORPNT
    "          : CONELL
    "          : NCTLIN
    "          :   ! FLUPRO(fluid properties)
    "          : MPROP
    "          : LINDIA
    "          :   ! FFACTR
FLYPAR
INTEG
    : ATMOSD
    : THRUST
    :   " NOZZEX
    : GUIDE
    :   " GOTOER
    :   " AEROF
    : AEROF
    : GOTOER
    : TRJPRN
    :   " GOTOER
    : KEPLER
SPRINT
LGWARN
TNDSUM
    : MPROP
PICTND
    : INITT
    :   " ERASE
    : DWINDO
    : TEKCHR
    : MOVEA
    : DRAWA
    : CAVHOR
    :   " MOVEA
    :   " DRAWA
    : DRAWR
    :   " DRAWA
    : HDCOPY
VEHSUM
    : CHRSIZ
    : ERASE
    : RESET
    : MPROP
    : LINFIX
    : FINITT
NCTPAR
PICVEH

```

Figure 3.1. ELES Flowchart (Sheet 9 of 10)

```

INITT
    " ERASE
DWINDO
TEKAXS
TEKCHR
MOVEA
DRAWR
    " DRAWA
DRAWA
CAVEDN
    " MOVEA
    " DRAWA
CAVEUP
    " MOVEA
    " DRAWA
HDCOPY
ERASE
RESET
PROSUM
    FLUPRO(fluid properties)
    LVPRES
ENGSUM
REGSUM
TPWSUM
    ! TSAT
TPASUM
WTSUM
VPRINT
NLPPEN
    RUNIT(repeat all design and trajectory)
FUNC
    ! SCALE
    " RUNIT(repeat all design and trajectory)
    " GOTOER
GOTOER
RINIT
GOTOER
SELOPT
GOTOER
VA1OA
    " FUNCT
    " FUNC
    " : SCALE
    " : RUNIT(repeat all design and trajectory)
    " : GOTOER
    " GOTOER
    " CARDS
    " GOTOER
GOTOER
PENSET
GOTOER
FUNC
    " SCALE
    " RUNIT(repeat all design and trajectory)
    " GOTOER
    " GOTOER
SIMEQ
CARDS
    GOTOER
SECOND

```

CTIM

Figure 3.1. ELES Flowchart (Sheet 10 of 10)

- 1) ACQUID - calculates the displacement volume and weight of propellant acquisition devices and propellant residual volumes in tanks.
- 2) AEROF - computes axial and normal aerodynamic forces acting on missile as a function of mach number, altitude and angle of attack.
- 3) ALLOW - calculates the design blade root centrifugal stress limit for turbine blades assuming 20% overspeed, 5% centrifugal bending stress, and 10% gas bending stress.
- 4) ANNEPS - calculates the area ratio of annular engines based on engine combustion performance, geometry, and thrust requirement.
- 5) ANULAR - calculates the performance of an annular engine. Detailed performance analysis in subroutine LPERF is required prior to this routine.
- 6) ATMOSD - computes ambient atmospheric pressure and speed of sound for a given altitude based on 1962 standard atmosphere.
- 7) AUTOGN - calculates propellant tank autogenous pressurization requirements. Assumes pressurant properties of pure oxidizer or pure fuel when pressurizing the oxidizer or fuel tank respectively.
- 8) BARMIX - calculates the combustion chamber barrier mixture ratio required for the cooling option under consideration.
- 9) BLADE - calculates the turbine blade height based on flowrate, velocity, and turbine exhaust gas density.
- 10) BLADR - calculates the positive expulsion bladder pressure differential, expulsion efficiency, and (for some configurations) thickness.

Figure 3.2. ELES Subroutine List (Sheet 1 of 15)

- 11) BLADWT - calculates the weight of positive expulsion bladders.
- 12) BPEFF - calculates the efficiency of boost pumps based on specific speed and impeller diameter.
- 13) BPHDCO - calculates boost pump head coefficient based on specific speed.
- 14) BTINT - called by subroutine BURNTM to set up time intervals in the array TBRN for interfacing liquid vehicles with the trajectory routines.
- 15) BURNTM - sets up the arrays FT, WDOT, and TBRN for interfacing liquid vehicles with the trajectory routines.
- 16) CALCON - calculates thermal conductivities of spray on foam insulation (SOFI) and multi layer insulation (MLI) under various operating conditions.
- 17) CARDS - saves intermediate values of optimization run.
- 18) CAVE - draws elliptical tank heads to the pseudo-Tektronix screen for vertical tank axes.
- 19) CAVHOR - draws elliptical tank heads to the pseudo-Tektronix screen for horizontal tank axes.
- 20) CETSQR - error trapping routine for negative square root calls.
- 21) CFVAC - computes theoretical vacuum thrust coefficient from nozzle expansion ratio and effective propellant ratio of specific heats.
- 22) CGPRES - calculates the helium pressurant requirements for a storable propellant tank.

Figure 3.2. ELES Subroutine List (Sheet 2 of 15)

- 23) CHRSIZ - a Tektronix graphics command. Has no function in the line-printer pseudo-Tektronix mode of ELES.
- 24) CMBGPR - returns combustion gas properties for combustion chamber cooling routines. (At present it provides only a fixed set of default values. This routine is targeted for future improvement).
- 25) CNSTBT - calculates temperatures at all tank wall interfaces and the heat flux for a constant temperature external boundary on the propellant tank.
- 26) COMPHX - calculates interface temperatures in a composite one dimensional heat transfer problem.
- 27) CONELL - used to calculate geometry of non-conventional tankage. Calculates the vertical difference in positions of an interfering conical frustum and ellipse. (Returns zero if frustum and ellipse do not touch.)
- 28) CSETNK - calculates the size and weight of a cylindrical-spherical-elliptical tank.
- 29) CUBROT - solves for the real roots of a cubic equation.
- 30) DBINT - double interpolates a two dimensional array of data.
- 31) DRAWA - simulates the Tektronix DRAWA command for making plots on line printer.
- 32) DRAWR - simulates the Tektronix DRAWR command for making plots on line printer.
- 33) DWINDO - simulates the Tektronix DWINDO command for making plots on line printer.

Figure 3.2. ELES Subroutine List (Sheet 3 of 15)

- 34) ELLELL - used to calculate geometry of non-conventional tankage. Calculates the difference in vertical positions of two interfering ellipses. (Returns zero if they do not touch.)
- 35) ENGSUM - prints a page of engine size/weight/performance summary data.
- 36) EPSTN - calculates the pressurant requirements for a cryogenic propellant tank using the Epstein equation.
- 37) ERASE - simulates the Tektronix ERASE command for making plots on line printer.
- 38) ERCSR - approximates the C* of a user defined propellant using the equivalence ratio method.
- 39) ERISP - approximates the Isp of a user defined propellant using the equivalence ratio method.
- 40) EXTRAZ - calculates the compressibility factor of supercritical fluids.
- 41) FFACTR - calculates the Weisbach-Darcy friction factor as a function of Reynolds number, absolute surface roughness, and hydraulic diameter.
- 42) FILCLS - closes all open files prior to a normal termination of program execution.
- 43) FILOPN - opens many of the files used during program execution.
- 44) FINITT - simulates the Tektronix FINITT command. (Performs no function in the line-printer mode.)
- 45) FLUCON - calculates the thermal conductivity of a fluid at any given temperature and pressure.

Figure 3.2. ELES Subroutine List (Sheet 4 of 15)

- 46) FLUCP - calculates the heat capacity of a fluid at a given temperature and pressure based on the Webb-Rubin equation of state.
- 47) FLUDEN - calculates the density of a fluid at a given temperature and pressure.
- 48) FLUPRO - calculates fluid density, viscosity, and thermal conductivity at a given temperature and pressure. (Calls routines FLUDEN, FLUVIS, and FLUCON.)
- 49) FLUVIS - calculates fluid viscosity at a given temperature and pressure.
- 50) FLYPAR - adjusts the thrust, burn time, and flowrate arrays in order to allow for parallel burns of integrated stages.
- 51) FREECN - calculates the fluid heat transfer coefficient due to free convection.
- 52) FUNC - evaluates the method of multipliers augmented Lagrangian function.
- 53) FUNCT - manipulates the internal arrays related to optimization.
- 54) GASDCP - calculates the difference in heat capacity between a real gas and an ideal gas.
- 55) GASH - calculates combustion chamber gas side heat transfer coefficient using Bartz correlation.
- 56) GASZ - calculates the compressibility factor of subcritical gases. (Called by FLUDEN.)
- 57) GENTRP - general interpolator for bivariate data.
- 58) GOTOER - an error trapping routine related to computed GO TO statements.
- 59) GRAPH - used by subroutine SSTAGE to design solid stage.

Figure 3.2. ELES Subroutine List (Sheet 5 of 15)

- 60) GUIDE - checks input flight profiles and exercises the corresponding guidance laws for trajectory calculations.
- 61) H2DATA - calculates density, thermal conductivity, viscosity, and heat capacity for para-hydrogen.
- 62) HDCOPY - simulates the Tektronix HDCOPY command for making plots on the line-printer.
- 63) HEADCO - calculates main pump head coefficient based on specific speed.
- 64) HEDATA - calculates density, thermal conductivity, viscosity, and heat capacity for helium.
- 65) HVAPVT - calculates liquid heat of vaporization vs. temperature.
- 66) HXHCV - for regenerative cooling model this routine calculates the coolant heat transfer coefficient if given velocity or velocity if given coolant heat transfer coefficient.
- 67) HXLIB - library of liquid propellant heat transfer data.
- 68) INITER - initialization routine for the equivalence ratio method of calculating performance of user defined propellants.
- 69) INITLQ - initialization routine for liquid stages. Provides fluid property constants and restructures input data structure.
- 70) INITMP - initializes the propellant temperature schedule throughout the feed system. Temperature estimates are improved as analysis continues.
- 71) INITT - simulates the Tektronix INITT command for making plots on the line-printer. (Performs form feed and erases the printing screen.)

Figure 3.2. ELES Subroutine List (Sheet 6 of 15)

- 72) INITWD - initializes the propellant flow rate schedule throughout the feed system. Flowrate estimates are improved as analysis continues.
- 73) INPROP - initializes propellant critical properties based on reference data and the method of corresponding states.
- 74) INTEG - integrates missile trajectory using either a 4th order Runge-Kutta or a 4th order Adams-Moulton predictor corrector procedure.
- 75) INTERM - checks for fatal input errors and terminates execution if discovered.
- 76) INTSAT - initializes the data arrays used in subroutine TSAT which calculates fluid saturation temperature.
- 77) KEPLER - examines orbital injection conditions, burnout radius, burnout flight path angle, and burnout velocity in order to calculate the orbital parameters described by that energy state.
- 78) LAYERV - calculates volumes of concentric cylindrical volumes with elliptical ends (i.e., insulation layers on a propellant tank).
- 79) LINDIA - calculates diameter of fluid feed lines with various bends, valves, etc.
- 80) LINFIX - used to format lines in the non-conventional tank summary output page.
- 81) LINI - linear interpolation routine.
- 82) LIQDCP - calculates the difference in heat capacity of a real liquid and an ideal gas.
- 83) LIQZ - Calculates the compressibility factor of a liquid at a given temperature and pressure.

Figure 3.2. ELES Subroutine List (Sheet 7 of 15)

- 84) LPERF - calculates the delivered performance of a liquid rocket engine.
- 85) LQTANK - calculates the size and weight of tandem tankage.
- 86) LQWARN - prints a listing of warning messages for the liquid stage under consideration. Messages relate to inputs outside of normal design range, components critical design constraints, and designs with potential problems.
- 87) LSTAGE - supervisory routine for calculating the size, weight, and performance of liquid stages.
- 88) LVPRES - calculates liquid vapor pressure based on the Riedel-Plank-Miller vapor pressure correlation.
- 89) MACH - calculates mach number in a combustion chamber in both the subsonic and supersonic regimes.
- 90) MAKCAS - loads internal data arrays for propellant combination performance. Reads values for specific impulse, characteristic velocity, and combustion temperature from the file "PROPLIB".
- 91) MAKCSR - interpolates characteristic velocity at a given chamber pressure and mixture ratio from the data arrays read by MAKCAS.
- 92) MAKODE - interpolates equilibrium specific impulse at a given chamber pressure, mixture ratio, and area ratio from the data arrays read by MAKCAS.
- 93) MAKODK - interpolates kinetic specific impulse at a given chamber pressure, mixture ratio, area ratio, and throat radius from the data arrays read by MAKCAS.
- 94) MAXRPM - checks the turbine blade root stress and if necessary causes the turbopump assembly.

Figure 3.2. ELES Subroutine List (Sheet 8 of 15)

- 95) MODEC - the overall executive program. Initializes variables, sets namelist definitions, etc.
- 96) MOVEA - simulates the Tektronix MOVEA command for making plots on line printer.
- 97) MPROP - the material properties library. Provides yield strength, modulus of elasticity, density, minimum gauge, heat capacity, and thermal conductivity.
- 98) NCTLIN - calculates propellant feed line weights for non-conventional tankage designs.
- 99) NCTPAR - prints a summary page of non-conventional tankage parameters.
- 100) NCTVOL - calculates tank volumes and pressures for non-conventional tankage designs.
- 101) NEWNLP - supervisory routine for the optimizer.
- 102) NLPIN - performs namelist input and input error checking for the optimizer routines.
- 103) NLPPEN - driver routine for the optimizer. Directs control of individual elements of the algorithm.
- 104) NOZZEX - calculates the pressure ratio, exit mach number, and Prandtl-Meyer angle of a nozzle.
- 105) ORBHX - calculates the external boundary temperature of an orbiting tank exposed to radiant heat flux.
- 106) PARCOE - gives coefficients for a parabolic curve fit.

Figure 3.2. ELES Subroutine List (Sheet 9 of 15)

- 107) PARSEL - selects appropriate parameters to be placed into the optimization list.
- 108) PARTAD - changes turbine design to partial admission if turbine blades become too small.
- 109) PENSET - updates the Lagrange multipliers and penalty constants between unconstrained function minimizations.
- 110) PICTND - creates a scaled schematic drawing of a tandem tank design on the line printer.
- 111) PICVEH - creates a scaled schematic drawing at a non-conventional tank design on the line printer.
- 112) PLUG - calculates the size and performance of a plug cluster engine.
- 113) PMPEFF - calculates the efficiency of a main pump using specific speed and impeller diameter.
- 114) PRESS - administrates the calculation of propellant tank pressurization requirements for storable or cryogenic propellants.
- 115) PROLIB - holds propellant properties data for library propellants.
- 116) PROSUM - prints a page of propellant property data over the operating temperature range of each propellant.
- 117) PSCHED - calculates the majority of the propellant feed pressure schedule.
- 118) PSYCHO - from a psychrometric chart this routine looks up the molar concentration of water in air as a function of relative humidity and ambient temperature.

Figure 3.2. ELES Subroutine List (Sheet 10 of 15)

- 119) PUMP - designs pumps for diameter, efficiency, number of stages, specific speed, and horse power requirements.
- 120) PVTFNC - checks the Benedict-Webb-Rubin equation of state to see if it is satisfied with input values of reduced temperature, reduced pressure, and reduced volume.
- 121) QUART - solves for the real roots of a quartic equation.
- 122) RADENG - calculates the gas side temperature required to maintain a radiation cooled TCA at the maximum allowable material temperature.
- 123) RAOCON - approximates the contour of a Rao nozzle with hyperbolic curve fits of Rao data.
- 124) READ3 - sets up position pointers prior to reading optimizer input namelist.
- 125) REGEN - calculates the pressure drop and temperature rise across a regenerative cooling jacket.
- 126) REGSUM - prints a one page summary of the regenerative cooling jacket analysis.
- 127) RESET - simulates the Tektronix RESET command for making plots on line printer. (Issues form feed for line printer.)
- 128) RINIT - initializes penalty constants for both equality and inequality constraints prior to start of Methods of Multipliers optimization algorithm.
- 129) RUNIT - administrates calls to solid and liquid stage design and trajectory model.
- 130) SAT4HX - calculates the surface area and average wall thickness of propellant tanks for use in heat transfer calculations.

Figure 3.2. ELES Subroutine List (Sheet 11 of 15)

- 131) SCALE - performs all the scaling and unscaling of control variables, objective function, and constraints for the optimizer.
- 132) SECOND - system specific routine used to determine run-time violations.
- 133) SELOPT - driver to select the method of unconstrained function minimization for the optimizer.
- 134) SHRTLD - computes the size, position, and weight of non-conventional tankage designs.
- 135) SIMEQ - solves a set of simultaneous linear equations.
- 136) SOLGG - calculates the solid gas generator pressurization requirements of a storable propellant tank including condensibles.
- 137) SPOUT - calculates the isentropic spouting velocity of a turbine configuration.
- 138) SPRINT - prints a summary of solid stage designs.
- 139) SSTAGE - calculates the size, weight, and performance of a solid stage.
- 140) SUPDCP - calculates the difference in heat capacity of a real fluid and an ideal fluid at supercritical pressures.
- 141) SUPERZ - calculates the compressibility factor of supercritical fluids.
- 142) SURTEN - calculates surface tension based on the Hakim equation.
- 143) TANKHX - calculates propellant tank heat flux for several different heat flux scenarios.

Figure 3.2. ELES Subroutine List (Sheet 12 of 15)

- 144) TBVSMR - calculates a propellant mixture ratio which corresponds to a desired combustion temperature.
- 145) TEKAXS - labels the plotting axes for the line-printer output plots.
- 146) TEKCHR - selects the character to be plotted on the line printer output.
- 147) THROTT - calculates the throttled chamber pressure and throttling efficiencies for liquid rocket engines.
- 148) THRUST - computes and integrates delivered thrust and propellant flow rate as a function of burn time.
- 149) THWALL - calculates the thickness of propellant tank walls for tandem tank designs.
- 150) TLTANG - calculates the required tilt angle for plug cluster modules.
- 151) TNDSUM - prints a one page summary of the tankage in a tandem design.
- 152) TNDVOL - calculates the volumes and pressures for tandem tank routines.
- 153) TNKAGE - administers routines for the tankage design routines.
- 154) TNKEST - administers routines which estimate the tank volumes for preliminary calculations.
- 155) TORPNT - used in non-conventional tankage geometry calculations to find the point on a torus to use as an effective ellipse in subroutine ELLELL.
- 156) TORUS - calculates the geometry of a toroidal tank and its associated weight.

Figure 3.2. ELES Subroutine List (Sheet 13 of 15)

- 157) TPAGG - designs the turbopump assembly (TPA) for gas generator bleed power cycles.
- 158) TPAOTH - designs the turbopump assembly (TPA) for staged combustion, staged reaction, and expander power cycles.
- 159) TPASUM - prints a one page summary of the turbopump assembly design.
- 160) TPASYS - administrates the turbopump assembly system design for all power cycles.
- 161) TPWSUM - prints a one page summary of the propellant feed system temperature, pressure, and flowrate schedules.
- 162) TRANSP - calculates the required mass flux of coolant required by a transpiration cooled chamber section.
- 163) TRBEFF - calculates the efficiency of a single stage turbine over a range of admission fractions.
- 164) TRJPRN - prints trajectory information at designated time steps.
- 165) TSAT - calculates fluid saturation temperature at a given pressure.
- 166) TSCHED - calculates the propellant feed system temperature schedule.
- 167) TURBIN - sizes the turbine and stages if required.
- 168) VA1#A - performs unconstrained function minimization by a quasi-Newton variable-metric technique.

Figure 3.2. ELES Subroutine List (Sheet 14 of 15)

- 169) VAPCON - calculates propellant vaporization constants which are used in the performance routine (LPERF) to determine the vaporization efficiency of the engine.
- 170) VEHSUM - prints a summary of non-conventional tankage.
- 171) VPRINT - prints a one page summary of the vehicle (one to four stages).
- 172) WSCHED - calculates the flowrate schedule for the propellant feed system.
- 173) WTPA - calculates the weight of the turbopump assembly (TPA) and related hardware.
- 174) WTRANZ - calculates the weight of spring actuated translating nozzles and gas deployed skirts.
- 175) WTSUM - prints a one page summary of the weight items of a stage.
- 176) WTTCA - calculates the weight of a liquid thrust chamber assembly (TCA)

Figure 3.2. ELES Subroutine List (Sheet 15 of 15)

4.0 NUMERICAL TECHNIQUES

There are a number of different numerical techniques used within ELES-1984. The choice of technique is based on accuracy requirements, implementation effort, code complexity, applicability, and impact on other components of ELES. Small weight items, for example, can tolerate high degrees of error in their weight calculations without appreciably affecting stage or vehicle weight. A simple curve fit would suffice in those instances. When high accuracy is required, an iteration scheme can sometimes work well. If it terminates based on an accuracy criteria, however, it can adversely affect derivative calculations made in the optimizer.

One of the most preferred techniques for use in ELES-1984 is physical modeling. When a component's dimensions, thicknesses, etc. can be calculated, the weights calculated from those dimensions tend to be more accurate and to scale more accurately. Examples of physical modeling in ELES include the thrust chamber, positive expulsion bladder, translating nozzles, and tank weights.

Another method for insuring the accuracy of a model over a wide range of applicability is the use of mechanistic models. These models represent major mechanisms of a process. The engine performance model, for example, starts with ideal performance and mechanistically approaches each loss component by calculating injector characteristics, propellant drop sizes, vaporization rates, element type, stream tube geometry, etc. Other models which utilize a mechanistic approach are the ablative thickness model, regenerative cooling, and transpiration cooling models.

Analytical solutions are another preferred approach. A typical problem with analytical solutions is that a number of simplifying assumptions are required. These assumptions can reduce the accuracy and applicability of the model. When these assumptions are reasonable, ELES employs analytical solutions. Examples include radiation cooling model, heat transfer through tank insulation, physical interference of non-conventional tankage, and solutions of cubic and quartic equations.

When physical modeling is too complex, a physically based scaling approach can be taken. Using only the major dimensions of a component, scaling equations can still reflect a great deal of reality and do not tend to "blow up" outside a narrow range of

4.0, Numerical Techniques (cont.)

applicability. Some component weights are calculated by this approach such as the pumps, turbines, valves, and injectors.

Another reliable method for obtaining good accuracy over a wide range of application is table look-up. For example, the ideal performance of the library propellant combinations, fluid properties of both hydrogen and helium, and the efficiencies of both pumps and turbines are looked up in tables. Potential draw-backs to this approach are that the generation of tabular data can be time consuming, erroneous table entries can be easily overlooked, tables take up a lot of computer memory, and table look-ups can take a lot of computer time (especially bivariate or trivariate data).

Curve fits are an extremely common method of representing the variation of a parameter. Depending on the form of the curve fit and the behavior of the data as the independent variables go to extreme values, curve fits can be very accurate and very well behaved. Because the reverse can also be true, extreme care must be taken with the use of curve fits. ELES uses curve fit methods to calculate gimbal system weight, thrust mount weight, expulsion efficiency, heat transfer through tank lines, cryogenic pressurization requirements, nozzle contours, non-optimum tank weight factors, heat transfer coefficients, bladder pressure differentials, fluid properties, and many other parameters.

A less common numerical technique used in ELES is scaling by analogy. Scaling by analogy involves using a model, which is normally used to calculate a parameter, as a way of scaling a known data point. The method of corresponding states, for example, is a method for predicting fluid properties based on critical temperatures and pressures, normal boiling points, molecular weights, etc. ELES uses this method to scale known reference values of those properties. (The accuracy of the predictive method is increased by its use as a scaling procedure.)

Another less common technique is inverse interpolation from curve fits. ELES uses this approach to calculate fluid saturation temperatures as a function of pressure. The method consists of an initialization phase and a subsequent usage phase. During initialization, ELES generates a data table of temperature vs. vapor pressure using the Riedel-Plank-Miller equation for vapor pressure.

4.0, Numerical Techniques (cont.)

$$\ln(P_{vr}) = \frac{G}{T_r} [1 - T_r^2 + K (3 + T_r) (1 - T_r)^3]$$

During the usage phase ELES interpolates the data table to obtain saturation temperature as a function of pressure. The interpolation is made using the form of a Clapeyron vapor pressure equation in order to enhance interpolation accuracy.

$$\ln(P_v) = A - B/T$$

In general, inverse interpolation from curve fits is used to provide more execution speed than an iterative solution can provide. The more calls there are to the routine the faster it is compared to iteration. This approach will also provide a better derivative than iterative methods especially if care is taken in the interpolation.

As implied above, iteration is a common method of obtaining the solution of a variable with a non-linear relationship to other known variables. There are a number of different methods of iteration, each of which has its advantages and disadvantages in the areas of convergence speed, convergence assurance, convergence detection, and ease of implementation.

For finding the mixture ratio of a propellant combination which corresponds to a desired combustion temperature, ELES uses the "brute force" halving the interval method. Although this method converges slowly, convergence is guaranteed and an iteration limit assures a known accuracy. Newton-Raphson and secant type methods were avoided in order to assure good program behavior even when the optimizer drives the program into regimes where non-convergence is more likely.

Some of the other iterations in ELES use a Gauss-Siedel or modified Gauss-Siedel technique. The overall area ratio of an annular engine is one of the simpler examples of this. The overall area ratio is a function of the Isp, and the Isp is a function of the overall area ratio. By starting with an initial guess of area ratio and calculating Isp, one can use this Isp value to calculate a better value of area ratio, from which a better value of Isp

4.0, Numerical Techniques (cont.)

can be obtained, and so on. A typical termination criteria is an accuracy criteria. However, ELES uses a constant number of iterations in an attempt to provide a more reliable derivative.

Some of the more complicated Gauss-Siedel iterations include the overall propellant feed system temperature schedule and the TPA power balance routine. Due to the numerous computations involved in even a single iteration for both of those solutions, the termination criteria is for +3% accuracy.

A final numerical technique, which is actually more of a programmer's technique, is the implementation of dummy routines to provide required data. The routine in ELES which provides combustion gas fluid properties, for example, merely returns a constant value for each of its outputs. Its function is to hold a place in the code and allow for future improvements in a modular manner. A second example is the material properties library, which currently has several materials in it but could easily be enlarged to incorporate many other materials.

4.1 WARNING FLAGS

There are many possible inputs to ELES which would create unreasonable designs or designs contrary to good engineering judgement. Because the optimizer may pass through such a design while searching for an optimum, ELES can not halt operation when this happens but must output information which the user and the optimizer can both use. The mechanism which informs the user is warning flags. The mechanism which informs the optimizer is constraint parameters.

The subroutine LQWARN (see flowchart in Figure 3.1) checks all warning flags at output time and issues appropriate messages to the user. Warning flags are set in the various design routines of ELES at the point where the potential error is detected. The format for setting the warning flag (IWARN) is:

IWARN (NS, I) = 0

If (condition) IWARN (NS, I) = 1

where: NS = stage number

I = identification number of warning

condition = condition under which warning should occur

The warning flag is first set to zero (no error) and then checked for the error condition so that only the last pass through that portion of code can set the warning flag. If the optimizer strays into a "bad" area, warnings will only occur if it does not return to a more accepted design before program termination.

A list of the current warning flags in ELES-1984 is listed in "Expanded Liquid Engine Simulation Computer Program Technical Information Manual", Aerojet TechSystems Company, 1984, section 13.0.

5.0 COMMON BLOCK VARIABLES

All of the variables which appear in common blocks are presented in Figure 5.1. The variables are given in alphabetical order and include a definition, the engineering units of the variable, its default value, the namelist in which it appears (if any), and the name of the labeled common block in which it appears. See the key at the top of the figure to interpret the format of the information.

CIIIIIIIIIIIIIIII ELES COMMON BLOCK VARIABLES IIIIIIIIIIIIIIIII
 CI
 CI (UNITS DEFAULT \$NAMELIST /COMMON/)
 CI
 CI AAA ENECA WEIGHT
 CI (LBM --- \$---- /SSCOM/)
 CI
 CI AATT NO AVAILABLE DEFINITION (/SSCOM/)
 CI ABAPGG MAXIMUM BURN AREA TO THROAT AREA RATIO
 CI (--- --- \$---- /GASGEN/)
 CI
 CI ABATGG BURN TO THROAT AREA RATIO IN SOLID GG
 CI (--- --- \$---- /GASGEN/)
 CI
 CI ACAMAX MAXIMUM ALLOWABLE AXIAL ACCELERATION DURING FLIGHT
 CI (G'S 50 \$INTRAJ /MOTOR/)
 CI
 CI ACLAPF CORRELATION COEFFICIENT USED IN CALCULATING FUEL
 CI SATURATION TEMPERATURE
 CI (--- --- \$---- /CLAP/)
 CI
 CI ACLAPO CORRELATION COEFFICIENT USED IN CALCULATING OX
 CI SATURATION TEMPERATURE
 CI (--- --- \$---- /CLAP/)
 CI
 CI ADHPFL NO AVAILABLE DEFINITION (/TPOUT2/)
 CI
 CI ADHPOX NO AVAILABLE DEFINITION (/TPOUT2/)
 CI
 CI AE FIBER AREA
 CI (IN**2/END 0. 000135 \$FILMNT /MOTOR/)
 CI
 CI AEPLUG EXIT AREA OF PLUG CLUSTER
 CI (IN**2 --- \$---- /PLUGCL/)
 CI
 CI AESSR CROSS SECTIONAL AREA OF ENGINE SHROUD STIFFENING
 CI RING
 CI (IN**2 0. 152 \$LTANK /TANKS/)
 CI
 CI AEXIT EXIT AREA OF NOZZLE
 CI (IN**2 1. 0 \$THVST /PERF/)
 CI
 CI AFL FUEL FLOW AREA IN INJECTOR FACE
 CI (IN**2 --- \$---- /LIQUID/)
 CI
 CI AFSSR CROSS SECTIONAL AREA OF FORWARD SHROUD STIFFENING
 CI RING
 CI (IN**2 0. 25 \$LTANK /TANKS/)
 CI
 CI ALFDIV EFFECTIVE HALF ANGLE
 CI (DEG --- \$---- /SSCOM/)
 CI
 CI ALFMIX BARRIER MIXING ANGLE IN CHAMBER
 CI (DEG 0. 286 \$INJECT /LIQUID/)
 CI
 CI ALFNOZ NOZZLE DIVERGENCE ANGLE OF CONICAL NOZZLES OR EXIT
 CI ANGLE OF CONTOURED NOZZLES
 CI (DEG 15. \$NOZZLE ///EQ///)
 CI
 CI ALFPRT EXIT HALF ANGLE
 CI (DEG --- \$---- /SSCOM/)
 CI
 CI ALFSTG NO AVAILABLE DEFINITION (/AERO/)
 CI
 CI ALFTB TURN BACK ANGLE
 CI (DEG --- \$---- /SSCOM/)
 CI
 CI ALFTRN INITIAL FLOW TURNING ANGLE FOR CONTOURED NOZZLES
 CI (FOR BELL(1) = 1 ONLY)
 CI (DEG 27 \$MATER /MOTOR/)
 CI
 CI ALPH ANGLE OF ATTACKS FOR WHICH AERODYNAMIC
 CI COEFFICIENTS ARE INPUT
 CI (DEG 0. \$AEROD /AERO/)
 CI
 CI ALPHA INITIAL ANGLE OF ATTACK
 CI (DEG 0. \$INTRAJ ///EQ///)
 CI
 CI ALPHAC COMMANDED CONSTANT ANGLE OF ATTACK; INPUT FOR
 CI TRAJECTORY GUIDANCE SECTIONS UTILIZING GUIDANCE
 CI OPTION 1
 CI (DEG 0 \$GUIDA ///EQ///)

Figure 5.1. Common Block Variables (Sheet 1 of 46)

CI	ALPMAX	NO AVAILABLE DEFINITION (/TRAJ/)
CI	ALPMLD	ANGLE OF ATTACKS PRODUCING MAXIMUM LIFT-TO-DRAG INPUT AS A FUNCTION OF MACH NUMBER FOR TRAJECTORIES UTILIZING GUIDANCE OPTION 9 (DEG 0. \$GUIDA /AERO/)
CI	ALPTOL	CONVERGENCE TOLERANCE FOR LC-RHA ITERATION FOR ANGLE OF ATTACK, ALPHA (--- .000001 \$AEROD /TRAJ/)
CI	ALT	NO AVAILABLE DEFINITION (/TRAJ/)
CI	ALTBOM	NO AVAILABLE DEFINITION (/TRAJ/)
CI	ALTI	INITIAL MISSILE ALTITUDE (FT 0.0 \$INTRAJ ///EQ///)
CI	ALTRE	ALTITUDE TO BEGIN RE-ENTRY CALCULATIONS (FT 3. E5 \$INTRAJ /TRAJ/)
CI	ALTSF	ALTITUDES FOR WHICH SKIN FRICTION COEFFICIENTS ARE INPUT (FT 0. \$AEROD /AERO/)
CI	ALTSTG	NO AVAILABLE DEFINITION (/TRAJ/)
CI	ALTTGT	ALTITUDE OF TARGET (FT 0.0 \$INTRAJ /TRAJ/)
CI	AMACH	MACH NUMBERS FOR WHICH AERODYNAMIC COEFFICIENTS ARE INPUT (--- 0. \$AEROD /AERO/)
CI	ANOZZ	NOZZLE LENGTH RATIO (--- --- \$--- /SSCOM/)
CI	AOB	NO AVAILABLE DEFINITION (/SSCOM/)
CI	AOX	OXIDIZER FLOW AREA IN INJECTOR FACE (IN**2 --- \$--- /LIQUID/)
CI	APARK	SEMIMAJOR AXIS OF PARKING ORBIT (FT 0.0 \$ORB ///EG///)
CI	APATAV	NO AVAILABLE DEFINITION (//EQ///)
CI	APATGG	MINIMUM PORT TO THROAT AREA RATIO (--- 3.0 \$OLDGG /GASGEN/)
CI	APOGEE	NO AVAILABLE DEFINITION (//EQ///)
CI	AREA	NO AVAILABLE DEFINITION (/AERO/)
CI	AREF	MISSILE AERODYNAMIC REFERENCE AREA INPUT FOR EACH STAGE (FT**2 0.0 \$THVST /AERO/)
CI	ARFPAY	NO AVAILABLE DEFINITION (/AERO/)
CI	ARGN	CORRELATION COEFFICIENT USED IN CALCULATING REGEN COOLANT SATURATION TEMPERATURE (--- --- \$--- /CLAP/)
CI	ASTGMX	NO AVAILABLE DEFINITION (/AERO/)
CI	AT	NOMINAL THROAT AREA FOR EACH STAGE (IN**2 100. \$INPGEN ///EQ///)
CI	ATILT	NO AVAILABLE DEFINITION (/PLUGCL/)
CI	AUTWTF	TOTAL FUEL AUTOGENOUS PRESSURANT WEIGHT (LB --- \$--- /TANKS2/)
CI	AUTWTO	TOTAL OXIDIZER AUTOGENOUS PRESSURANT WEIGHT (LB --- \$--- /TANKS2/)
CI	B	NO AVAILABLE DEFINITION (/SSCOM/)
CI	BALPAR	NO AVAILABLE DEFINITION (/TPDOUT2/)
CI	BCLAPP	CORRELATION COEFFICIENT USED IN CALCULATING FUEL SATURATION TEMPERATURE (--- --- \$--- /CLAP/)
CI	BCLAPO	CORRELATION COEFFICIENT USED IN CALCULATING OX SATURATION TEMPERATURE (--- --- \$--- /CLAP/)
CI	BETA	TOLERANCE TO TEST FOR PENALTY CONSTANT INCREASE (--- 0.25 \$NLP /WARN/)

Figure 5.1. Common Block Variables (Sheet 2 of 46)

CI	BHPBPF	NO AVAILABLE DEFINITION (/TPAOUT/)
CI	BHPBPO	NO AVAILABLE DEFINITION (/TPAOUT/)
CI	BHPFL	FUEL PUMP BRAKE HORSE POWER (HP --- \$---- /TPAOUT/)
CI	BHPOX	OXIDIZER PUMP BRAKE HORSE POWER (HP --- \$---- /TPAOUT/)
CI	BLSPCA	SPACE BETWEEN TRANSVERSE BLADDER AND AFT TANK WALL (KBLAT = 1) (IN 0.01 \$---- /TANKS/)
CI	BLSPCF	SPACE BETWEEN TRANSVERSE BLADDER AND FORWARD TANK WALL (KBLFT = 1) (IN 0.01 \$---- /TANKS/)
CI	BLSPFL	FUEL TANK TRANSVERSE COLLAPSING BLADDER SPACE (IN .01 \$BLADER /TANKS2/)
CI	BLSPOX	OXIDIZER TANK TRANSVERSE COLLAPSING BLADDER SPACE (IN .01 \$BLADER /TANKS2/)
CI	BPFRFL	FUEL BOOST PUMP FRACTION OF TOTAL HEAD RISE (--- 0.0464 \$PUMP /PRESCH/)
CI	BPFROX	OXIDIZER BOOST PUMP FRACTION OF TOTAL HEAD RISE (--- 0.0464 \$PUMP /PRESCH/)
CI	BRGN	CORRELATION COEFFICIENT USED IN CALCULATING REGEN COOLANT SATURATION TEMPERATURE (--- --- \$---- /CLAP/)
CI	BRGGG	RATIO OF MAXIMUM TO MINIMUM BURN RATE IN SOLID GG (--- --- \$---- /GASGEN/)
CI	BTEQGG	RATIO OF EQUILIBRIUM TEMPERATURE IN PROPELLANT TANK TO MINIMUM OPERATING TEMPERATURE (TMIN) (--- 1.5 \$BOLDGG /GASGEN/)
CI	BULK	COMPOSITE MOTOR CASE MATERIAL BULK FACTOR FOR EACH STAGE (--- 1. \$MATER /MOTOR/)
CI	BURNRA	GRAIN BURN RATE FOR START CARTRIDGE (ISTART=3) (IN/SEC 0.14 \$PUMP /TPAIN/)
CI	BYPREG	REGEN JACKET BYPASS FLOW FRACTION (--- 0.0 \$INREGN /SCHEDW/)
CI	BYPTUR	TURBINE BYPASS FLOW FRACTION (--- 0.0 \$INREGN /SCHEDW/)
CI	C	NO AVAILABLE DEFINITION (/ATMOS/)
CI	CA	AERODYNAMIC AXIAL FORCE COEFFICIENTS INPUT AS FUNCTIONS OF MACH NUMBER AND ANGLE OF ATTACK CA(I,J) CORRESPONDS TO AMACH(I) (--- --- \$AEROD /AERO/)
CI	CAB	BASE DRAG CORRECTION FACTOR; DECREASE IN CA FOR POWER-ON (--- 0. \$AEROD /AERO/)
CI	CALPH	NO AVAILABLE DEFINITION (/TRAJ/)
CI	CBM	CRITICAL BENDING MOMENT (IN/LBF 0.0 \$LTANK /TANKS/)
CI	CBMLT	BASE PRESSURE THRUST MULTIPLIER ON PLUG CLUSTER AND ANNULAR ENGINES (--- 0.7 \$NOZZLE /PLUGCL/)
CI	CBRGG	BURN RATE COEFFICIENT OF SOLID GRAIN (IN/SEC 0.095 \$BOLDGG /GASGEN/)
CI	CCHIP	NO AVAILABLE DEFINITION (/TRAJ/)
CI	CCHIR	NO AVAILABLE DEFINITION (/TRAJ/)
CI	CCLEN	CHAMBER LENGTH (IN --- \$--- //EQ///)
CI	CCRIT	CRITICAL THERMAL CONDUCTIVITY OF REGEN COOLANT (BTU/IN**2/SEC/DEGR/IN --- \$--- /COOLNT/)
CI	CCRITF	FUEL CRITICAL THERMAL CONDUCTIVITY

Figure 5.1. Common Block Variables (Sheet 3 of 46)

CI	CORITO	(BTU/IN/SEC/DEGR --- \$---- /PROPRO/) OX CRITICAL THERMAL CONDUCTIVITY
CI	CDESOG	(BTU/IN/SEC/DEGR --- \$---- /PROPRO/) DESIGN COMPLEXITY MULTIPLIER ON GAS GENERATOR
CI	CDIFL	(--- 1.25 \$OLDGG /GASGEN/) FUEL INJECTOR DISCHARGE COEFFICIENT
CI	CDIOX	(--- 0.77 \$INJECT /LIQUID/) OXIDIZER INJECTOR DISCHARGE COEFFICIENT
CI	CDVLVF	(--- 0.72 \$INJECT /LIQUID/) NO AVAILABLE DEFINITION (/TCA/)
CI	CDVLVD	(--- 0.72 \$INJECT /LIQUID/) NO AVAILABLE DEFINITION (/TCA/)
CI	CFTCAB	ABLATIVE THICKNESS COEFFICIENT FOR CHAMBER (--- 0. \$ABLATE /TCA/)
CI	CFTNAB	ABLATIVE THICKNESS COEFFICIENT FOR NOZZLE (--- 0. \$ABLATE /TCA/)
CI	CFTTAB	ABLATIVE THICKNESS COEFFICIENT FOR THROAT (--- 0. \$ABLATE /TCA/)
CI	CFVLS	NO AVAILABLE DEFINITION (/SSCOM/)
CI	CGAMA	NO AVAILABLE DEFINITION (/TRAJ/)
CI	CHIDOT	COMMAND CONSTANT INERTIAL PITCH RATE; INPUT FOR TRAJECTORY GUIDANCE SECTIONS UTILIZING GUIDANCE OPTION 5 (DEG/SEC --- \$GUIDA ///EQ///)
CI	CHIP	NO AVAILABLE DEFINITION (/TRAJ/)
CI	CHIPO	INITIAL VALUE OF INERTIAL ATTITUDE (DEG --- \$INTRAJ /TRAJ/)
CI	CHIPC	COMMANDED CONSTANT INERTIAL ATTITUDE; INPUT FOR TRAJECTORY GUIDANCE SECTIONS UTILIZING GUIDANCE OPTION 2 (DEG --- \$GUIDA ///EQ///)
CI	CHIR	NO AVAILABLE DEFINITION (/TRAJ/)
CI	CHMULT	COOLING CHANNEL MULTIPLIER IN REGEN COOLING LOGIC (--- 1.0 \$INREGN /WTREGN/)
CI	CHPOPC	NO AVAILABLE DEFINITION (/LIQUID/)
CI	CHRPIX	CHARACTERS PER INCH OUTPUT BY THE LINE PRINTER IN THE HORIZONTAL DIRECTION (USED BY PSEUDO-TEKTRONIX ROUTINES) (CHAR/IN 10 \$NCTINP /PSUTEK/)
CI	CHRPIY	CHARACTERS PER INCH IN THE Y DIRECTION OUTPUT BY THE LINE PRINTER (FOR PSEUDO-TEKTRONIX ROUTINE) (CHAR/IN 6 \$NCTINP /PSUTEK/)
CI	CLOVOL	CLOSEOUT VOLUME OF REGENERATIVELY COOLED CHAMBER (IN**3 --- \$---- /WTREGN/)
CI	CLRAF	SPACE BETWEEN AFT AND FORWARD TANK HEADS (IN 0.0 \$LTANK /TANKS/)
CI	CLRFP	SPACE BETWEEN FORWARD TANK HEAD AND PRESSURE TANK HEAD (IN 0.0 \$LTANK /TANKS/)
CI	CLRNOZ	(NOT USED)
CI	CLRTNK	(IN 0.0 \$NOZZLE ///EQ///) CLEARANCE BETWEEN NON-CONVENTIONAL TANKS WHEN LOADING THEM INTO STAGE ENVELOPE (IN 2.0 \$NCTINP /NCTIN/)
CI	CM	MOTOR EFFICIENCY FOR EACH STAGE; AFFECTS THRUST ONLY (--- 0.9 \$PROPEL /MOTOR/)
CI	CMMAX	MAXIMUM CARRY MOMENT (IN/LBF 0.0 \$LTANK /TANKS/)
CI	CN	AERODYNAMIC NORMAL FORCE COEFFICIENTS INPUT AS FUNCTIONS OF MACH NUMBER AND ANGLE OF ATTACK.

Figure 5.1. Common Block Variables (Sheet 4 of 46)

CI	CNMLI	CN(I,J) CORRESPONDS TO AMACH(I) AND ALPH(J) (---- \$AEROD /AERO/) EFFECTIVE THERMAL CONDUCTIVITY OF MULTILAYER INSULATION (MLI)	I
CI	CNSOFI	(BTU/IN-SEC-DEGR 4. E-9 \$TANKHX /INSLHX/) EFFECTIVE THERMAL CONDUCTIVITY OF SPRAY ON FOAM, INSULATION (SOFI)	I
CI	CNSTRN	(BTU/IN-SEC-DEGR 3. 5E-7 \$TANKHX /INSLHX/) VALUE OF CONSTRAINT (---- \$INPOPT /OPTIM/)	I
CI	CNW	NO AVAILABLE DEFINITION (/MOTOR/)	I
CI	CONDCT	MATERIAL THERMAL CONDUCTIVITY TABLE	I
CI	CONDGG	(BTU/IN-SEC-DEGR . 00023, . 0001, 8*0 \$LIQMAT /MTPPCP CONDENSATION LOSS MULTIPLIER FOR SOLID GG (---- \$--- /GASGEN/)	I
CI	CONDNZ	NOZZLE EXTENSION THERMAL CONDUCTIVITY AT TNENOM (BTU/IN/SEC/DEGR . 000555 \$LIQENG /COOLNT/)	I
CI	CONREF	PRODUCT OF EQUIVALENCE RATIO AND MIXTURE RATIO FOR USER DEFINED PROPELLANT (IPROP=0) (---- 2. 249 \$LPROP /EQUIVR/)	I
CI	CONSIM	PRODUCT OF EQUIVALENCE RATIO AND MIXTURE RATIO FOR THE LIBRARY PROPELLANT (---- \$--- /EQUIVR/)	I
CI	CONTOL	TOLERANCE FOR CONSTRAINT (---- \$INPOPT /OPTIM/)	I
CI	CPCNAF	CONSTANT IN EQUATION OF IDEAL GAS HEAT CAPACITY FOR FUEL (---- \$LFUEL /PROPRO/)	I
CI	CPCNAO	CONSTANT IN EQUATION OF IDEAL GAS HEAT CAPACITY FOR OX (---- \$LOXID /PROPRO/)	I
CI	CPCNBF	CONSTANT IN EQUATION OF IDEAL GAS HEAT CAPACITY FOR FUEL (---- \$LFUEL /PROPRO/)	I
CI	CPCNBO	CONSTANT IN EQUATION OF IDEAL GAS HEAT CAPACITY FOR OX (---- \$LOXID /PROPRO/)	I
CI	CPCNCF	CONSTANT IN EQUATION OF IDEAL GAS HEAT CAPACITY FOR FUEL (---- \$LFUEL /PROPRO/)	I
CI	CPCNCO	CONSTANT IN EQUATION OF IDEAL GAS HEAT CAPACITY FOR OX (---- \$LOXID /PROPRO/)	I
CI	CPCNDF	CONSTANT IN EQUATION OF IDEAL GAS HEAT CAPACITY FOR FUEL (---- \$LFUEL /PROPRO/)	I
CI	CPCNDO	CONSTANT IN EQUATION OF IDEAL GAS HEAT CAPACITY FOR OX (---- \$LOXID /PROPRO/)	I
CI	CPCONA	IDEAL HEAT CAPACITY CONSTANT (---- 3. 89 \$LPROP /COOLNT/)	I
CI	CPCONB	IDEAL HEAT CAPACITY CONSTANT (---- 23. 2 \$LPROP /COOLNT/)	I
CI	CPCONC	IDEAL HEAT CAPACITY CONSTANT (---- -9. 818 \$LPROP /COOLNT/)	I
CI	CPCOND	IDEAL HEAT CAPACITY CONSTANT (---- 1. 666 \$LPROP /COOLNT/)	I
CI	CPFACT	HEAT CAPACITY CORRECTION FACTOR TO REFERENCE HEAT CAPACITY (CPREF) (---- \$--- /COOLNT/)	I

Figure 5.1. Common Block Variables (Sheet 5 of 46)

CPFCTF	NO AVAILABLE DEFINITION (/PROPRO/)	I
CPFCTD	NO AVAILABLE DEFINITION (/PROPRO/)	I
CPGGPB	HEAT CAPACITY OF GAS GENERATOR/PREBURNER COMBUSTION GAS (BTU/LB/DEGR . 721 \$PUMP /TPAIN/)	I
CPLINF	FRACTION OF FACE P ACROSS FUEL LINE (--- 0.172 \$LIQUID /LIQUID/)	I
CPLINO	FRACTION OF FACE P ACROSS OXIDIZER LINE (--- 0.207 \$LIQUID /LIQUID/)	I
CPREF	REFERENCE HEAT CAPACITY FOR COOLANT (BTU/LBM/DEGR 0.725 \$LPROP /COOLNT/)	I
CPREFF	FUEL REFERENCE HEAT CAPACITY (BTU/LB/DEGR --- \$LFUEL /PROPRO/)	I
CPREFD	OX REFERENCE HEAT CAPACITY (BTU/LB/DEGR --- \$LOXID /PROPRO/)	I
CPVLVF	FRACTION OF FACE P ACROSS FUEL VALVE (--- 0.409 \$LIQUID /LIQUID/)	I
CPVLVO	FRACTION OF FACE P ACROSS OXIDIZER VALVE (--- 0.28 \$LIQUID /LIQUID/)	I
CR	CONTRACTION RATIO OF LIQUID ENGINE (--- 2.54 \$LIQENG ///EQ///)	I
CREF	REFERENCE THERMAL CONDUCTIVITY FOR COOLANT (BTU/IN/SEC/DEGR 3.85E-6 \$LPROP /COOLNT/)	I
CREFFL	FUEL REFERENCE THERMAL CONDUCTIVITY (BTU/IN/SEC/DEGR --- \$LFUEL /PROPRO/)	I
CREFOX	OX REFERENCE THERMAL CONDUCTIVITY (BTU/IN/SEC/DEGR --- \$LOXID /PROPRO/)	I
CSGG	SOLID GRAIN CHARACTERISTIC VELOCITY (FT/SEC 3932. \$SOLDGG /GASGEN/)	I
CSREFF	CSTAR EFFICIENCY (--- --- \$--- /LIQUID/)	I
CSRMX	CSTAR FOR USER PROPELLANT AT PC=500 AND QFRMX (FT/SEC 5689. \$LPROP /EQUIVR/)	I
CSRODE	IDEAL ONE DIMENSIONAL EQUILIBRIUM CSTAR (FT/SEC --- \$--- /LIQUID/)	I
CSSMMX	CSTAR OF LIBRARY PROPELLANT AT MAX ISP FOR PC=500 E=20 (FT/SEC --- \$--- /EQUIVR/)	I
CSTAR	PROPELLANT CHARACTERISTIC VELOCITY INPUT AS A FUNCTION OF CHAMBER PRESSURE; CSTAR(J, I) CORRESPONDS TO PCR(J) FOR THE I-TH STAGE (FT/SEC 0. \$PROPEL /MOTOR/)	I
CSTARL	DELIVERED CSTAR FOR TCA (KPERF=0) (FT/SEC 5523. \$LQPERF /LIQUID/)	I
CSTODE	IDEAL CHARACTERISTIC VELOCITY TABLES (FT/SEC --- \$--- /OPCOND/)	I
CTMLT	MULTIPLIER ON THRUST COEFFICIENT FOR PLUG CLUSTERS AND ANNULAR ENGINES (--- 0.99 \$NOZZLE /PLUGCL/)	I
CTOL	NO AVAILABLE DEFINITION (/CUT/)	I
CV	START VALVE COMPLEXITY MULTIPLIER (--- 1.0 \$PUMP /TPAIN/)	I
CVACUM	ACCUMULATOR VALVE COMPLEXITY MULTIPLIER (ISTART=2) (--- 1.0 \$PUMP /TPAIN/)	I
CVMAX	MAXIMUM VALUES FOR CONTROL VECTOR (IOPT) ELEMENTS (--- --- \$INPOPT /CVBOND/)	I
CVMIN	MINIMUM VALUES FOR CONTROL VECTOR (IOPT) ELEMENTS (--- --- \$INPOPT /CVBOND/)	I
CVMLTF	CONTROL VALVE PRESSURE DROP MULTIPLIER USED TO CALCULATE PRESSURE DROP FROM PUMP DISCHARGE TO	I

Figure 5.1. Common Block Variables (Sheet 6 of 46)

CI		GAS GENERATOR/PRE-BURNER INJECTOR INLET (--- 0.65 \$PUMP /PRESCH/)	I
CI		HEAT TRANSFER COEFFICIENT MULTIPLIER FOR HEAT EXCHANGER ON FUEL SIDE (--- .38073 \$--- /TPAIN/)	I
CI	CXHTCF	HEAT TRANSFER COEFFICIENT MULTIPLIER FOR HEAT EXCHANGER ON OXIDIZER SIDE (--- 0.23439 \$--- /TPAIN/)	I
CI		INJECTOR COMPLEXITY MULTIPLIER (--- 1. \$CXWMLT /TCA/)	I
CI	CXINJ	VALVE COMPLEXITY MULTIPLIER (--- 1. \$CXWMLT /TCA/)	I
CI	CXVALV	AFT TANK LINE WEIGHT MULTIPLIER (--- 1. \$CXWMLT /MULT/)	I
CI	CXWATL	AFT TANK WEIGHT MULTIPLIER (--- 1. \$--- /TWTMLT/)	I
CI	CXWATN	CHAMBER WEIGHT MULTIPLIER (--- 1. \$CXWMLT /TCA/)	I
CI	CXWDUC	HOT GAS DUCT WEIGHT MULTIPLIER (--- 2.5 \$PUMP /TPAIN/)	I
CI	CXWENG	ENGINE WEIGHT MULTIPLIER (--- 1.05 \$CXWMLT /TCA/)	I
CI	CXWFLT	FUEL TANK WEIGHT MULTIPLIER (--- 1. \$CXWMLT /TWTMLT/)	I
CI	CXWFTL	FORWARD TANK LINE WEIGHT MULTIPLIER (--- 1. \$CXWMLT /MULT/)	I
CI	CXWFTN	FORWARD TANK WEIGHT MULTIPLIER (--- 1. \$--- /TWTMLT/)	I
CI	CXWGIM	WEIGHT MULTIPLIER ON ENGINE GIMBALING SYSTEM (--- 1.0 \$CXWMLT /TWTMLT/)	I
CI	CXWIGG	GAS GENERATOR OR PRE-BURNER INJECTOR WEIGHT MULTIPLIER (--- 1.0 \$PUMP /TPAIN/)	I
CI	CXWLIN	ENGINE BAY PROPELLANT LINE WEIGHT MULTIPLIER (--- 2.5 \$PUMP /TPAIN/)	I
CI	CXWNCT	NO AVAILABLE DEFINITION (/NCTIN/)	I
CI	CXWNZE	NOZZLE EXTENSION WEIGHT MULTIPLIER (--- 1.1 \$CXWMLT /TCA/)	I
CI	CXWOXT	OXIDIZER TANK WEIGHT MULTIPLIER (--- 1. \$CXWMLT /TWTMLT/)	I
CI	CXPCH	PRESSURANT CONTROL HARDWARE WEIGHT MULTIPLIER (--- 1. \$CXWMLT /MULT/)	I
CI	CXWPTL	PRESSURE TANK LINE WEIGHT MULTIPLIER (--- 1. \$CXWMLT /MULT/)	I
CI	CXWPTN	PRESSURE TANK WEIGHT MULTIPLIER (--- 1. \$CXWMLT /TWTMLT/)	I
CI	CXWSTR	STRUCTURAL WALL WEIGHT MULTIPLIER (--- 1. \$CXWMLT /MULT/)	I
CI	CXWTHM	WEIGHT MULTIPLIER ON ENGINE THRUST MOUNT (--- 1.0 \$CXWMLT /TWTMLT/)	I
CI	CXWTNK	TANK WEIGHT MULTIPLIER (FOR BOTH TANDEM AND NON-CONVENTIONAL) (--- 1. \$CXWMLT /MULT/)	I
CI	CXWTPA	TURBOPUMP ASSEMBLY WEIGHT MULTIPLIER (--- 1. \$CXWMLT /TPAIN/)	I
CI	CYLLAT	CYLINDRICAL LENGTH OF AFT TANK (IN --- \$--- /TANKS/)	I
CI	CYLLFT	CYLINDRICAL LENGTH OF FORWARD TANK (IN --- \$--- /TANKS/)	I
CI	CYLLPT	CYLINDRICAL LENGTH OF PRESSURE TANK	I

Figure 5.1. Common Block Variables (Sheet 7 of 46)

CI	CYLTK	NO AVAILABLE DEFINITION	(/NCTOUT/)	I
CI	CZERFL	NO AVAILABLE DEFINITION	(/TPAOUT/)	I
CI	CZERO	NO AVAILABLE DEFINITION	(/TPAOUT/)	I
CI	CZEROX	NO AVAILABLE DEFINITION	(/TPAOUT/)	I
CI	DACCFL	NO AVAILABLE DEFINITION	(/TPOUT2/)	I
CI	DACCOX	NO AVAILABLE DEFINITION	(/TPOUT2/)	I
CI	DACQFL	FUEL TANK ACQUISITION DEVICE DENSITY (KACQFL=6)	(/TPOUT2/)	I
CI	DACQOX	(LB/IN**3 0.1 \$LTANK /TANKS2/)	OXIDIZER TANK ACQUISITION DEVICE DENSITY(KACQOX=6)	I
CI	DANBAS	(LB/IN**3 0.1 \$LTANK /TANKS2/)	DIAMETER OF BASE OF ANNULAR ENGINE	I
CI	DANEX	(IN --- \$--- /PLUGCL/)	DIAMETER OF ANNULAR THROAT OF ANNULAR ENGINE	I
CI	DBEXPA	(IN 48 \$NOZZLE /PLUGCL/)	EXPONENT ON REYNOLDS NUMBER IN LIQUID HEAT TRANSFER COEFFICIENT CALCULATION	I
CI	DBEXPB	(--- 0.95 \$LPROP /COOLNT/)	EXPONENT ON PRANDTL NUMBER IN LIQUID HEAT TRANSFER COEFFICIENT CALCULATION	I
CI	DBMLTK	(--- 0.4 \$LPROP /COOLNT/)	MULTIPLYING FACTOR IN LIQUID HEAT TRANSFER COEFFICIENT CALCULATION	I
CI	DBNDFL	(--- 0.005 \$LPROP /COOLNT/)	FUEL TANK BOND DENSITY	I
CI	DBNDOX	(LB/IN**3 .04 \$BLADER /TANKS2/)	OXIDIZER TANK BOND DENSITY	I
CI	DBOTFL	NO AVAILABLE DEFINITION	(/TPOUT2/)	I
CI	DBOTOX	NO AVAILABLE DEFINITION	(/TPOUT2/)	I
CI	DBPFL	NO AVAILABLE DEFINITION	(/TPAOUT/)	I
CI	DBPOX	NO AVAILABLE DEFINITION	(/TPAOUT/)	I
CI	DBRCSC	NO AVAILABLE DEFINITION	(/TPAOUT/)	I
CI	DCBAT	CENTER BODY DIAMETER IN AFT TANK	(IN --- \$--- /TANKS/)	I
CI	DCBFT	CENTER BODY DIAMETER IN FORWARD TANK	(IN --- \$--- /TANKS/)	I
CI	DCHAM	CHAMBER INSIDE DIAMETER	(IN --- \$--- /LIQUID/)	I
CI	DCHARC	REFERENCE CHAR DEPTH IN CHAMBER	(IN 1.02 \$ABLATE /TCA/)	I
CI	DCHARN	NOZZLE REFERENCE CHAR DEPTH	(IN 0.087 \$ABLATE /TCA/)	I
CI	DCHART	REFERENCE CHAR DEPTH IN THROAT	(IN 1.33 \$ABLATE /TCA/)	I
CI	DCRIT	CRITICAL DENSITY OF REGEN COOLANT	(LBM/IN**3 --- \$--- /COOLNT/)	I
CI	DCRITF	FUEL CRITICAL DENSITY	(LB/IN**3 --- \$--- /PROPRO/)	I
CI	DCRITO	OX CRITICAL DENSITY	(LB/IN**3 --- \$--- /PROPRO/)	I
CI	DDUCBF	NO AVAILABLE DEFINITION	(/TPOUT2/)	I
CI	DDUCFL	NO AVAILABLE DEFINITION	(/TPOUT2/)	I
CI	DDUCOX	NO AVAILABLE DEFINITION	(/TPOUT2/)	I
CI	DDUCT	NO AVAILABLE DEFINITION	(/TPOUT2/)	I
CI	DDUCTI	NO AVAILABLE DEFINITION	(/TPOUT2/)	I
CI	DEEXIT	EXIT DIAMETER	(IN --- \$--- /SSCOM/)	I
CI	DEL	INITIAL OPTIMIZATION STEP SIZE	(--- 5 \$INPOPT /OPTIM/)	I

Figure 5.1. Common Block Variables (Sheet 8 of 46)

CI	DELCHK	NO AVAILABLE DEFINITION (//EQ///)
CI	DELINC	INCLINATION CHANGE
CI	DELMIN	(DEG 0.0 \$ORB //EQ///)
CI		MINIMUM OPTIMIZATION STEP SIZE FOR CONVERGENCE
CI	DELT	(---- \$INPOPT /OPTIM/)
CI		TRAJECTORY INTEGRATION TIME STEP INTERVAL
CI		(CONSTANT DURING FLIGHT)
CI	DELT24	(SEC 1 \$INTRAJ /TRAJ/)
CI	DELTAP	NO AVAILABLE DEFINITION (/TRAJ/)
CI		TOTAL DELTA P ACROSS REGEN JACKET
CI		(PSI --- \$--- /COOLNT/)
CI	DELTAT	TOTAL DELTA T ACROSS REGEN JACKET
CI		(DEGR --- \$--- /COOLNT/)
CI	DELTAV	NO AVAILABLE DEFINITION (//EQ///)
CI	DELTEE	NO AVAILABLE DEFINITION (/TPAOUT/)
CI	DELTFL	NO AVAILABLE DEFINITION (/TPAOUT/)
CI	DELTOX	NO AVAILABLE DEFINITION (/TPAOUT/)
CI	DEXIT	NOZZLE EXIT DIAMETER
CI		(IN --- \$--- /LSCOM/)
CI	DFL	FUEL PUMP DIAMETER
CI		(IN --- \$--- /TPAOUT/)
CI	DFL2	NO AVAILABLE DEFINITION (/TPOUT2/)
CI	DFLJ	FUEL INJECTOR ORIFICE DIAMETER
CI		(IN --- \$--- /LIQUID/)
CI	DGGPB	NO AVAILABLE DEFINITION (/TPOUT2/)
CI	DGPRD	NO AVAILABLE DEFINITION (/CONST/)
CI	DHVAPF	FUEL HEAT OF VAPORIZATION AT NORMAL BOILING POINT
CI		(BTU/LB --- \$LFUEL /PROPRO/)
CI	DHVAPD	OX HEAT OF VAPORIZATION AT NORMAL BOILING POINT
CI		(BTU/LB --- \$LOXID /PROPRO/)
CI	DIFTBF	USED TO CALCULATE BARRIER TEMPERATURE FOR REGEN
CI		COOLED CHAMBERS AND TRANS-REGEN CHAMBERS USING
CI		TBARRIER = DIFTBF * (TCORE - TGWNOM) + TGWNOM
CI		(--- 1.0 \$INREGN //EQ///)
CI	DLAFT	AFT LINE DIAMETER
CI		(IN --- \$--- /TANKS/)
CI	DLBPFL	NO AVAILABLE DEFINITION (/TPOUT2/)
CI	DLBPOX	NO AVAILABLE DEFINITION (/TPOUT2/)
CI	DLFWD	FORWARD LINE DIAMETER
CI		(IN --- \$--- /TANKS/)
CI	DLMPFL	NO AVAILABLE DEFINITION (/TPOUT2/)
CI	DLMPOX	NO AVAILABLE DEFINITION (/TPOUT2/)
CI	DMINSG	MINIMUM ALLOWABLE SOLID GRAIN DIAMETER
CI		(IN 3.0 \$SOLDGG /TANKS/)
CI	DMOTOR	MOTOR OUTSIDE DIAMETER INCLUDING EXTERNAL
CI		INSULATION
CI		(IN 66. \$INPGEN //EQ///)
CI	DNMLI	MULTILAYER INSULATION (MLI) DENSITY
CI		(LBM/IN**3 .002 \$TANKHX /TANKS2/)
CI	DNSOFI	SPRAY ON FOAM INSULATION (SOFI) DENSITY
CI		(LBM/IN**3 .00127 \$TANKHX /TANKS2/)
CI	DOX	OXIDIZER PUMP DIAMETER
CI		(IN --- \$--- /TPAOUT/)
CI	DOX2	NO AVAILABLE DEFINITION (/TPOUT2/)
CI	DOXJ	OXIDIZER INJECTOR ORIFICE DIAMETER
CI		(IN --- \$--- /LIQUID/)
CI	DPBLDA	AFT BLADDER DELTA P
CI		(PSI --- \$--- /TANKS/)
CI	DPBLDF	FORWARD BLADDER DELTA P
CI		(PSI --- \$--- /TANKS/)

Figure 5.1. Common Block Variables (Sheet 9 of 46)

CI	DPBLFL	FUEL BLADDER DELTA P (PSI --- \$--- /PRESCH/)
CI	DPBLOX	OXIDIZER BLADDER DELTA P (PSI --- \$--- /PRESCH/)
CI	DPBPFL	DELTA P BETWEEN FUEL IN TANK AND BOOST PUMP INLET (PSIA --- \$--- /PRESCH/)
CI	DPBPOX	DELTA P BETWEEN OX IN TANK AND BOOST PUMP INLET (PSIA --- \$--- /PRESCH/)
CI	DPGPBF	FUEL DELTA P ACROSS GAS GENERATOR/PREBURNER INJECTOR (PSIA --- \$--- /PRESCH/)
CI	DPGPBO	OX DELTA P ACROSS GAS GENERATOR/PREBURNER INJECTOR (PSIA --- \$--- /PRESCH/)
CI	DPIJFL	FUEL INJECTOR DELTA P (PSI --- \$--- /LIQUID/)
CI	DPIJOX	OXIDIZER INJECTOR DELTA P (PSI --- \$--- /LIQUID/)
CI	DPLNFL	FUEL LINE DELTA P (PSI --- \$--- /LIQUID/)
CI	DPLNOX	OXIDIZER LINE DELTA P (PSI --- \$--- /LIQUID/)
CI	DPPMPF	DELTA P ACROSS FUEL PUMP (PSIA --- \$--- /PRESCH/)
CI	DPPMPO	DELTA P ACROSS OX PUMP (PSIA --- \$--- /PRESCH/)
CI	DPREGF	FUEL DELTA P ACROSS REGEN JACKET (PSIA --- \$--- /PRESCH/)
CI	DPREGO	OX DELTA P ACROSS REGEN JACKET (PSIA --- \$--- /PRESCH/)
CI	DPSYSF	FUEL FEED SYSTEM DELTA P (PSI --- \$--- /LIQUID/)
CI	DPSYSO	OXIDIZER FEED SYSTEM DELTA P (PSI --- \$--- /LIQUID/)
CI	DPTURB	DELTA P ACROSS TURBINE (PSIA --- \$--- /PRESCH/)
CI	DPVLVF	FUEL VALVE DELTA P (PSI --- \$--- /LIQUID/)
CI	DPVLVO	OXIDIZER VALVE DELTA P (PSI --- \$--- /LIQUID/)
CI	DREF	REFERENCE VALUE OF DENSITY FOR COOLANT (LB/IN**3 0.0327 \$LPROP /COOLNT/)
CI	DREFFL	FUEL REFERENCE DENSITY (LB/IN**3 --- \$LFUEL /PROPRO/)
CI	DREFOX	OX REFERENCE DENSITY (LB/IN**3 --- \$LOXID /PROPRO/)
CI	DRGL	NO AVAILABLE DEFINITION (/TRAJ/)
CI	DRGLOS	IDEAL VELOCITY LOSSES DUE TO AERODYNAMIC DRAG (FT/SEC 0 \$INTRAJ /TRAJ/)
CI	DSPH	NO AVAILABLE DEFINITION (/TPOUT2/)
CI	DTBPFL	FUEL DELTA T ACROSS BOOST PUMP (DEGR --- \$--- /TEMSCH/)
CI	DTBPOX	OX DELTA T ACROSS BOOST PUMP (DEGR --- \$--- /TEMSCH/)
CI	DTHRT	INITIAL THROAT DIAMETER (IN --- \$--- /LSCOM/)
CI	DTIJFL	FUEL DELTA T ACROSS TCA INJECTOR (DEGR --- \$--- /TEMSCH/)
CI	DTIJOX	OX DELTA T ACROSS TCA INJECTOR (DEGR --- \$--- /TEMSCH/)
CI	DTLNFL	FUEL DELTA T ACROSS FEED LINE

Figure 5.1. Common Block Variables (Sheet 10 of 46)

CI	DTLNOX	(DEGR ---- \$---- /TEMSCH/) OX DELTA T ACROSS FEED LINE	I
CI	DTPA	(DEGR ---- \$---- /TEMSCH/) NO AVAILABLE DEFINITION (/TPOUT2/)	I
CI	DTPABF	NO AVAILABLE DEFINITION (/TPOUT2/)	I
CI	DTPABO	NO AVAILABLE DEFINITION (/TPOUT2/)	I
CI	DTPAFL	NO AVAILABLE DEFINITION (/TPOUT2/)	I
CI	DTPAOX	NO AVAILABLE DEFINITION (/TPOUT2/)	I
CI	DTPMPF	FUEL DELTA T ACROSS MAIN PUMP (DEGR ---- \$---- /TEMSCH/)	I
CI	DTPMPO	OX DELTA T ACROSS MAIN PUMP (DEGR ---- \$---- /TEMSCH/)	I
CI	DTREGF	FUEL DELTA T ACROSS REGEN JACKET (DEGR ---- \$---- /TEMSCH/)	I
CI	DTREGO	OX DELTA T ACROSS REGEN JACKET (DEGR ---- \$---- /TEMSCH/)	I
CI	DTTURB	TEMPERATURE DROP ACROSS TURBINE (DEGR ---- \$---- /TEMSCH/)	I
CI	DTURB	TURBINE DIAMETER (IN --- \$---- /TPAOUT/)	I
CI	DTURBF	NO AVAILABLE DEFINITION (/TPAOUT/)	I
CI	DTURBO	NO AVAILABLE DEFINITION (/TPAOUT/)	I
CI	DTVLVF	FUEL DELTA T ACROSS BIPROP VALVE (DEGR ---- \$---- /TEMSCH/)	I
CI	DTVLVO	OX DELTA T ACROSS BIPROP VALVE (DEGR ---- \$---- /TEMSCH/)	I
CI	DVREQ	NO AVAILABLE DEFINITION (/MOTOR/)	I
CI	E	REGEN STATION LOCAL AREA RATIO (--- --- \$---- /RGNSUM/)	I
CI	EAFSKT	MODULUS OF ELASTICITY OF STAGE AFT SKIRT (LBF/IN**2 29. E6 \$INTSTG /MOTOR/)	I
CI	EARIR	EARTH INFRA-RED HEAT FLUX (KHXOPT=2)	I
CI	EARREF	(BTU/SEC-IN**2 1. 35E-4 \$TANKHX /INSLHX/) EARTH REFLECTANCE (ALBEDO) (KHXOPT=2)	I
CI	EBRGG	(--- 0. 39 \$TANKHX /INSLHX/) BURN RATE EXPONENT OF SOLID GRAIN	I
CI	ECASE	(--- 0. 64 \$SOLDGG /GASGEN/) MODULUS OF ELASTICITY OF CASE MATERIAL	I
CI	ECCEN	(LBF/IN**2 29. E6 \$MATER /MOTOR/)	I
CI	ECFTHR	NO AVAILABLE DEFINITION (///EQ///) TABLE OF NOZZLE EFFICIENCIES FOR THROTTLED PRESSURE FRACTIONS	I
CI	ECSVAP	(--- --- \$THROT /THREFF/) CSTAR VAPORIZATION EFFICIENCY	I
CI	EDES	(--- --- \$---- /LIQUID/) ECCENTRICITY OF DESTINATION ORBIT	I
CI	EECRAT	(--- 0. 0 \$ORB ///EQ///) EXTENDABLE EXIT CONE EXPANSION RATIO	I
CI	EINSTG	(--- 1. 5 \$NOZZLE ///EQ///) MODULUS OF ELASTICITY OF INTERSTAGE MATERIAL AT THE TOP OF EACH LOWER STAGE	I
CI	ELDENS	(LBF/IN**2 1. 8E6 \$INTSTG /MOTOR/) INJECTOR ELEMENT DENSITY	I
CI	ELDOME	(ELEMENTS/IN**2 3. 1 \$INJECT ///EQ///) ELLIPSE RATIO FOR THE CASE/TANK DOMES	I
CI	ELLCHM	(--- 1. \$INPGEN ///EQ///) NO AVAILABLE DEFINITION (/NCTIN/)	I
CI	ELLTNK	NO AVAILABLE DEFINITION (/NCTIN/)	I
CI	ELPRIM	NO AVAILABLE DEFINITION (/NCTIN/)	I
CI	ELRP	PRESSURE TANK ELLIPSE RATIO	I

Figure 5.1. Common Block Variables (Sheet 11 of 46)

CI	EMISTC	THRUST CHAMBER EMMISIVITY FOR TCA RADIATION COOLING MODEL (--- 1.0 \$FLTANK //EQ///)	I
CI	EMISVE	VEHICLE EMMISIVITY IN ENGINE BAY FOR TCA RADIATION COOLING MODEL (--- 0.9 \$LIQENG /COOLNT/)	I
CI	ENDROV	NUMBER OF ENDS PER ROVING (--- 0.5 \$LIQENG /COOLNT/)	I
CI	ENDVAL	NO AVAILABLE DEFINITION (//EQ///)	I
CI	ENDVLO	VALUE OF ENDING PARAMETER AT WHICH GUIDANCE SECTION IS TO BE TERMINATED (--- --- \$GUIDA //EQ///)	I
CI	ENDVLM	VALUE OF MOTOR ENDING PARAMETER AT WHICH MOTOR SECTION IS TO BE TERMINATED (--- --- \$GUIDA //EQ///)	I
CI	ENGANG	NO AVAILABLE DEFINITION (/NCTIN/)	I
CI	ENGRAD	NO AVAILABLE DEFINITION (/NCTIN/)	I
CI	ENGSPC	MINIMUM SPACE BETWEEN NOZZLE EXITS IN NON-CONVENTIONAL TANK DESIGN (IN 2.0 \$NCTINP /NCTIN/)	I
CI	EPARK	ECCENTRICITY OF PARKING ORBIT (--- 0.0 \$ORB //EQ///)	I
CI	EPIPE	ABSOLUTE SURFACE ROUGHNESS OF COOLING CHANNELS (IN 0.00008 \$INREGN /COOLNT/)	I
CI	EPS	NOMINAL EXPANSION RATIO FOR EACH STAGE (--- 10. \$INPGEN //EQ///)	I
CI	EPSATT	EXPANSION RATIO AT THE NOZZLE-DOME ATTACH POINT FOR SOLID STAGES. EXPANSION RATIO WHERE RADIATION COOLED NOZZLE IS ATTACHED FOR LIQUID STAGES (--- 1. \$INPGEN //EQ///)	I
CI	EPSEEC	AVERAGE EXPANSION RATIO (--- --- \$--- //EQ///)	I
CI	EPSGGB	AREA RATIO OF BLEED NOZZLE (--- 2.0 \$PUMP /TPAIN/)	I
CI	EPSPLG	PLUG CLUSTER OVERALL AREA RATIO (--- --- \$--- /PLUGCL/)	I
CI	EPSR	REFERENCE EXPANSION RATIO AT WHICH PROPELLANT BALLISTIC PERFORMANCE DATA IS INPUT: SHOULD APPROXIMATE FINAL DESIGN EXPANSION RATIO (--- 10. \$PROPEL /MOTOR/)	I
CI	EPSTH	HOOP FIBER ULTIMATE STRAIN (% 0.015 \$FILMNT /MOTOR/)	I
CI	EPSTRD	DOWNTSTREAM AREA RATIO FOR TRANSPIRATION COOLING (--- 1.2 \$INREGN /TRANCO/)	I
CI	EPSTRU	UPSTREAM AREA RATIO FOR TRANSPIRATION COOLING (--- 2 \$INREGN /TRANCO/)	I
CI	EPTRAT	ATTACH AREA RATIO OF TRANSLATING NOZZLE (--- 50 \$LIQENG /TRANZO/)	I
CI	EREMIX	MIXING EFFICIENCY (--- --- \$--- /LIQUID/)	I
CI	EREMRD	MIXTURE RATIO MALDISTRIBUTION LOSS MULTIPLIER (--- --- \$--- /LIQUID/)	I
CI	ERETHR	TABLE OF CHAMBER EFFICIENCIES FOR THROTTLED PRESSURE FRACTIONS (--- --- \$THROT /THREFF/)	I
CI	EREVAP	VAPORIZATION EFFICIENCY (--- --- \$--- /LIQUID/)	I
CI	ERFCHR	REFERENCE AREA RATIO FOR DCHARN (--- 7.5 \$ABLATE /TCA/)	I

Figure 5.1. Common Block Variables (Sheet 12 of 46)

CI	ERMR	PRODUCT OF EQUIVALENCE RATIO AND MIXTURE RATIO (--- \$--- /LIQUID/)	I
CI	ERRMX	EQUIVALENCE RATIO OF USER PROPELLANT AT REFERENCE MIXTURE RATIO (OFRMX) (--- \$--- /EQUIVR/)	I
CI	ERSMMX	EQUIVALENCE RATIO OF LIBRARY PROPELLANT AT MAX ISP FOR PC=500 E=20 (--- \$--- /EQUIVR/)	I
CI	ETABAR	LOSS MULTIPLIER ON BARRIER PERFORMANCE (--- 0.9 \$LQPERF /LIQUID/)	I
CI	ETABL	BOUNDARY LAYER LOSS MULTIPLIER (--- \$--- /LIQUID/)	I
CI	ETACF	NOZZLE PERFORMANCE EFFICIENCY (--- \$--- /LIQUID/)	I
CI	ETADIV	DIVERGENCE LOSS MULTIPLIER (--- \$--- /LIQUID/)	I
CI	ETAERE	CHAMBER ENERGY RELEASE EFFICIENCY (--- \$--- /LIQUID/)	I
CI	ETAGGB	GAS GENERATOR BLEED PERFORMANCE LOSS MULTIPLIER (--- \$--- /TPAOUT/)	I
CI	ETAKE	KINETIC LOSS EFFICIENCY (--- \$--- /LIQUID/)	I
CI	ETASUB	NO AVAILABLE DEFINITION (/SSCOM/)	I
CI	ETATP	TWO PHASE FLOW LOSS MULTIPLIER (--- \$--- /LIQUID/)	I
CI	EXPLFL	FUEL TANK EXPULSION EFFICIENCY (--- .995 \$LTANK /TANKS/)	I
CI	EXPLOX	OXIDIZER TANK EXPULSION EFFICIENCY (--- .995 \$LTANK /TANKS/)	I
CI	EXPULA	EXPULSION EFFICIENCY OF AFT TANK (--- 0.99 \$--- /TANKS/)	I
CI	EXPULF	EXPULSION EFFICIENCY OF FORWARD TANK (--- 0.99 \$--- /TANKS/)	I
CI	F	NO AVAILABLE DEFINITION (/PERF/)	I
CI	FAA	NO AVAILABLE DEFINITION (/TRAJ/)	I
CI	FADFL	NO AVAILABLE DEFINITION (/TPAOUT/)	I
CI	FADMIS	TURBINE ADMISSION FRACTION (--- \$--- /TPAOUT/)	I
CI	FADOX	NO AVAILABLE DEFINITION (/TPAOUT/)	I
CI	FALFAF	ALLOWABLE HELICAL FIBER STRESS (LBF/IN**2 270000. \$FILMNT /MOTOR/)	I
CI	FANBAS	NO AVAILABLE DEFINITION (/PLUGCL/)	I
CI	FANMOT	FRACTION OF MOTOR DIAMETER USED FOR CALCULATING EXIT DIAMETER (DANEX) OF ANNULAR ENGINE (--- 0.8 \$NOZZLE /PLUGCL/)	I
CI	FASKTL	AFT SKIRT FRACTIONAL LENGTH OF ENGINE BAY LENGTH (FOR NON-CONVENTIONAL TANKS IT IS THE AFT SKIRT FRACTIONAL LENGTH OF STAGE LENGTH) (--- 0.067 \$LIQUID /TANKS/)	I
CI	FCHGFL	FRACTION OF INJECTOR FACE PRESSURE FOR FUEL DELTA P ACROSS INJECTOR (--- 0.15 \$LIQUID ///EQ///)	I
CI	FCHGOX	FRACTION OF INJECTOR FACE PRESSURE FOR OX DELTA P ACROSS INJECTOR (--- 0.15 \$LIQUID ///EQ///)	I
CI	FEEDK	INTERNAL CONSTANT USED TO OPTIMIZE PROPELLANT PRESSURE SCHEDULE (--- 1.0 \$--- ///EQ///)	I
CI	FFFC	FUEL FILM COOLING FRACTION (--- \$--- /LIQUID/)	I

Figure 5.1. Common Block Variables (Sheet 13 of 46)

CI	FFLV	FRACTION OF FUEL WHICH IS VAPORIZED (--- \$--- /LIQUID/)	I
CI	FFSKTL	FORWARD SKIRT FRACTIONAL LENGTH OF FORWARD DOME HEIGHT (FOR NON-CONVENTIONAL TANKS IT IS THE FORWARD SKIRT FRACTIONAL LENGTH OF STAGE DIAMETER) (--- 0.3 \$LIQUID /TANKS/)	I
CI	FH20GG	MOLAR FRACTION OF WATER IN COMBUSTION PRODUCTS OF GAS GENERATOR (--- 0.2662 \$SOLDGG /GASGEN/)	I
CI	FLKFCF	NUMBER OF VELOCITY HEADS LOST IN FUEL FEED LINE DUE TO BENDS, VALVES, ETC. (VEL-HEADS 5. \$LTANK /TANKS2/)	I
CI	FLNPSH	FUEL PUMP NET POSITIVE SUCTION HEAD (FT --- \$--- /TPAOUT/)	I
CI	FLNPSP	FUEL NET POSITIVE SUCTION PRESSURE IN TANK (PSIA 10. \$PUMP /PRESCH/)	I
CI	FLOPEL	NUMBER OF FUEL ORIFICES/ELEMENT (--- 2.0 \$INJECT /ELEMEN/)	I
CI	FLTTIM	STAGE ACTION TIME (USED IN TANK HEAT LOSS) (SEC 100. \$TANKHX /INSLHX/)	I
CI	FNA	NO AVAILABLE DEFINITION (/TRAJ/)	I
CI	FOXV	FRACTION OF OXIDIZER WHICH IS VAPORIZED (--- \$--- /LIQUID/)	I
CI	FPGGMR	FRACTION OF MAXIMUM GAS GENERATOR OPERATING PRESSURE LOST ACROSS GAS GENERATOR'S INJECTOR (--- 0.65 \$PUMP ///EQ///)	I
CI	FPLUGV	PLUG CLUSTER VACUUM DELIVERED THRUST (LBF --- \$--- /PLUGCL/)	I
CI	FPULCG	MULTIPLYING FACTOR ON ULLAGE PRESSURE TO CALCULATE MINIMUM GAS BOTTLE BLOWDOWN PRESSURE (--- 0.8 \$COLDG /COLDG/)	I
CI	FPULGG	MULTIPLYING FACTOR ON ULLAGE PRESSURE TO CALCULATE MINIMUM OPERATING GAS GENERATOR PRESSURE (--- 1.1 \$SOLDGG /GASGEN/)	I
CI	FRACYL	RATIO OF CHAMBER CYLINDRICAL LENGTH TO TOTAL CHAMBER LENGTH (--- \$--- /LIQUID/)	I
CI	FT	THRUST VALUES INPUT FOR SPECIFYING MOTOR PERFORMANCE; USED IN VARIABLE THRUST-TIME TABLE WHERE FT(J, I) CORRESPONDS TO TBRN(J) FOR THE ITH STAGE (LBF 0.0 \$THVST /PERF/)	I
CI	FTHF	ALLOWABLE HOOP FIBER STRESS (LBF/IN**2 300000. \$FILMNT /MOTOR/)	I
CI	FTPNCMI	NO AVAILABLE DEFINITION (/CONST/)	I
CI	FVAC	VACUUM THRUST PER LIQUID THRUST CHAMBER (LBF 0.0 \$LIQUID ///EQ///)	I
CI	FVACD	VACUUM DELIVERED THRUST (LBF --- \$--- /PERF/)	I
CI	FVENTF	FRACTION OF FUEL TANK NOMINAL ULLAGE PRESSURE AT WHICH VENT OCCURS (--- 1.1 \$TANKHX /INSLHX/)	I
CI	FVENTO	FRACTION OF OX TANK NOMINAL ULLAGE PRESSURE AT WHICH VENT OCCURS (--- 1.1 \$TANKHX /INSLHX/)	I
CI	FWEB	WEB FRACTION (--- 0.85 \$--- /MOTOR/)	I
CI	G	NO AVAILABLE DEFINITION (/TRAJ/)	I
CI	GO	GRAVITATIONAL CONSTANT (FT/SEC**2 32.174 \$--- /CONST/)	I

Figure 5.1. Common Block Variables (Sheet 14 of 46)

CI	GA	NO AVAILABLE DEFINITION (/TRAJ/)	I
CI	GAGE	NO AVAILABLE DEFINITION (/TPAOUT/)	I
CI	GAGEFL	NO AVAILABLE DEFINITION (/TPAOUT/)	I
CI	GAGEOX	NO AVAILABLE DEFINITION (/TPAOUT/)	I
CI	GAMABO	NO AVAILABLE DEFINITION (///EQ///)	I
CI	GAMAX	NO AVAILABLE DEFINITION (/TRAJ/)	I
CI	GAMDOT	COMMANDER RATE OF CHANGE OF FLIGHT PATH ANGLE; INPUT FOR TRAJECTORY GUIDANCE SECTIONS (DEG/SEC 0. \$GUIDA ///EQ///)	I
CI	GAMGG	GAS GENERATOR COMBUSTION PRODUCTS SPECIFIC HEAT RATIO (--- 1.27 \$SOLDGG /GASGEN/)	I
CI	GAMGPB	RATIO OF SPECIFIC HEATS OF GAS GENERATOR/PREBURNER COMBUSTION GAS (--- 1.25 \$PUMP /TPAIN/)	I
CI	GAMICG	COLD GAS ISENTROPIC RATIO OF SPECIFIC HEAT (--- 1.66 \$COLDG /COLDGP/)	I
CI	GAMM	NO AVAILABLE DEFINITION (/SSCOM/)	I
CI	GAMMA	NO AVAILABLE DEFINITION (/TRAJ/)	I
CI	GAMMAO	NO AVAILABLE DEFINITION (/TRAJ/)	I
CI	GAMMAC	COMMANDER CONSTANT FLIGHT PATH ANGLE; INPUT FOR GUIDANCE SECTIONS UTILIZING GUIDANCE OPTION 3 (DEG -1.E20 \$GUIDA ///EQ///)	I
CI	GAMMAI	INITIAL MISSILE FLIGHT PATH ANGLE (DEG 90. \$INTRAJ ///EQ///)	I
CI	GAMMAL	APPROXIMATION OF LIQUID COMBUSTION PRODUCTS RATIO OF SPECIFIC HEATS (--- --- \$--- /LIQUID/)	I
CI	GAMPBG	COLD GAS POLYTROPIC GAMMA AT INFINITE TIME (--- 1. \$COLDG /COLDGP/)	I
CI	GAMRED	NO AVAILABLE DEFINITION (///EQ///)	I
CI	GAMSTG	NO AVAILABLE DEFINITION (/TRAJ/)	I
CI	GASMW	MOLECULAR WEIGHT OF PRESSURIZATION GAS (ISTART=2: (LBM/LB-MOLE 28 \$PUMP /TPAIN/)	I
CI	GG	NO AVAILABLE DEFINITION (/GSTOR/)	I
CI	GGCR	GAS GENERATOR OR PRE-BURNER CONTRACTIN RATIO (--- 12 \$PUMP /TPAIN/)	I
CI	GIMINT	INTERFERENCE GIMBAL ANGLE OF ADJACENT NOZZLES (DEG --- \$--- /GIMBAL/)	I
CI	GMAX	NO AVAILABLE DEFINITION (/TRAJ/)	I
CI	GMBANG	MAXIMUM ANGLE TO WHICH NOZZLES GIMBAL (DEG 6.0 \$LIQUID /GIMBAL/)	I
CI	GN	NO AVAILABLE DEFINITION (/TRAJ/)	I
CI	GNMAX	NO AVAILABLE DEFINITION (/TRAJ/)	I
CI	GNW	NO AVAILABLE DEFINITION (/MOTOR/)	I
CI	GPC	NO AVAILABLE DEFINITION (/TRAJ/)	I
CI	GPOLY	COLD GAS POLYTROPIC RATIO OF SPECIFIC HEATS (--- --- \$--- /COLDGP/)	I
CI	GRAVL	NO AVAILABLE DEFINITION (/TRAJ/)	I
CI	GREMAX	NO AVAILABLE DEFINITION (/TRAJ/)	I
CI	GREMIN	NO AVAILABLE DEFINITION (/TRAJ/)	I
CI	GREMN1	NO AVAILABLE DEFINITION (/TRAJ/)	I
CI	GRVLOS	IDEAL VELOCITY LOSSES DUE TO GRAVITY FORCES (FT/SEC 0 \$INTRAJ /TRAJ/)	I
CI	GTOT	NO AVAILABLE DEFINITION (/TRAJ/)	I
CI	GTPARM	NO AVAILABLE DEFINITION (/TRAJ/)	I
CI	GTURN	COMMANDER TOTAL ACCELERATION DURING MISSILE TURN; INPUT FOR GUIDANCE SECTIONS USING GUIDANCE OPT 6 (DEG 0. \$GUIDA ///EQ///)	I
CI	GUIPAR	NO AVAILABLE DEFINITION (///EQ///)	I

Figure 5.1. Common Block Variables (Sheet 15 of 46)

CI	QUIPAR	NO AVAILABLE DEFINITION (/TRAJ/)	I
CI	GWMING	MINIMUM GUAGE OF CHAMBER GAS WALL (IN 0.025 \$INREGN /WTREGN/)	I
CI	GWVOL	GAS WALL MATERIAL VOLUME IN REGEN CHAMBER (IN**3 ---- \$---- /WTREGN/)	I
CI	H	AN APPROXIMATION OF HESSIAN USED IN THE QUASI- NEWTON UNCONSTRAINED FUNCTION MINIMIZATION (--- --- \$NLP /RGNSUM/)	I
CI	HAFPI	NO AVAILABLE DEFINITION (/CONST/)	I
CI	HBFL	NO AVAILABLE DEFINITION (/TPAOUT/)	I
CI	HBLADE	NO AVAILABLE DEFINITION (/TPAOUT/)	I
CI	HBOX	NO AVAILABLE DEFINITION (/TPAOUT/)	I
CI	HPFPL	NO AVAILABLE DEFINITION (/TPAOUT/)	I
CI	HBPOX	NO AVAILABLE DEFINITION (/TPAOUT/)	I
CI	HC	REGEN STATION LOCAL COOLANT SIDE HEAT TRANSFER COEFFICIENT (BTU/IN**2/SEC/DEGR --- \$--- /RGNSUM/)	I
CI	HCPFPL	NO AVAILABLE DEFINITION (/TPAOUT/)	I
CI	HCBPOX	NO AVAILABLE DEFINITION (/TPAOUT/)	I
CI	HCFL	NO AVAILABLE DEFINITION (/TPAOUT/)	I
CI	HCFL2	NO AVAILABLE DEFINITION (/TPAOUT/)	I
CI	HCONI	NO AVAILABLE DEFINITION (/MOTOR/)	I
CI	HCOX	NO AVAILABLE DEFINITION (/TPAOUT/)	I
CI	HCOX2	NO AVAILABLE DEFINITION (/TPAOUT/)	I
CI	HFL	HEAD RISE OF FUEL PUMP (FT --- \$--- /TPAOUT/)	I
CI	HFL2	NO AVAILABLE DEFINITION (/TPAOUT/)	I
CI	HG	REGEN STATION LOCAL GAS SIDE HEAT TRANSFER COEFF (BTU/IN**2/SEC/DEGR --- \$--- /RGNSUM/)	I
CI	HH	NO AVAILABLE DEFINITION (/HSTOR/)	I
CI	HLDTIM	STAGE HOLD TIME (USED IN TANK HEAT LOSS) (SEC 100. \$TANKHX /INSLHX/)	I
CI	HOMMAX	MAXIMUM DEPTH TO WIDTH RATIO IN COOLING CHANNELS (--- 5.0 \$INREGN /COOLNT/)	I
CI	HOX	HEAD RISE OF OXIDIZER PUMP (FT --- \$--- /TPAOUT/)	I
CI	HOX2	NO AVAILABLE DEFINITION (/TPAOUT/)	I
CI	HTRNOZ	HEIGHT OF TRANSLATING PORTION OF NOZZLE (IN --- \$--- /TRANOZ/)	I
CI	HTURB	NO AVAILABLE DEFINITION (/TPOUT2/)	I
CI	HTURBF	NO AVAILABLE DEFINITION (/TPOUT2/)	I
CI	HTURBO	NO AVAILABLE DEFINITION (/TPOUT2/)	I
CI	HXALT	AVERAGE ORBITAL ALTITUDE FROM EARTH SURFACE (KHXOPT=2) (MILES 125. \$TANKHX /INSLHX/)	I
CI	IAM4	FLAG SPECIFYING TRAJECTORY METHOD -1 = 4TH ORDER RUNGE-KUTTA INTEGRATION THROUGHOUT 0 = 4TH ORDER RUNGE-KUTTA DURING MOTOR BURN 4TH ORDER ADAMS-MOULTON AFTER BURNOUT +1 = 4TH ORDER ADAMS-MOULTON THROUGHOUT FLIGHT (--- 0 \$INTRAJ /TRAJ/)	I
CI	IBELL	FLAG INDICATING NOZZLE TYPE 0 = CONICAL NOZZLE 1 = CONTOURED NOZZLE (CIRCULAR ARC) 2 = ELLIPSOIDAL OR HYPERBOLIC NOZZLE (--- 0 \$NOZZLE /MOTOR/)	I
CI	ICOAST	NO AVAILABLE DEFINITION (/PERF/)	I
CI	ICOMPS	COMPOSITE CASE INDICATOR 0 = METAL CASE 1 = COMPOSIT CASE	I

Figure 5.1. Common Block Variables (Sheet 16 of 46)

CI	ICON	(--- 0 \$MATER /MOTOR/) (I,1) - REFERENCE NUMBER OF VARIABLE TO BE CONSTRANED (I,2) - CONSTRAINT TYPE -1 = LESS THAN OR EQUAL 0 = EQUAL TO +1 = GREATER THAN OR EQUAL (--- --- \$INPOPT /OPTIM/)
CI	ICPFAG	WARNING FLAG FOR HEAT CAPACITY ROUTINE CALLED WITH OUT OF RANGE INPUT
CI	ICPFLG	WARNING FLAG FOR HEAT CAPACITY ROUTINE CALL WITH OUT OF RANGE INPUTS
CI	ICRYFL	(--- 0 \$--- /WARN/) FUEL CRYOGENIC FLAG (0=STORABLE, 1=CRYOGENIC)
CI	ICRYOX	OXIDIZER CRYOGENIC FLAG (0=STORABLE, 1=CRYOGENIC)
CI	ICRYTM	(--- 0 \$LFLAG /LIQUID/) NO AVAILABLE DEFINITION (/TEMSCH/)
CI	ICS	ICS = 1 - PREPREG WINDING = 1 - WET WIND (--- 0 \$FILMNT /MOTOR/)
CI	IDRAW	NON-CONVENTIONAL TANK DRAW FLAG (1=DRAW THREE VIEWS ON ONE PAGE, 2=DRAW EACH VIEW ON A SEPARATE PAGE) (--- 2 \$NCTINP /NCTIN/)
CI	IDTRAN	TRANSPIRATION COOLING CRITERIA FLAG (1=USE QMAXTR TO CALCULATE EPSTRD AND EPSTRU, 2=USE THE INPUT VALUES FOR EPSTRD AND EPSTRU) (--- 2 \$INREGN /TRANCO/)
CI	IELDEN	INJECTOR ELEMENT DENSITY FLAG 0 = INPUT NUMBER OF ORIFICES 1 = INPUT ELEMENT DENSITY (--- 0 \$INJECT /ELEMEN/)
CI	IENDPG	NO AVAILABLE DEFINITION (///EQ///)
CI	IENDPM	NO AVAILABLE DEFINITION (///EQ///)
CI	IENDPR	NO AVAILABLE DEFINITION (///EQ///)
CI	IENDPR	NO AVAILABLE DEFINITION (/TRAJ/)
CI	IENEC	FLAG INDICATING EXTENDABLE EXIT CONE 0 = NONE 1 = SEGMENT CONE 2 = GAS DEPLOYED SKIRT (--- 0 \$NOZZLE /MOTOR/)
CI	IERRMD	NO AVAILABLE DEFINITION (/CVBOND/)
CI	IFREGN	REGEN COOLING FLUID FLAG 0 = OXIDIZER IS COOLANT 1 = FUEL IS COOLANT (--- 1 \$INREGN /COOLNT/)
CI	IFUEL	NO AVAILABLE DEFINITION (/TPAIN/)
CI	IGPHSE	NO AVAILABLE DEFINITION (/TRAJ/)
CI	IGUID	NO AVAILABLE DEFINITION (/TRAJ/)
CI	IGUISC	NO AVAILABLE DEFINITION (/TRAJ/)
CI	IHYPER	HYPERGOLIC PROPELLANT FLAG (REQUIRED FOR NON- LIBRARY PROPELLANTS (IPROP=0)) 0 = NOT HYPERGOLIC 1 = HYPERGOLIC (--- 1 \$LFLAG /LIQUID/)
CI	ILIFT	NO AVAILABLE DEFINITION (/AERO/)
CI	IMMAN	NO AVAILABLE DEFINITION (/MOTOR/)
CI	INDES	DESIGN LOOP INDICATOR +1 = MOTOR IS SIMULATED, NO TRAJECTORY INTEGRATION

Figure 5.1. Common Block Variables (Sheet 17 of 46)

CI 0 = TRAJECTORY INTEGRATION
 CI -1 = TRAJECTORY INTEGRATION PLUS DELTA V CALC
 CI -2 = TRAJECTORY USING THRUST-TIME TRACE, NO
 CI MOTOR SIMULATION
 CI (--- \$INPOPT /TRAJ/)
 CI INPUT FUEL TANK EXPULSION EFFICIENCY FLAG (0=I
 CI CALCULATE EXPULSION EFFICIENCY, 1=USE VALUE INPUT
 CI FOR EXPLFL) I
 CI (--- 0 \$LFLAG /TANKS/) I
 CI INPUT OXIDIZER TANK EXPULSION EFFICIENCY FLAG I
 CI (0=CALCULATE EXPULSION EFFICIENCY, 1=USE VALUE I
 CI INPUT FOR EXPLOX) I
 CI (--- 0 \$LFLAG /TANKS2/) I
 CI NO AVAILABLE DEFINITION (/NCTIN/) I
 CI INDEX SPECIFYING THE OPTIMIZATION OBJECTIVE FUNC I
 CI (--- \$INPOPT /OPTIM/) I
 CI NO AVAILABLE DEFINITION (/PRINT/) I
 CI PARAMETER OPTIMIZATION SWITCHES (SEE METHOD OF I
 CI MULTIPLIERS DOCUMENTATION) I
 CI (--- 0 \$INPOPT /OPTIM/) I
 CI NO AVAILABLE DEFINITION (/OPTIM/) I
 CI NO AVAILABLE DEFINITION (/TRAJ/) I
 CI NO AVAILABLE DEFINITION (/OPTIM/) I
 CI TWO PHASE FLOW WARNING FLAG I
 CI (--- \$--- /COOLNT/) I
 CI INDEX FLAG FOR PLOT DATA (GENERATES TAPE 4 FOR RPL I
 CI CALCOMP PLOT ROUTINES). THE OPTIMIZER SHOULD BE I
 CI OFF FOR THIS FEATURE. I
 CI 0 = NO PLOT I
 CI 1 = PLOT I
 CI (--- 0 \$INPOPT /TRAJ/) I
 CI PLUG CLUSTER FLAG I
 CI 0 = NO PLUG CLUSTER I
 CI 1 = PLUG CLUSTER I
 CI 2 = ANNULAR ENGINE I
 CI (--- 0 \$LIQUID /PLUGCL/) I
 CI OUTPUT PRINT INDICATOR I
 CI IPRINT(1) - INPUT DATA FILE I
 CI 0 = NO PRINTOUT I
 CI 1= PRINT INPUT I
 CI IPRINT(2) - INITIAL GUESS DESIGN I
 CI 0 = NO PRINTOUT I
 CI 1 = PRINT MOTOR SUMMARY I
 CI 2 = PRINT MOTOR SUMMARY AND TRAJECTORY PROFILE I
 CI IPRINT(3) - NOT USED I
 CI IPRINT(4) - FINAL DESIGN I
 CI 0 = NO PRINTOUT I
 CI 1 = PRINT MOTOR SUMMARY I
 CI 2 = PRINT MOTOR SUMMARY AND TRAJECTORY PROFILE I
 CI IPRINT(5) - NUMBER OF FINAL DESIGN SUMMARIES I
 CI ALSO I
 CI A VARIABLE OF THE SAME NAME IS USED IN \$NLP AS A I
 CI FLAG USED TO CONTROL INTERMEDIATE ITERATION I
 CI PRINTOUT VALUES RANGE FROM 0 TO 11. THE GREATER I
 CI THE VALUE THE GREATER THE INTERMEDIATE OUTPUT I
 CI (--- 1 \$INPOPT /OPTIM/) I
 CI PROPELLANT SELECTION FLAG I
 CI 0 = NON-LIBRARY PROPELLANT I
 CI 1 = N2O4/MMH I
 CI 2 = MON-25/MHF-3 I

Figure 5.1. Common Block Variables (Sheet 18 of 46)

CI 3 = CLF5/MHF-3
 CI 4 = MON-25/60%MFH-3 + 40% AL
 CI 5 = LO2/LH2
 CI 6 = LO2/RP-1
 CI 7 = LO2/CH4
 CI 8 = LF2/LH2
 CI 9 = LF2/N2H4
 CI (--- 0 \$LFLAG /LIQUID/)
 CI IPRSIM PROPELLANT SIMILARITY FLAG (IPROP = 0)
 CI (--- 1 \$LPROP /LIQUID/)
 CI IPRTFL NO AVAILABLE DEFINITION (/PRINT/)
 CI IPUTMP NO AVAILABLE DEFINITION (/TEMSCH/)
 CI IPRRNT REGENERATIVE COOLING PRINT FLAG
 CI 0 = NO PRINTOUT OF REGEN SUMMARY
 CI 1 = PRINT REGEN SUMMARY
 CI (--- 0 \$INREGN /COOLNT/)
 CI ISET NO AVAILABLE DEFINITION (/ATMOS/)
 CI ISF NO AVAILABLE DEFINITION (/AERO/)
 CI ISTART TPA START SYSTEM FLAG
 CI 0=TANK HEAD 1=COLD GAS SPIN 2=START TANKS
 CI 3=SOLID CARTRIDGE
 CI (--- 0 \$PUMP /TPAIN/)
 CI ISTG NO AVAILABLE DEFINITION (/PERF/)
 CI ITARGE NO AVAILABLE DEFINITION (/TRAJ/)
 CI ITB BURN TIME INTERPOLATION INDEX
 CI (--- 1 \$--- /PERF/)
 CI ITER NO AVAILABLE DEFINITION (/PERF/)
 CI ITERAT NO AVAILABLE DEFINITION (/TPAOUT/)
 CI ITLIM OPTIMIZER ITERATION LIMIT (BASE POINT)
 CI (--- 500 \$INPOPT /OPTIM/)
 CI ITRMAX NO AVAILABLE DEFINITION (/CUT/)
 CI IVEH VEHICLE SCHEMATIC ARRAY
 CI (--- --- \$--- /LPRVLI/)
 CI IWARN ARRAY OF WARNING MESSAGE FLAGS
 CI (--- 0 \$--- /WARN/)
 CI IWDFIX NO AVAILABLE DEFINITION (/FIXFLG/)
 CI JBPFL FUEL BOOST PUMP SELECTION FLAG
 CI 0 = NO BOOST PUMP FOR FUEL
 CI 1 = BOOST PUMP
 CI (--- 0 \$PUMP /TPAIN/)
 CI JBPOX OXIDIZER BOOST PUMP SELECTION FLAG
 CI 0 = NO BOOST PUMP FOR OXIDIZER
 CI 1 = BOOST PUMP
 CI (--- 0 \$PUMP /TPAIN/)
 CI JCNFIG TPA CONFIGURATION FLAG
 CI 1=GEARBOX 2=SINGLE SHAFT TPA 3=TWIN TPA IN
 CI SERIES 4=PARALLEL TPAS
 CI (--- 2 \$PUMP /TPAIN/)
 CI K NO AVAILABLE DEFINITION (/SSCOM/)
 CI KACQFL KIND OF FUEL ACQUISITION DEVICE (0=NO ACQUISITION
 CI DEVICE, 1=TRANSVERSE COLLAPSING ALUMINUM BLADDER.
 CI 2=FULL BONDED ROLLING DIAPHRAM(AL), 3=HALF BRD (AL)
 CI 4=FULL BRD (SS), 5=HALF BRD (SS), 6=SURFACE
 CI TENSION ACQUISITION DEVICE)
 CI (--- 0 \$LFLAG /TANKS/)
 CI KACQOX KIND OF OXIDIZER ACQUISITION DEVICE (SEE KACQFL)
 CI (--- 0 \$LFLAG /TANKS/)
 CI KALCON CALCULATE TANK INSULATION THERMAL CONDUCTIVITIES
 CI FLAG (0=USE INPUT, 1=CALCULATE)
 CI (--- 1 \$TANKHX /INSLHX/)

Figure 5.1. Common Block Variables (Sheet 19 of 46)

CI	KALMOD	FLAG DETERMINES CALCULATION MODE FOR NON-CONVENTIONAL TANKS (0=USE DIMENSIONLESS INPUT , 1= USE MAJOR TANK DIMENSION (RMAJ)) (--- 0 \$NCTINP /NCTIN/)	I
CI	KBLAT	AFT TANK BLADDER FLAG 0 = NO BLADDER 1 = TRANSVERSE COLLAPSING ALUMINUM BLADDER 2 = FULL BONDED ROLLING DIAPHRAM (ALUMINUM) 3 = HALF BONDED ROLLING DIAPHRAM (ALUMINUM) 4 = FULL BONDED ROLLING DIAPHRAM (STAINLESS STEEL) 5 = HALF BONDED ROLLING DIAPHRAM (STAINLESS STEEL) (--- 0 \$--- /TANKS/)	I
CI	KBLFT	FORWARD TANK BLADDER FLAG (SEE KBLAT) (--- 0 \$--- /TANKS/)	I
CI	KCYCLE	0 = PRESSURE FED 1 = PUMP FED (GG BLEED) 2 = STAGED COMBUSTION (FUEL RICH PREBURNER) 3 = EXPANDER CYCLE (HYDROGEN FUEL) 4 = STAGED REACTION (MONOPROPellant FUEL) (--- 0 \$LFLAG /TPAIN/)	I
CI	KDOME	COMMON DOME FLAG FOR AFT AND FORWARD TANKS 0 = SEPARATE HEADS 1 = COMMON DOME (--- 1 \$TNKGEO /TANKS/)	I
CI	KEXNOZ	NOZZLE EXTENSION FLAG 0 = NO EXTENSION 1 = NOZZLE EXTENSION (--- 1 \$LIQENG /MAITCA/)	I
CI	KGAS	PROPELLANT TANK PRESSURIZATION FLAG 1 = SOLID GAS GENERATOR 2 = COLD GAS PRESSURIZATION (USED IF OX AND FUEL TANKS DO NOT USE AUTOGENDOUS PRESSURIZATION) (--- 2 \$LFLAG /TANKS/)	I
CI	KGASFL	FUEL TANK AUTOGENDOUS PRESSURIZATION FLAG (0=USE KGAS TYPE PRESSURIZATION, 1=AUTOGENDOUS) (--- 0 \$LFLAG /TANKS/)	I
CI	KGASOX	OX TANK AUTOGENDOUS PRESSURIZATION FLAG (0=USE KGAS TYPE PRESSURIZATION, 1=AUTOGENDOUS) (--- 0 \$LFLAG /TANKS/)	I
CI	KGIMB	MODE OF GIMBALING FLAG FOR MULTIPLE TCA'S (NOT USED AT PRESENT) (--- 2 \$LIQUID /GIMBAL/)	I
CI	KGPOWR	FLAG WHICH DETERMINES LOCATION OF GIMBALING POWER SUPPLY 0 = NOT ON STAGE 1 = ON STAGE (--- 0 \$LIQUID /GIMBAL/)	I
CI	KHXOPT	TANK HEAT TRANSFER OPTION (0=IGNORE TANK HEAT TRANSFER, 1=EXTERNAL BOUNDARY EXPOSED TO CONDUCTIVE SOURCE, 2=WORST CASE SOLAR RADIATION, 3=CONDUCTIVE AND CONVECTIVE SOURCE WITH GROUND-HOLD LAYER OF ICE) (--- 0 \$LFLAG /INSLHX/)	I
CI	KLINEA	FEED LINE FLAG 0 = EXTERNAL FEED LINE 1 = INTERNAL FEED LINE (--- 1 \$TNKGEO /TANKS/)	I
CI	KNEST	ENGINE NESTING FLAG FOR NON-CONVENTIONAL TANKS (0=NO NESTING, 1=NEST EACH ENGINE INDEPENDENTLY)	I

Figure 5.1. Common Block Variables (Sheet 20 of 46)

CI		2=NEST ENGINES TO SAME EXIT PLANE, 3=NEST ENGINES TO EXIT PLANE AT END OF TANKAGE + XMOUNT)	I
CI		(--- 2 \$NCTINP /NCTIN/)	I
CI	KNOZ	NOZZLE TYPE FLAG	I
CI		1 = CONICAL	I
CI		2 = RAO	I
CI		(--- 1 \$LIQENG /LIQUID/)	I
CI	KOOLNZ	NOZZLE COOLING METHOD FLAG (1=ABLATIVE, 2=REGEN, 3=TRANS-REGEN, 4=RADIATION, 5=FLIM)	I
CI		(--- 1 \$LFLAG /COOLNT/)	I
CI	KOOLTC	THRUST CHAMBER COOLING METHOD FLAG (1=ABLATIVE, 2=REGEN, 3=TRANS-REGEN, 4=RADIATION)	I
CI		(--- 1 \$LFLAG /COOLNT/)	I
CI	KORBOR	NO AVAILABLE DEFINITION (/INSLHX/)	I
CI	KPERF	ENGINE PERFORMANCE FLAG	I
CI		0 = INPUT PERFORMANCE (DO NOT CALCULATE)	I
CI		1 = CALCULATE ENGINE PERFORMANCE	I
CI		(--- 1 \$LFLAG /MAILPE/)	I
CI	KPRESS	PRESSURE TANK LOCATION FLAG	I
CI		0 = SPHERICAL IN ENGINE BAY	I
CI		1 = SUSPENDED FORWARD OF FORWARD TANK	I
CI		2 = MONOCOQUE SEPARATE DOME	I
CI		3 = MONOCOQUE COMMON DOME	I
CI		4 = CYLINDRICAL IN FORWARD TANK	I
CI		(--- 0 \$TNKGEO /TANKS/)	I
CI	KPRPA	PROPELLANT LOCATION FLAG	I
CI		1 = FUEL IN AFT TANK	I
CI		2 = OXIDIZER IN AFT TANK	I
CI		(--- 2 \$TNKGEO /TANKS/)	I
CI	KPUMP	1 = 1 TPA ASSEMBLY PER STAGE	I
CI		2 = 1 TPA ASSEMBLY PER ENGINE	I
CI		(--- 1 \$PUMP /TPAIN/)	I
CI	KREG	THROAT REGRESSION FLAG	I
CI		0 = NO REGRESSION	I
CI		1 = (NOT USED)	I
CI		2 = INPUT THROAT REGRESSION COEFFICIENTS	I
CI		(--- 1 \$LFLAG /LIQUID/)	I
CI	KSTAGE	FLAG INDICATING STAGE TYPE	I
CI		1 = SOLID STAGE	I
CI		2 = LIQUID STAGE	I
CI		3 = LIQUID STAGE INTEGRATED WITH LOWER STAGE (MUST USE NON-CONVENTIONAL TANKAGE)	I
CI		(--- 1 \$INPGEN /STAGE/)	I
CI	KTANKS	NO AVAILABLE DEFINITION (/NCTIN/)	I
CI	KTHICK	NO AVAILABLE DEFINITION (/NCTIN/)	I
CI	KTRNOZ	KIND OF TRANSLATING NOZZLE FLAG (0=NONE, 1=SPRING ACTUATED, 2=GAS DEPLOYED)	I
CI		(--- 0 \$LIQENG /TRANZOZ/)	I
CI	KWTMOD	ENGINE WEIGHT MODEL FLAG	I
CI		-1 = INPUT ENGINE WEIGHT	I
CI		0 = SIMPLIFIED ABLATIVE ENGINE WEIGHT MODEL	I
CI		1 = PHYSICAL MODEL	I
CI		(--- 0 \$LFLAG /TCA/)	I
CI	KXATAH	AFT TANK AFT HEAD CONVEXITY FLAG	I
CI		-1 = CONVEX FORWARD	I
CI		i = CONVEX AFT	I
CI		(--- 1 \$TNKGEO /TANKS/)	I
CI	KXATFH	AFT TANK FORWARD HEAD CONVEXITY FLAG	I
CI		-1 = CONVEX FORWARD	I
CI		1 = CONVEX AFT	I

Figure 5.1. Common Block Variables (Sheet 21 of 46)

CI	KXFTAH	(--- -1 \$TNKGEO /TANKS/) FORWARD TANK AFT HEAD CONVEXITY FLAG -1 = CONVEX FORWARD 1 = CONVEX AFT	I
CI	KXFTFH	(--- -1 \$TNKGEO /TANKS/) FORWARD TANK FORWARD HEAD CONVEXITY FLAG -1 = CONVEX FORWARD 1 = CONVEX AFT	I
CI	LABEL	(--- -1 \$TNKGEO /TANKS/) NO AVAILABLE DEFINITION (/PLABEL/)	I
CI	LNFULL	LINES FULL AT BURNOUT FLAG(0=EMPTY, 1=FULL)	I
CI	LOOP	(--- 1 \$LFLAG /TANKS2/) ITERATION LOOP COUNTER IN ROUTINE MAXRPM	I
CI	LOOPFL	(--- ---- \$---- /TPAOUT/) ITERATION LOOP COUNTER IN ROUTINE MAXRPM	I
CI	LOOPOX	(--- ---- \$---- /TPOUT2/) ITERATION LOOP COUNTER IN ROUTINE MAXRPM	I
CI	LTHRTL	(--- ---- \$---- /TPOUT2/) THROTTLING FLAG (LOGICAL --- \$---- /THRLOG/)	I
CI	LTPABF	NO AVAILABLE DEFINITION (/TPOUT2/)	I
CI	LTPABO	NO AVAILABLE DEFINITION (/TPOUT2/)	I
CI	LTURFD	TURBINE FEED LOCATION FLAG 0 = FEED TURBINE FROM REGEN OUTLET 1 = FEED TURBINE FROM UPSTREAM OF REGEN JACKET USING REGEN BYPASS FLOW SET BY THE VARIABLE BYPREG.	I
CI	LUSEP	(--- 0 \$LFLAG /SCHEDW/) PROPELLANT USE FLAG TRUE = ALL PROPELLANT IS TO BE BURNED FALSE = THRUST TERMINATES AT THE END OF THE LAST TIME INTERVAL IN TIMTHR FOR THAT STAGE	I
CI	MANDEG	(LOGICAL . TRUE. \$THROT /THRLOG/) METHOD OF ANNULAR ENGINE EXIT DIAMETER CALCULATION (0=INPUT DANEX, 1=CALCULATE DANEX AS DMOTOR*FANMOT	I
CI	MATAT	(--- 1 \$NOZZLE /PLUGCL/) MATERIAL FLAG FOR AFT TANK (IN ARRAYS RHO, SIGMAX, , AND YMOD)	I
CI	MATATL	(--- 1 \$---- /TANKS/) MATERIAL FLAG FOR AFT TANK LINE	I
CI	MATFT	(--- 1 \$---- /TANKS/) MATERIAL FLAG FOR FORWARD TANK	I
CI	MATFTL	(--- 1 \$---- /TANKS/) MATERIAL FLAG FOR FORWARD TANK LINE	I
CI	MATNKS	(--- 2 \$LIQMAT /TANKS/) NO AVAILABLE DEFINITION (/NCTIN/)	I
CI	MATPT	MATERIAL FLAG FOR PRESSURE TANK	I
CI	MATPTL	(--- 1 \$LIQMAT /TANKS/) MATERIAL FLAG FOR PRESSURE TANK LINES (IN ARRAYS RHO, SIGMAX, AND YMOD)	I
CI	MATSTR	(--- 1 \$LIQMAT /TANKS/) MATERIAL FOR STRUCTURAL WALL	I
CI	METHOD	NO AVAILABLE DEFINITION (/OPTIM/)	I
CI	MG	NO AVAILABLE DEFINITION (/GSTOR/)	I
CI	MH	NO AVAILABLE DEFINITION (/HSTOR/)	I
CI	MLIENV	MULTILAYER INSULATION (MLI) ENVIRONMENT FLAG (1=GROUNd HOLD WITH N2 PURGE, 2=GROUNd HOLD WITH HE PURGE, 3=SPACE HOLD WITH N2 PURGE AT PRGMLI PSIA, 4=SPACE HOLD WITH HE AT PRGMLI PSIA)	I

Figure 5.1. Common Block Variables (Sheet 22 of 46)

CI	MNCQA	(--- 1 \$TANKHX /INSLHX/) AFT TANK MONOCOQUE FLAG 0 = SUSPENDED TANK 1 = MONOCOQUE TANK
CI	MNCQF	(--- 1 \$TNKGEO /TANKS/) FORWARD TANK MONOCOQUE FLAG 0 = SUSPENDED TANK 1 = MONOCOQUE TANK
CI	MPHSE	(--- 1 \$TNKGEO /TANKS/) NO AVAILABLE DEFINITION (/TRAJ/)
CI	MTNKFL	MATERIAL FLAG FOR FUEL TANK AND FUEL LINES
CI	MTNKOX	(--- 1 \$LIQMAT /TANKS2/) MATERIAL FLAG FOR OXIDIZER TANK AND OXIDIZER LINES
CI	MX	(--- 1 \$LIQMAT /TANKS2/) NO AVAILABLE DEFINITION (/XSTOR/)
CI	N	NO AVAILABLE DEFINITION (/OPTIM/)
CI	NALPHA	NO AVAILABLE DEFINITION (/AERO/)
CI	NALTSF	NO AVAILABLE DEFINITION (/AERO/)
CI	NAME	NO AVAILABLE DEFINITION (/OPNAME/)
CI	NAMEP	PROPELLANT NAME (CHARACTER --- \$---- /PROPN/)
CI	NBPT	NO AVAILABLE DEFINITION (/THRLOG/)
CI	NCON	NUMBER OF SEGMENTS IN CONVERGENT CHAMBER SECTION FOR HEAT TRANSFER ANALYSIS (--- 5 \$INREGN /COOLNT/)
CI	NCRYOG	NUMBER OF CRYOGENIC PROPELLANTS ON BOARD THE STAGE (VALUES OF 0-2 FOR BI-PROPELLANT STAGE) (ONLY REQUIRED FOR NON-LIBRARY PROPELLANTS (IPROP=0)) (--- 0 \$---- /LIQUID/)
CI	NCTNK	NONCONVENTIONAL TANK SELECTION FLAG (0=TANDEM, 1= NON-CONVENTIONAL) (--- 0 \$LFLAG /NCTIN/)
CI	NCYL	NUMBER OF SEGMENTS IN CYLINDRICAL CHAMBER SECTION FOR HEAT TRANSFER ANALYSIS (--- 5 \$INREGN /COOLNT/)
CI	NELEM	NUMBER OF INJECTOR ELEMENTS (--- 336 \$INJECT /LIQUID/)
CI	NFLORF	NUMBER OF FUEL INJECTOR ORIFICES (--- 672 \$INJECT /LIQUID/)
CI	NGIMB	NUMBER OF GIMBALING NOZZLES (--- 1 \$LIQUID /GIMBAL/)
CI	NITHX	NUMBER OF ITERATIONS IN SUBROUTINE TANKHX WHICH CONTROLS THE ACCURACY OF TANK HEAT TRANSFER CALC (--- 8 \$TANKHX /INSLHX/)
CI	NMACH	NO AVAILABLE DEFINITION (/AERO/)
CI	NNOZ	NUMBER OF SOLID MOTOR NOZZLES PER STAGE (--- 1 \$NOZZLE /GENRL/)
CI	NNZL	NUMBER OF NOZZLE SEGMENTS USED IN HEAT TRANSFER ANALYSIS (--- 5 \$INREGN /COOLNT/)
CI	NODEAR	NUMBER OF ENTRIES IN AREA RATIO ARRAY ODEEPS (--- ---- \$---- /OPCOND/)
CI	NODEMR	NUMBER OF ENTRIES IN MIXTURE RATIO ARRAY ODEMR (--- ---- \$---- /OPCOND/)
CI	NODEPC	NUMBER OF ENTRIES IN CHAMBER PRESSURE ARRAY ODEPC (--- ---- \$---- /OPCOND/)
CI	NODKAR	NUMBER OF ENTRIES IN AREA RATIO ARRAY ODKEPS (--- ---- \$---- /OPCOND/)

Figure 5.1. Common Block Variables (Sheet 23 of 46)

CI	NODKMR	NUMBER OF ENTRIES IN ARRAY ODKMR (--- --- \$---- /OPCOND/)	I
CI	NODKPC	NUMBER OF ENTRIES IN ARRAY ODKPC (--- --- \$---- /OPCOND/)	I
CI	NOXORF	NUMBER OF OXIDIZER ORIFICES IN INJECTOR FACE (--- 500 \$INJECT /LIQUID/)	I
CI	NPCR	NUMBER OF REFERENCE CHAMBER PRESSURES (--- 1 \$PROPEL /MOTOR/)	I
CI	NPHSE	NO AVAILABLE DEFINITION (/TRAJ/)	I
CI	NPOINT	NUMBER OF HEAT TRANSFER ANALYSIS POINTS ALONG REGENERATIVELY COOLED CHAMBER (--- --- \$--- /RGNSUM/)	I
CI	NPRB	NUMBER OF PRESSURE BOTTLES IN ENGINE BAY (KPRESS = 0) (--- 1 \$TNKGEO /TANKS/)	I
CI	NR	NUMBER OF ENGINE RESTARTS (USED TO SIZE START SYSTEM) (--- 1 \$PUMP /TPAIN/)	I
CI	NRUNIT	NO AVAILABLE DEFINITION (/OPTIM/)	I
CI	NSTGES	NUMBER OF STAGES (--- 3 \$INPGEN /PERF/)	I
CI	NTANKS	TOTAL NUMBER OF NON-CONVENTIONAL TANKS ON STAGE (--- 3 \$NCTINP /NCTIN/)	I
CI	NTB	NUMBER OF POINTS DESCRIBING THRUST PROFILE (--- --- \$--- /PERF/)	I
CI	NTBL	NUMBER OF POINTS DESCRIBING THRUST PROFILE (--- --- \$--- /LIQUID/)	I
CI	NTC	NUMBER OF LIQUID THRUST CHAMBERS OR PLUG MODULES (--- 1 \$LIQENG /LIQUID/)	I
CI	NTHEFF	NUMBER OF ENTRIES IN TABLES THRPC, ECFTHR, AND ERETHR FOR EACH STAGE (--- 7 \$THROT /THREFF/)	I
CI	NTHINT	NUMBER OF THROTTLING INTERVALS (--- --- \$--- /THRLOG/)	I
CI	NTINT	NO AVAILABLE DEFINITION (/THRLOG/)	I
CI	NTMPIT	NUMBER OF INTERATIONS ON TEMPERATURE SCHEDULE IN SUBROUTINE LSTAGE. ALSO CONTROLS NUMBER OF ITERATIONS ON FLOWRATE SCHEDULE (--- 1 \$LIQUID /TEMSCH/)	I
CI	OBJSCL	SCALING FACTOR FOR OBJECTIVE FUNCTION (--- --- \$INPOPT /OPTIM/)	I
CI	OODEEPS	ARRAY OF AREA RATIOS CORRESPONDING TO ODE PERFORMANCE IN ARRAYS ODEST (--- --- \$--- /OPCOND/)	I
CI	ODEMR	ARRAY OF MIXTURE RATIOS CORRESPONDING TO ODE PERFORMANCE IN ARRAYS ODEST (--- --- \$--- /OPCOND/)	I
CI	ODEPC	ARRAY OF CHAMBER PRESSURE CORRESPONDING TO ODE PERFORMANCE IN ARRAYS ODEST (--- --- \$--- /OPCOND/)	I
CI	ODEST1	IDEAL ONE DIMENSIONAL EQUILIBRIUM ISP DATA ARRAY (--- --- \$--- /OPCOND/)	I
CI	ODEST2	IDEAL ONE DIMENSIONAL EQUILIBRIUM ISP DATA ARRAY (--- --- \$--- /OPCOND/)	I
CI	ODEST3	IDEAL ONE DIMENSIONAL EQUILIBRIUM ISP DATA ARRAY (--- --- \$--- /OPCOND/)	I
CI	ODEST4	IDEAL ONE DIMENSIONAL EQUILIBRIUM ISP DATA ARRAY (--- --- \$--- /OPCOND/)	I
CI	ODKEPS	NO AVAILABLE DEFINITION (/OPCOND/)	I
CI	ODKMR	ARRAY OF MIXTURE RATIOS CORRESPONDING TO ODK	I

Figure 5.1. Common Block Variables (Sheet 24 of 46)

CI		PERFORMANCE DATA IN ODKST	I
CI		(---- \$--- /OPCOND/)	I
CI	ODKPC	ARRAY OF CHAMBER PRESSURE CORRESPONDING TO ODK	I
CI		PERFORMANCE DATA IN ODKST	I
CI		(---- \$--- /OPCOND/)	I
CI	ODKST1	IDEAL ONE DIMENSIONAL KINETIC ISP DATA ARRAY	I
CI		(---- \$--- /OPCOND/)	I
CI	ODKST2	IDEAL ONE DIMENSIONAL KINETIC ISP DATA ARRAY	I
CI		(---- \$--- /OPCOND/)	I
CI	ODKST3	IDEAL ONE DIMENSIONAL KINETIC ISP DATA ARRAY	I
CI		(---- \$--- /OPCOND/)	I
CI	ODKST4	IDEAL ONE DIMENSIONAL KINETIC ISP DATA ARRAY	I
CI		(---- \$--- /OPCOND/)	I
CI	DFBARR	MIXTURE RATIO OF BARRIER	I
CI		(--- 1.0 \$--- //EQ///)	I
CI	DFCORE	MIXTURE OF GAS CORE IN LIQUID COMBUSTION CHAMBER	I
CI		(--- 1.9 \$LQPERF //EQ///)	I
CI	DFGOPB	MIXTURE RATIO OF GAS GENERATOR/PREBURNER	I
CI		(--- 0.1 \$PUMP /TPAIN/)	I
CI	DFMTC	OVERALL ENGINE MIXTURE RATIO (KPERF=0)	I
CI		(--- 1.782 \$LQPERF /LIQUID/)	I
CI	OFRMX	MIXTURE RATIO ON USER PROPELLANT AT MAX ISP.	I
CI		PC=500 (IPROP=0)	I
CI		(--- 2.03 \$LPROP /EQUIVR/)	I
CI	OMEGA	ACENTRIC FACTOR OF REGEN COOLANT	I
CI		(--- \$--- /COOLNT/)	I
CI	OMEGAF	FUEL ACENTRIC FACTOR	I
CI		(--- \$--- /PROPRO/)	I
CI	OMEGAO	OX ACENTRIC FACTOR	I
CI		(--- \$--- /PROPRO/)	I
CI	DRBANG	ANGLE BETWEEN THE EARTH-SUN VECTOR AND VEHICLE	I
CI		ORBITAL PLANE (KHXOPT=2)	I
CI		(DEG 0.0 \$TANKHX /INSLHX/)	I
CI	DXKFCT	NUMBER OF VELOCITY HEADS LOST IN OXIDIZER FEED	I
CI		LINE DUE TO BENDS, VALVES, ETC.	I
CI		(VEL-HEADS 5. \$LTANK /TANKS2/)	I
CI	DXNPSH	OXIDIZER PUMP NET POSITIVE SUCTION HEAD	I
CI		(FT --- \$--- /TPAOUT/)	I
CI	DXNPSP	OX NET POSITIVE SUCTION PRESSURE IN TANK	I
CI		(PSIA 10. \$PUMP /PRESCH/)	I
CI	DXOPEL	NUMBER OF OXIDIZER ORIFICES/ELEMENT	I
CI		(--- 1.5 \$INJECT /ELEMEN/)	I
CI	P	REGEN STATION LOCAL PRESSURE	I
CI		(PSIA --- \$--- /RGNSUM/)	I
CI	P1000N	NO AVAILABLE DEFINITION (/MOTOR/)	I
CI	PA	NO AVAILABLE DEFINITION (/PERF/)	I
CI	PAMB	AMBIENT PRESSURE CORRECTION FOR VARIABLE THRUST-	I
CI		TIME TRACE	I
CI		(PSIA 0.0 \$THVST /PERF/)	I
CI	PARAM	NO AVAILABLE DEFINITION (//EQ///)	I
CI	PARAM	NO AVAILABLE DEFINITION (/PURAM/)	I
CI	PARAML	NO AVAILABLE DEFINITION (//EQ///)	I
CI	PBASE	NO AVAILABLE DEFINITION (/PLUGCL/)	I
CI	PBINJF	FUEL PRESSURE AT PREBURNER INJECTOR INLET	I
CI		(PSIA --- \$--- /PRESCH/)	I
CI	PBINJO	OX PRESSURE AT PREBURNER INJECTOR INLET	I
CI		(PSIA --- \$--- /PRESCH/)	I
CI	PBPFL0	FUEL BOOST PUMP INLET PRESSURE	I
CI		(PSIA --- \$--- /PRESCH/)	I
CI	PBPOXO	OX BOOST PUMP INLET PRESSURE	I

Figure 5.1. Common Block Variables (Sheet 25 of 46)

CI	PBPRF	(PSIA --- \$---- /PRESCH/) FUEL PRESSURE RATIO ACROSS PREBURNER INJECTOR	I
CI	PBPRO	(PSIA 1.2 \$PUMP /PRESCH/) OX PRESSURE RATIO ACROSS PREBURNER INJECTOR	I
CI	PBURST	(PSIA 1.2 \$PUMP /PRESCH/) MINIMUM EXPECTED BURST PRESSURE	I
CI	PC	(LBF/IN**2 1200. \$FILMNT /MOTOR/) NOMINAL OPERATING CHAMBER PRESSURE	I
CI	PCAV	(LBF/IN**2 600. \$INPGEN ///EQ///) NO AVAILABLE DEFINITION (/MOTOR/)	I
CI	PCFACE	INJECTOR FACE PRESSURE	I
CI	PCISP1	(PSIA --- \$---- /LIQUID/) INTERMEDIATE CHAMBER PRESSURE ARRAY IN PERFORMANCE ROUTINES	I
CI	PCR	(--- --- \$---- /OPCOND/) REFERENCE CHAMBER PRESSURES AT WHICH CSTAR AND SPECIFIC IMPULSE DATA IS INPUT	I
CI	PCRIT	(LBF/IN**2 600. \$PROPEL /MOTOR/) CRITICAL PRESSURE OF COOLANT	I
CI	PCRITF	(PSIA 1731. \$LPROP /COOLNT/) FUEL CRITICAL PRESSURE	I
CI	PCRITO	(PSIA --- \$LFUEL /PROPRO/) OX CRITICAL PRESSURE	I
CI	PCTHRT	(PSIA --- \$LOXID /PROPRO/) CHAMBER PRESSURE FRACTIONS FOR THROTTLED OPERATION	I
CI	PEFBPF	(--- 1. \$THROT /THROTL/) NO AVAILABLE DEFINITION (/TPAOUT/)	I
CI	PEFBPO	NO AVAILABLE DEFINITION (/TPAOUT/)	I
CI	PEFFFL	FUEL PUMP EFFICIENCY	I
CI	PEFFL2	(--- --- \$---- /TPAOUT/) NO AVAILABLE DEFINITION (/TPOUT2/)	I
CI	PEFFOX	OXIDIZER PUMP EFFICIENCY	I
CI	PEFOX2	(--- --- \$---- /TPAOUT/) NO AVAILABLE DEFINITION (/TPOUT2/)	I
CI	PERIGE	NO AVAILABLE DEFINITION (///EQ///)	I
CI	PFLPIN	FUEL PUMP INLET PRESSURE	I
CI	PGAS	(PSIA --- \$---- /TPAOUT/) NO AVAILABLE DEFINITION (/TANKS/)	I
CI	PGMAX	PRESSURANT TANK MAXIMUM PRESSURE	I
CI	PI	(PSIA --- \$---- /TANKS/) NO AVAILABLE DEFINITION (/CONST/)	I
CI	PICG	MAX INITIAL PRESSURE OF COLD GAS BOTTLE	I
CI	PINJFL	(PSIA 4365. \$COLDG ///EQ///) FUEL INJECTOR INLET PRESSURE	I
CI	PINJOX	(PSIA --- \$---- /LIQUID/) OXIDIZER INJECTOR INLET PRESSURE	I
CI	PIO3	(PSIA --- \$---- /LIQUID/) NO AVAILABLE DEFINITION (/CONST/)	I
CI	PIO4	NO AVAILABLE DEFINITION (/CONST/)	I
CI	PIPKG	TEMPERATURE SENSITIVITY OF GAS GENERATOR OPERATING PRESSURE	I
CI	PLF	(1/DEGR 0.0036 \$SOLDGG /GASGEN/) VOLUMETRIC LOADING FRACTION FOR EACH STAGE BASED ON THE VOLUME INSIDE THE LINER, AND REDUCED BY THE SUBMERGED SECTION OF THE NOZZLE	I
CI	PLGODE	(--- .85 \$PROPEL ///EQ///) PLUG CLUSTER IDEAL ODE ISP	I
CI	PMFRAC	(SEC --- \$---- /PLUGCL/) STAGE PROPELLANT MASS FRACTION	I
CI		(--- --- \$---- ///EQ///)	I

Figure 5.1. Common Block Variables (Sheet 26 of 46)

CI	PNZREF	REFERENCE NOZZLE CHAMBER PRESSURE (PSIA 125. \$LIQENG /TCA/)	I
CI	POWRAT	NO AVAILABLE DEFINITION (/TPAOUT/)	I
CI	POXPIN	OXIDIZER PUMP INLET PRESSURE (PSIA --- \$--- /TPAOUT/)	I
CI	PPOWFL	NO AVAILABLE DEFINITION (/TPAOUT/)	I
CI	PPOWOX	NO AVAILABLE DEFINITION (/TPAOUT/)	I
CI	PPRPFL	FUEL PRESSURE IN TANK (PSIA --- \$--- /LIQUID/)	I
CI	PPRPOX	OXIDIZER PRESSURE IN TANK (PSIA --- \$--- /LIQUID/)	I
CI	PRATP	NO AVAILABLE DEFINITION (/TPAOUT/)	I
CI	PREF	PRESSURE AT WHICH REFERENCE PROPERTIES APPLY (PSIA 14.7 \$LPROP /COOLNT/)	I
CI	PREFFL	FUEL REFERENCE PRESSURE FOR REFERENCE PROPERTIES (PSIA --- \$--- \$FUEL /PROPRO/)	I
CI	PREFOX	OX REFERENCE PRESSURE FOR REFERENCE PROPERTIES (PSIA --- \$LOXID /PROPRO/)	I
CI	PREGFO	FUEL PRESSURE AT REGEN JACKET OUTLET (PSIA --- \$--- /PRESCH/)	I
CI	PREGOO	OX PRESSURE AT REGEN JACKET OUTLET (PSIA --- \$--- /PRESCH/)	I
CI	PREL	NO AVAILABLE DEFINITION (/TRAJ/)	I
CI	FRELLOS	IDEAL VELOCITY LOSSES DUE TO PRESSURE FORCES (FT/SEC 0 \$INTRAJ /TRAJ/)	I
CI	PRFCHM	REFERENCE CHAMBER PRESSURE FOR CHAMBER STRESS (PSIA 125. \$LIQENG /TCA/)	I
CI	PRFCHR	REFERENCE CHAMBER PRESSURE FOR CHAR DEPTH (PSIA 125. \$ABLATE /TCA/)	I
CI	PRGMLI	MLI PURGE GAS PRESSURE AT SPACE HOLD CONDITIONS (PSIA 2.0E-7 \$TANKHX /INSLHX/)	I
CI	PSTAGF	NO AVAILABLE DEFINITION (/TPOUT2/)	I
CI	PSTAGO	NO AVAILABLE DEFINITION (/TPOUT2/)	I
CI	PTANKS	NO AVAILABLE DEFINITION (/NCTIN/)	I
CI	PTEFL1	NO AVAILABLE DEFINITION (/TPOUT2/)	I
CI	PTEOX1	NO AVAILABLE DEFINITION (/TPOUT2/)	I
CI	PTURBI	TURBINE INLET PRESSURE (PSIA --- \$--- /PRESCH/)	I
CI	PTURBO	TURBINE OUTLET PRESSURE (PSIA --- \$PUMP /PRESCH/)	I
CI	PULLFL	FUEL TANK ULLAGE PRESSURE (PSIA --- \$--- /PRESCH/)	I
CI	PULLOX	OX TANK ULLAGE PRESSURE (PSIA --- \$--- /PRESCH/)	I
CI	PUMPHP	NO AVAILABLE DEFINITION (/TPAOUT/)	I
CI	PVENTF	FUEL TANK VENT PRESSURE (PSIA --- \$--- /INSLHX/)	I
CI	PVENTO	OXIDIZER TANK VENT PRESSURE (PSIA --- \$--- /INSLHX/)	I
CI	PVLVFL	FUEL VALVE INLET PRESSURE (PSIA --- \$--- /LIQUID/)	I
CI	PVLVFO	FUEL PRESSURE AT BIPROP VALVE OUTLET (PSIA --- \$--- /PRESCH/)	I
CI	PVLVOO	OX PRESSURE AT BIPROP VALVE OUTLET (PSIA --- \$--- /PRESCH/)	I
CI	PVLVOX	OXIDIZER VALVE INLET PRESSURE (PSIA --- \$--- /LIQUID/)	I
CI	PVMAXF	VAPOR PRESSURE OF FUEL AT TMAX (PSIA 3.6 \$LPROP /LIQUID/)	I
CI	PVMAXO	VAPOR PRESSURE OF OXIDIZER ST TMAX	I

Figure 5.1. Common Block Variables (Sheet 27 of 46)

CI	PVPLN	(PSIA 2.4 \$LPROP /LIQUID/) NATURAL LOGARITHM OF VAPOR PRESSURE ARRAY USED IN CALCULATING SATURATION TEMPERATURE OF COOLANT IN A REGENERATIVELY COOLED CHAMBER	I
CI	PVPLNF	(--- --- \$--- /CLAP/) NATURAL LOGARITHM OF VAPOR PRESSURE ARRAY USED IN CALCULATING SATURATION TEMPERATURE OF FUEL	I
CI	PVPLNO	(--- --- \$--- /CLAP/) NATURAL LOGARITHM OF VAPOR PRESSURE ARRAY USED IN CALCULATING SATURATION TEMPERATURE OF OX	I
CI	Q	(--- --- \$--- /CLAP/) NO AVAILABLE DEFINITION (/TRAJ/)	I
CI	QALPMX	NO AVAILABLE DEFINITION (/AERO/)	I
CI	QFL	FUEL PUMP VOLUMETRIC FLOW RATE (GPM --- \$--- /TPAOUT/)	I
CI	QFL2	NO AVAILABLE DEFINITION (/TPAOUT/)	I
CI	QMAXTR	MAXIMUM HEAT FLUX COOLED BY REGEN JACKET BEFORE TRANSPIRATION COOLING IS USED (BTU/IN**2/SEC 1.0 \$INREGN /TRANCO/)	I
CI	QOX	OXIDIZER PUMP VOLUMETRIC FLOW RATE (GPM --- \$--- /TPAOUT/)	I
CI	QOX2	NO AVAILABLE DEFINITION (/TPAOUT/)	I
CI	QRGN	REGEN STATION LOCAL HEAT FLUX (BTU/IN**2/SEC --- \$--- /RGNSUM/)	I
CI	QSTG	NO AVAILABLE DEFINITION (///EQ///)	I
CI	QTANKF	HEAT FLUX INTO FUEL TANK(S) (BTU/SEC --- \$--- /INSLHX/)	I
CI	QTANKO	HEAT FLUX INTO OXIDIZER TANK(S) (BTU/SEC --- \$--- /INSLHX/)	I
CI	QTURB	NO AVAILABLE DEFINITION (/TPOUT2/)	I
CI	QTURBF	NO AVAILABLE DEFINITION (/TPOUT2/)	I
CI	QTURBO	NO AVAILABLE DEFINITION (/TPOUT2/)	I
CI	QULTC1	CONSTANT IN NUCLEATE BOILING ULTIMATE HEAT FLUX EQUATION (BTU/IN**2/SEC 4.55 \$LPROP /COOLNT/)	I
CI	QULTC2	MULTIPLYING CONSTANT IN NUCLEATE BOILING HEAT FLUX EQUATION (BTU/IN**3/SEC 0.00686 \$LPROP /COOLNT/)	I
CI	RA	NO AVAILABLE DEFINITION (/SSCOM/)	I
CI	RADLOC	NO AVAILABLE DEFINITION (/NCTIN/)	I
CI	RADPIN	RADIATION SHIELDS PER INCH IN MULTILAYER INSULA- TION (MLI) (#/IN 40. \$TANKHX /INSLHX/)	I
CI	RANGE	NO AVAILABLE DEFINITION (/TRAJ/)	I
CI	RATANK	NO AVAILABLE DEFINITION (/NCTIN/)	I
CI	RATE	BURN RATE (MOTOR COND) (IN/SEC --- \$--- /MOTOR/)	I
CI	RATMLR	RATIO OF NOZZLE LENGTH TO THAT OF A MINIMUM LENGTH RAO NOZZLE (--- 1.177 \$LIQENG ///EQ///)	I
CI	RATTCH	NO AVAILABLE DEFINITION (/SSCOM/)	I
CI	RB1000	NO AVAILABLE DEFINITION (///EQ///)	I
CI	RBO	NO AVAILABLE DEFINITION (///EQ///)	I
CI	RCHAM	NO AVAILABLE DEFINITION (/NCTIN/)	I
CI	RCNOW	NO AVAILABLE DEFINITION (/MOTOR/)	I
CI	RCONI	NO AVAILABLE DEFINITION (/MOTOR/)	I
CI	RCRT	RATIO OF THROAT RADIUS OF CURVATURE TO THROAT RADIUS (--- 1.2 \$NOZZLE /MOTOR/)	I
CI	RDIM	NO AVAILABLE DEFINITION (/NCTIN/)	I

Figure 5.1. Common Block Variables (Sheet 28 of 46)

CI	RDPDG	NO AVAILABLE DEFINITION (/CONST/)
CI	REREARTH	NO AVAILABLE DEFINITION (/CONST/)
CI	REEXIT	NO AVAILABLE DEFINITION (///EQ///)
CI	REFNWT	REFERENCE NOZZLE WEIGHT (LBM 1000. \$PROPEL /MOTOR/)
CI	REFSTF	FUEL REFERENCE SURFACE TENSION (LB/IN --- \$LFUEL /PROPRO/)
CI	REFSTO	OX REFERENCE SURFACE TENSION (LB/IN --- \$LOXID /PROPRO/)
CI	REFWDT	REFERENCE NOZZLE FLOW RATE (LBM/SEC 100. \$PROPEL /MOTOR/)
CI	REGA	THROAT REGRESSION COEFFICIENT (--- 0.002798 \$ABLATE /LIQUID/)
CI	REGB	THROAT REGRESSION COEFFICIENT (--- 0.0005995 \$ABLATE /LIQUID/)
CI	REGC	THROAT REGRESSION COEFFICIENT (--- 0.4246 \$ABLATE /LIQUID/)
CI	RELHUM	RELATIVE HUMIDITY OF AMBIENT ATMOSPHERE FOR USE WITH KHXOPT=3 (--- 50. \$TANKHX /INSLHX/)
CI	REPLUG	PLUG CLUSTER EXIT RADIUS (IN --- \$--- /PLUGCL/)
CI	RESIDA	AFT TANK RESIDUAL PROPELLANT WEIGHT (LBM --- \$--- /TANKS/)
CI	RESIDF	FORWARD TANK RESIDUAL PROPELLANT WEIGHT (LBM --- \$--- /TANKS/)
CI	REXIT	NOZZLE EXIT RADIUS (IN --- \$--- ///EQ///)
CI	RF	RADIUS OF FORWARD DOME POLAR BOSS OPENING (IN 2. \$FILMNT /MOTOR/)
CI	RGIMB	NO AVAILABLE DEFINITION (/GIMBAL/)
CI	RHBNDAA	DENSITY OF AFT BLADDER BOND MATERIAL (LBM/IN**3 0.04 \$--- /TANKS/)
CI	RHBNDFF	DENSITY OF FORWARD BLADDER BOND MATERIAL (LBM/IN**3 0.04 \$--- /TANKS/)
CI	RHCABL	DENSITY OF CHAMBER ABLATIVE MATERIAL (LBM/IN**3 0.0632 \$LIQMAT /TCA/)
CI	RHCSTR	DENSITY OF CHAMBER STRUCTURAL MATERIAL (LBM/IN**3 0.0632 \$LIQMAT /TCA/)
CI	RHO	MATERIAL DENSITY TABLE (LBM/IN**3 0.29, 0.16, 8*0.0 \$LIQMAT /MTPROP/)
CI	RHOABP	BAND DENSITY (ENDS/IN/PLY 35. \$FILMNT /MOTOR/)
CI	RHOALF	DENSITY OF HELICAL WINDINGS (LBM/IN**3 0.042 \$FILMNT /MOTOR/)
CI	RHOATM	NO AVAILABLE DEFINITION (/ATMOS/)
CI	RHOBOT	START BOTTLE MATERIAL DENSITY (ISTART=2) (LBM/IN**3 0.16 \$PUMP /TPAIN/)
CI	RHOCAS	CASE MATERIAL DENSITY (LBM/IN**3 .282 \$MATER /MOTOR/)
CI	RHOCLS	REGEN CHAMBER CLOSEOUT MATERIAL DENSITY (LBM/IN**3 0.322 \$LIQMAT /WTREGN/)
CI	RHOCYL	START CYLINDER MATERIAL DENSITY (ISTART=2) (LBM/IN**3 0.3 \$PUMP /TPAIN/)
CI	RHOEXF	NO AVAILABLE DEFINITION (/TPOUT2/)
CI	RHOEXH	NO AVAILABLE DEFINITION (/TPOUT2/)
CI	RHOEXO	NO AVAILABLE DEFINITION (/TPOUT2/)
CI	RHOEXT	DENSITY OF EXTERNAL INSULATION (LBM/IN**3 .06 \$MATER /MOTOR/)
CI	RHOGG	SOLID GRAIN DENSITY

Figure 5.1. Common Block Variables (Sheet 29 of 46)

CI	RHOGW	(LB/IN**3 0.056 \$SOLDGG /GASGEN/) REGEN CHAMBER GAS WALL MATERIAL DENSITY	I
CI	RHOINJ	(LBM/IN**3 0.28 \$LIQMAT /WTREGN/) INJECTOR MATERIAL DENSITY	I
CI	RHOINS	(LBM/IN**3 0.098 \$LIQMAT /TCA/) DENSITY OF INTERNAL INSULATION	I
CI	RHOINT	(LBM/IN**3 .0414 \$MATER /MOTOR/) DENSITY OF INTERSTAGE MATERIAL	I
CI	RHOLNR	(LBM/IN**3 .101 \$INTSTG /MOTOR/) LINER DENSITY	I
CI	RHONDZ	(LBM/IN**3 .0414 \$MATER /MOTOR/) DENSITY OF NOZZLE EXIT CONE	I
CI	RHONZE	(LBM/IN**3 .06 \$NOZZLE /GENRL/) NO AVAILABLE DEFINITION (/TCA/)	I
CI	RHOP	PROPELLANT DENSITY FOR EACH STAGE	I
CI	RHOPLB	(LBM/IN**3 0. *PROPEL /MOTOR/) PLUG CLUSTER BASE DENSITY (IPLUG = 1)	I
CI	RHOSPH	(LBM/IN**3 0.06 \$LIQMAT /PLGBAS/) START SYSTEM SPHERE MATERIAL DENSITY (ISTART=1)	I
CI	RHOTFL	(LB/IN**3 0.1 \$PUMP /TPAIN/) FUEL TURBINE BLADE MATERIAL DENSITY (JCNFIG=3 OR 4)	I
CI	RHOOTH	(LBM/IN**3 0.3 \$PUMP /TPAIN/) DENSITY OF HOOP WINDINGS	I
CI	RHOТОX	(LBM/IN**3 0.042 \$FILMNT /MOTOR/) DX TURBINE BLADE MATERIAL DENSITY (JCNFIG=3 OR 4)	I
CI	RHOTPA	(LBM/IN**3 0.3 \$PUMP /TPAIN/) TPA EFFECTIVE DENSITY	I
CI	RHOTUR	(LBM/IN**3 0.3 \$PUMP /TPAIN/) TURBINE BLADE MATERIAL DENSITY (JCNFIG=1 OR 2)	I
CI	RHOVLY	(LBM/IN**3 0.3 \$PUMP /TPAIN/) VALVE MATERIAL DENSITY	I
CI	RHPTIN	(LBM/IN**3 0.098 \$LIQMAT /TCA/) DENSITY OF TANK INSULATION	I
CI	RHTRIN	(LBM/IN**3 0.04 \$LIQMAT /TANKS/) MATERIAL DENSITY OF TRANSPERSION COOLING THROAT INSERT	I
CI	RINTNK	(LBM/IN**3 0.28 \$LIQMAT /TRANCO/) NO AVAILABLE DEFINITION (/NCTOUT/)	I
CI	RLNR12	NO AVAILABLE DEFINITION (/MOTOR/)	I
CI	RMFFL	FUEL DROPLET RADIUS CORRECTION FACTOR	I
CI	RMFOX	(--- 0.33 \$LQPERF /LIQUID/) OXIDIZER DROPLET RADIUS CORRECTION FACTOR	I
CI	RMOTOR	NO AVAILABLE DEFINITION (/NCTIN/)	I
CI	RNGBO	NO AVAILABLE DEFINITION (//EQ//)	I
CI	RNGIMP	NO AVAILABLE DEFINITION (//EQ//)	I
CI	RNCNM	NO AVAILABLE DEFINITION (//EQ//)	I
CI	RNGRE	NO AVAILABLE DEFINITION (//EQ//)	I
CI	RNGSTG	NO AVAILABLE DEFINITION (/TRAJ/)	I
CI	RNZEXT	NO AVAILABLE DEFINITION (/NCTIN/)	I
CI	RNZREF	REFERENCE NOZZLE THROAT RADIUS	I
CI	ROACVL	(IN 3.74 \$LIGENG /TCA/) ACCUMULATOR VALVE MATERIAL DENSITY (ISTART=2)	I
CI	ROCART	(LB/IN**3 0.3 \$PUMP /TPAIN/) START CARTRIDGE MATERIAL DENSITY (ISTART=3)	I
CI	ROGRAN	(LBM/IN**3 0.3 \$PUMP /TPAIN/) START CARTRIDGE GRAIN DENSITY (ISTART=3)	I
CI	ROINGG	(LBM/IN**3 0.07 \$PUMP /TPAIN/) GAS GENERATOR OR PRE-BURNER INJECTOR MATERIAL DENSITY	I

Figure 5.1. Common Block Variables (Sheet 30 of 46)

CI		(LBM/IN**3 0.3 \$PUMP /TPAIN/)	I
CI	ROLINE	PROPELLANT LINE MATERIAL DENSITY(ENGINE BAY LINES)	I
CI		(LB/IN**3 0.3 \$PUMP /TPAIN/)	I
CI	ROOTNZ	NO AVAILABLE DEFINITION (/MOTOR/)	I
CI	ROSPVL	DENSITY OF COLD GAS VALVE MATERIAL (ISTART=1)	I
CI		(LBM/IN**3 0.3 \$PUMP /TPAIN/)	I
CI	ROSTAK	HOT GAS DUCT MATERIAL DENSITY	I
CI		(LBM/IN**3 0.3 \$PUMP /TPAIN/)	I
CI	ROTRNZ	DENSITY OF TRANSLATING NOZZLE MATERIAL	I
CI		(LB/IN**3 0.28 \$LIQMAT /TRANOZ/)	I
CI	ROUTNK	NO AVAILABLE DEFINITION (/NCTOUT/)	I
CI	RPM	SINGLE SHAFT TPA SPEED OF ROTATION	I
CI		(RPM --- \$--- /TPAOUT/)	I
CI	RPMBPF	NO AVAILABLE DEFINITION (/TPAOUT/)	I
CI	RPMBPO	NO AVAILABLE DEFINITION (/TPAOUT/)	I
CI	RPMBRS	NO AVAILABLE DEFINITION (/TPAOUT/)	I
CI	RPML	NO AVAILABLE DEFINITION (/TPAOUT/)	I
CI	RPMOX	NO AVAILABLE DEFINITION (/TPAOUT/)	I
CI	RPMSFL	NO AVAILABLE DEFINITION (/TPAOUT/)	I
CI	RPMSOX	NO AVAILABLE DEFINITION (/TPAOUT/)	I
CI	RPMTFL	NO AVAILABLE DEFINITION (/TPAOUT/)	I
CI	RPMTOX	NO AVAILABLE DEFINITION (/TPAOUT/)	I
CI	RPMTUR	NO AVAILABLE DEFINITION (/TPAOUT/)	I
CI	RRFCHM	REFERENCE CHAMBER RADIUS FOR TCA WEIGHT	I
CI		(IN 5.95 \$LIQENG /TCA/)	I
CI	RTCORR	KINETIC LOSS THROAT CORRECTION FACTOR	I
CI		(--- --- \$--- /OPCOND/)	I
CI	RTHRT	CHAMBER THROAT RADIUS	I
CI		(IN --- \$--- //EQ///)	I
CI	RTOT	NO AVAILABLE DEFINITION (/TRAJ/)	I
CI	RTRATT	RADIUS OF NOZZLE AT ATTACH POINT OF TRANSLATING NOZZLE	I
CI		(IN --- \$--- /TRANOZ/)	I
CI	RUFFFL	ABSOLUTE SURFACE ROUGHNESS OF FUEL FEED LINE	I
CI		(IN .0001 \$LTANK /TANKS2/)	I
CI	RUFFOX	ABSOLUTE SURFACE ROUGHNESS OF OXIDIZER FEED LINE	I
CI		(IN .0001 \$LTANK /TANKS2/)	I
CI	SABSOR	STAGE ABSORBTIVITY (KHXOPT=2)	I
CI		(--- 0.2 \$TANKHX /INSLHX/)	I
CI	SACCEL	AVERAGE STAGE ACCELERATION (FOR TANK HEAT LOSS)	I
CI		(G'S 2.0 \$TANKHX /INSLHX/)	I
CI	SAFACT	CASE DESIGN SAFETY FACTOR	I
CI		(--- 1.5 \$MATER /MOTOR/)	I
CI	SALFT	NO AVAILABLE DEFINITION (/MOTOR/)	I
CI	SALPH	NO AVAILABLE DEFINITION (/TRAJ/)	I
CI	SAMULT	SURFACE AREA MULTIPLIER ON REGEN COOLED ENGINE	I
CI		(--- 1.0 \$INREGN /WTREGN/)	I
CI	SCASE	DESIGN STRENGTH OF CASE MATERIAL (HOOP)	I
CI		(LBF/IN**2 220000. \$MATER /MOTOR/)	I
CI	SCHIP	NO AVAILABLE DEFINITION (/TRAJ/)	I
CI	SCHIR	NO AVAILABLE DEFINITION (/TRAJ/)	I
CI	SCREEN	NO AVAILABLE DEFINITION (/PSUTK2/)	I
CI	SDOMEH	DOME HOOP DESIGN STRENGTH	I
CI		(LBF/IN**2 220000. \$MATER /MOTOR/)	I
CI	SDOMEM	DOME MERIDIONAL STRENGTH	I
CI		(LBF/IN**2 220000. \$MATER /MOTOR/)	I
CI	SEMISI	STAGE EMMISIVITY (KHXOPT=2)	I
CI		(--- 0.9 \$TANKHX /INSLHX/)	I
CI	SEPRNG	NO AVAILABLE DEFINITION (//EQ///)	I
CI	SFABL	ABLATIVE THICKNESS SAFETY FACTOR	I

Figure 5.1. Common Block Variables (Sheet 31 of 46)

CI	SFC	(--- 1. \$ABLATE /TCA/) AERODYNAMIC SKIN FRICTION COEFFICIENTS INPUT AS FUNCTIONS OF MACH NUMBER AND ALTITUDE; SFC(I,J) CORRESPONDS TO AMACH(I) AND ALTSF(J)	I
CI	SFCHM	(--- 0. \$AEROD /AERO/) CHAMBER STRUCTURAL SAFETY FACTOR	I
CI	SFFLTK	(--- 1. \$LIQENG /TCA/) SAFETY FACTOR FOR FUEL TANK	I
CI	SFINST	(--- 1.25 \$LIQMAT /TWTMLT/) DESIGN SAFETY FACTOR FOR INTERSTAGE THICKNESS SIZING	I
CI	SFLINE	(---- 1.5 \$INTSTG /MOTOR/) SAFETY FACTOR FOR PROPELLANT AND PRESSURIZATION LINES	I
CI	SFOXTK	(---- 2.0 \$LIQMAT /TWTMLT/) SAFETY FACTOR FOR OXIDIZER TANK	I
CI	SFRPTK	(---- 1.25 \$LIQMAT /TWTMLT/) SAFETY FACTOR FOR PRESSURE TANK	I
CI	SFSTRC	(---- 1.5 \$LIQMAT /TWTMLT/) SAFETY FACTOR FOR STRUCTURAL WALL OF STAGE	I
CI	SFTNKS	(---- 1.25 \$LIQMAT /TWTMLT/) NO AVAILABLE DEFINITION (/NCTIN/)	I
CI	SGAMA	(---- 1.25 \$LIQMAT /TWTMLT/) NO AVAILABLE DEFINITION (/TRAJ/)	I
CI	SIGCHM	HOT CHAMBER DESIGN STRENGTH (PSI 25000. \$LIQMAT /TCA/)	I
CI	SIGCLS	DESIGN STRESS OF REGEN JACKET CLOSEOUT MATERIAL (PSIA 25000 \$LIQMAT /TCA/)	I
CI	SIGGG	BURN RATE TEMPERATURE SENSITIVITY OF SOLID GRAIN (1/DEGR 0.0013 \$SOLDGG /GASGEN/)	I
CI	SIGINJ	INJECTOR MATERIAL DESIGN STRESS (PSI 25000. \$LIQMAT /TCA/)	I
CI	SIGMAX	MATERIAL DESIGN STRESS TABLE (NOT INCLUDING SAFETY FACTORS)	I
CI	SIGNZE	(PSI 112300., 130000., 8*0. \$LIQMAT /MTPROP/) DESIGN STRESS OF NOZZLE EXTENSION MATERIAL	I
CI	SINST	(PSIA 25000 \$LIQMAT /TCA/) DESIGN STRENGTH OF INTERSTAGE MATERIAL	I
CI	SMASS	(LBF/IN**2 220000. \$INTSTG /MOTOR/) STAGE MASS RATIO	I
CI	SOFIA	(--- --- \$--- /SSCOM/) CONSTANT IN SOFI THERMAL CONDUCTIVITY EQUATION K = SOFIA + SOFIB * TEMPERATURE	I
CI	SOFIB	(BTU/IN-SEC-DEGR 3.935E-8 \$TANKHX /INSLHX/) CONSTANT IN SOFI THERMAL CONDUCTIVITY EQUATION K = SOFIA + SOFIB * TEMPERATURE	I
CI	SOLCON	(BTU/IN-SEC-DEGR**2 5.676E-10 \$TANKHX /INSLHX/) SOLAR HEAT FLUX (KHXOPT=2)	I
CI	SPCNOZ	(BTU/SEC-IN**2 8.28E-4 \$TANKHX /INSLHX/) SPACE BETWEEN ADJACENT NOZZLES	I
CI	SPHEAT	(IN 1.0 \$LIQENG /GIMBAL/) MATERIAL SPECIFIC HEAT TABLE	I
CI	SPRMX	(BTU/LB-DEGR .12, .13, 8*0. \$LIQMAT /MTPROP/) MAXIMUM ISP FOR USER PROPELLANT AT PC=500 AREA RATIO=20 (IPROP=0)	I
CI	SPSMMX	(SEC 328.8 \$LPROP /EQUIVR/) ISP OF LIBRARY PROPELLANT AT MAX ISP FOR PC=500 AND E=20	I
CI	SSBPFL	(--- --- \$--- /EQUIVR/) NO AVAILABLE DEFINITION (/TPAOUT/)	I
CI	SSBPOX	(--- --- \$--- /EQUIVR/) NO AVAILABLE DEFINITION (/TPAOUT/)	I

Figure 5.1. Common Block Variables (Sheet 32 of 46)

CI	SSFL	FUEL PUMP SPECIFIC SPEED (--- \$--- /TPAOUT/)	I
CI	SSFL2	NO AVAILABLE DEFINITION (/TPAOUT/)	I
CI	SSHEAR	NO AVAILABLE DEFINITION (/MOTOR/)	I
CI	SSMIN	MINIMUM SPECIFIC SPEED ALLOWED IN PUMPS (--- BOO. \$PUMP ///EQ///)	I
CI	SSOX	OXIDIZER PUMP SPECIFIC SPEED (--- \$--- /TPAOUT/)	I
CI	SSOX2	NO AVAILABLE DEFINITION (/TPAOUT/)	I
CI	SSSBPF	MAXIMUM SUCTION SPECIFIC SPEED OF FUEL BOOST PUMP (RPM-GPM-FT 30000-OR-40000 \$PUMP /TPAIN/)	I
CI	SSSBPO	MAXIMUM SUCTION SPECIFIC SPEED OF OX BOOST PUMP (RPM-GPM-FT 30000 \$PUMP /TPAIN/)	I
CI	SSSFL	MAXIMUM SUCTION SPECIFIC SPEED OF FUEL PUMP (RPM-GPM-FT 20000 \$PUMP /TPAIN/)	I
CI	SSSMAX	MAXIMUM SUCTION SPECIFIC SPEED ALLOWED IN PUMPS (--- 20000. \$PUMP ///EQ///)	I
CI	SSSOX	MAXIMUM SUCTION SPECIFIC SPEED OF OXIDIZER PUMP (RPM-GPM-FT 20000 \$PUMP /TPAIN/)	I
CI	SSTRFL	NO AVAILABLE DEFINITION (/TPOUT2/)	I
CI	SSTROX	NO AVAILABLE DEFINITION (/TPOUT2/)	I
CI	SSTURB	NO AVAILABLE DEFINITION (/TPOUT2/)	I
CI	STGIMP	NO AVAILABLE DEFINITION (///EQ///)	I
CI	SYBOT	START BOTTLE YIELD STRENGTH (ISTART=2) (PSI 75000 \$PUMP /TPAIN/)	I
CI	SYCART	YIELD STRENGTH FOR START CARTRIDGE (ISTART=3) (PSI 100000 \$PUMP /TPAIN/)	I
CI	SYCYL	START CYLINDER YIELD STRENGTH (ISTART=2) (PSI 30000 \$PUMP /TPAIN/)	I
CI	SYDUCT	HOT GAS DUCT MATERIAL YEILD STRENGTH (PSI 30000 \$PUMP /TPAIN/)	I
CI	SYINGG	GAS GENERATOR OR PRE-BURNER INJECTOR YIELD STRENGTH (PSI 30000 \$PUMP /TPAIN/)	I
CI	SYLIN	PROPELLANT LINE YIELD STRENGTH (ENGINE BAY LINES) (PSI 30000 \$PUMP /TPAIN/)	I
CI	SYSPH	START SYSTEM SPHERE YIELD STRENGTH (ISTART=1) (PSI 47000 \$PUMP /TPAIN/)	I
CI	TALFT	NO AVAILABLE DEFINITION (/MOTOR/)	I
CI	TALFT2	NO AVAILABLE DEFINITION (/MOTOR/)	I
CI	TAMICE	AMBIENT TEMPERATURE FOR GROUND HOLD ICE HEAT TRANSFER CALCULATION (KHXOPT=3) (DEGR 560 \$TANKHX /INSLHX/)	I
CI	TAMRAD	AMBIENT TEMPERATURE FOR TCA RADIATION COOLING (DEGR 560 \$LIQENG /COOLNT/)	I
CI	TANGLE	NO AVAILABLE DEFINITION (/NCTIN/)	I
CI	TAUWEB	WEB INSULATION THICKNESS (IN --- \$--- ///EQ///)	I
CI	TB	CHAMBER BARRIER TEMPERATURE (DEGR --- \$--- /LIQUID/)	I
CI	TBKCS	NO AVAILABLE DEFINITION (/MOTOR/)	I
CI	TBKIST	NO AVAILABLE DEFINITION (/MOTOR/)	I
CI	TBLDFL	FUEL TANK BLADDER THICKNESS (IN .025 \$BLADER /TANKS2/)	I
CI	TBLDOX	OXIDIZER TANK BLADDER THICKNESS (IN .025 \$BLADER /TANKS2/)	I
CI	TBNDFL	FUEL TANK BOND THICKNESS (IN .04 \$BLADER /TANKS2/)	I
CI	TBNDGX	OXIDIZER TANK BOND THICKNESS (IN .04 \$BLADER /TANKS2/)	I

Figure 5.1. Common Block Variables (Sheet 33 of 46)

CI	TB0GAS	START BOTTLE GAS TEMPERATURE (ISTART=2) (DEGR 530 \$PUMP /TPAIN/)	I
CI	TBOGG	TEMPERATURE OF SOLID GAS GENERATOR PRESSURANT AT BURNOUT (DEGF ---- \$---- /GASGEN/)	I
CI	TBOIL	NORMAL BOILING POINT OF COOLANT (DEGR 618. \$LPROP /COOLNT/)	I
CI	TBOILF	FUEL NORMAL BOILING POINT (DEGR --- \$LFUEL /PROPRO/)	I
CI	TBOILO	OX NORMAL BOILING POINT (DEGR --- \$LOXID /PROPRO/)	I
CI	TBONDA	THICKNESS OF AFT TANK BOND MATERIAL (KBLAT=2-5) (IN 0.04 \$--- /TANKS/)	I
CI	TBONDF	THICKNESS OF FORWARD TANK BOND MATERIAL (KBLFT = 2-5) (IN 0.04 \$--- /TANKS/)	I
CI	TBPFL0	FUEL TEMPERATURE AT BOOST PUMP OUTLET (DEGR --- \$--- /TEMSCH/)	I
CI	TBPOX0	OX TEMPERATURE AT BOOST PUMP OUTLET (DEGR --- \$--- /TEMSCH/)	I
CI	TBR	REGEN STATION COOLANT BULK TEMPERATURE (DEGR --- \$--- /RGNSUM/)	I
CI	TBRCHR	REFERENCE BURN TIME FOR CHAR DEPTH (SEC 500. \$ABLATE /TCA/)	I
CI	TBRN	TABLE OF MOTOR BURN TIMES; INPUT FOR EACH STAGE (SEC 0.0 \$THVST /PERF/)	I
CI	TBUCKL	NO AVAILABLE DEFINITION (/SSCOM/)	I
CI	TBURN	STAGE BURN TIME (SEC --- \$--- /LSCOM/)	I
CI	TC	CHAMBER CORE COMBUSTION TEMPERATURE (DEGR --- \$--- /LIQUID/)	I
CI	TCASE	CASE THICKNESS (IN --- \$--- /MOTOR/)	I
CI	TCHAM	IDEAL EQUILIBRIUM CHAMBER TEMPERATURE DATA ARRAY (--- --- \$--- /OPCOND/)	I
CI	TCHMAB	ABLATIVE THICKNESS IN CHAMBER (IN --- \$--- /TCA/)	I
CI	TCHMST	CHAMBER STRUCTURAL THICKNESS (IN --- \$--- /TCA/)	I
CI	TCMBGG	GAS GENERATOR COMBUSTION TEMPERATURE (DEGR 2130. \$SOLDGG /GASGEN/)	I
CI	TCONE	THICKNESS OF NOZZLE EXIT CONE (IN 0.0 \$NOZZLE /MOTOR/)	I
CI	TCRIT	CRITICAL TEMPERATURE OF COOLANT (DEGR 1093. \$LPROP /COOLNT/)	I
CI	TCRITF	FUEL CRITICAL TEMPERATURE (DEGR --- \$LFUEL /PROPRO/)	I
CI	TCRITO	OX CRITICAL TEMPERATURE (DEGR --- \$LOXID /PROPRO/)	I
CI	TCW	REGEN STATION LOCAL COOLANT WALL TEMPERATURE (DEGR --- \$--- /RGNSUM/)	I
CI	TDCYGG	TEMPERATURE DECAY TIME CONSTANT (SEC 100. \$SOLDGG /GASGEN/)	I
CI	TDESTR	DESIGN TEMPERATURE OF TRANSPERSION COOLED WALL MATERIAL (DEGR 2000 \$INREGN /TRANCO/)	I
CI	TDOME	DOME THICKNESS (IN --- \$--- /MOTOR/)	I
CI	TEKCH	NO AVAILABLE DEFINITION (/PSUTK2/)	I
CI	TEKXMN	NO AVAILABLE DEFINITION (/PSUTEK/)	I

Figure 5.1. Common Block Variables (Sheet 34 of 46)

CI	TEKXMX	NO AVAILABLE DEFINITION (/PSUTEK/)	I
CI	TEKXP	NO AVAILABLE DEFINITION (/PSUTEK/)	I
CI	TEKYMN	NO AVAILABLE DEFINITION (/PSUTEK/)	I
CI	TEKYMX	NO AVAILABLE DEFINITION (/PSUTEK/)	I
CI	TEKYP	NO AVAILABLE DEFINITION (/PSUTEK/)	I
CI	TENTTR	AVERAGE TEMPERATURE RISE OF TRANSPERSION COOLANT UP TO THE INJECTION POINT (DEGR ---- \$---- /TRANCO/)	I
CI	TEXBOU	EXTERNAL BOUNDARY TEMPERATURE (KHXOPT=1) (DEGR 560. \$TANKHX /INSLHX/)	I
CI	TF1	TEMPERATURE OF COLD GAS PRESSURANT IN TANK 1 AFTER EXPANSION (DEGF ---- \$---- /COLDGP/)	I
CI	TF2	TEMPERATURE OF COLD GAS PRESSURANT IN TANK 2 AFTER EXPANSION (DEGF ---- \$---- /COLDGP/)	I
CI	TFACFL	FUEL TEMPERATURE AT TCA INJECTOR FACE (DEGR ---- \$---- /TEMSCH/)	I
CI	TFACOX	OX TEMPERATURE AT TCA INJECTOR FACE (DEGR ---- \$---- /TEMSCH/)	I
CI	TFB	TEMPERATURE OF COLD GAS PRESSURANT IN PRESSURE TANK AFTER EXPANSION INTO PROPELLANT TANKS (DEGF ---- \$---- /COLDGP/)	I
CI	TFLPIN	FUEL TEMPERATURE AT PUMP INLET (DEGR ---- \$---- /TEMSCH/)	I
CI	TGAS	REGEN STATION LOCAL COMBUSTION GAS TEMPERATURE (DEGR ---- \$---- /RGNSUM/)	I
CI	TGEDH	PLATELET THICKNESS OF TRANSPERSION COOLED SECTION (IN .08 \$INREGN /TRANCO/)	I
CI	TGEOL	PLATELET LAND THICKNESS OF TRANSPERSION COOLED SECTION (IN .1 \$INREGN /TRANCO/)	I
CI	TGEOS	SEPARATOR PLATELET THICKNESS IN TRANSPIRATION COOLED SECTION (IN .04 \$INREGN /TRANCO/)	I
CI	TGEOW	PLATELET FLOW PASSAGE WIDTHS IN TRANSPIRATION COOLED SECTION (IN .14 \$INREGN /TRANCO/)	I
CI	TGW	REGEN STATION LOCAL GAS WALL TEMPERATURE (DEGR ---- \$---- /RGNSUM/)	I
CI	TGWNOM	NOMINAL GAS WALL TEMPERATURE (NOT TO BE EXCEEDED) (DEGR 2000. \$INREGN /COOLNT/)	I
CI	THATHD	AFT TANK DOME THICKNESS (IN ---- \$---- /TANKS/)	I
CI	THFTHD	FORWARD TANK DOME THICKNESS (IN ---- \$---- /TANKS/)	I
CI	THIKNS	NO AVAILABLE DEFINITION (/SSCOM/)	I
CI	THKBLA	AFT BLADDER MATERIAL THICKNESS (KBLAT = 1) (IN 0.025 \$---- /TANKS/)	I
CI	THKBLF	FORWARD BLADDER MATERIAL THICKNESS (KBLFT = 1) (IN 0.025 \$---- /TANKS/)	I
CI	THKCYL	NO AVAILABLE DEFINITION (/NCTOUT/)	I
CI	THKEND	NO AVAILABLE DEFINITION (/NCTOUT/)	I
CI	THPTCH	PRESSURE TANK COMMON HEAD THICKNESS (IN ---- \$---- /TANKS/)	I
CI	THPTHD	PRESSURE TANK DOME THICKNESS (IN ---- \$---- /TANKS/)	I
CI	THRPC	TABLE OF CHAMBER PRESSURE FRACTIONS FOR CORRESPONDING VALUES OF ERETHR AND ECFTHR (--- ---- \$THROT /THREFF/)	I

Figure 5.1. Common Block Variables (Sheet 35 of 46)

CI	TEKXMX	NO AVAILABLE DEFINITION (/PSUTEK/)	I
CI	TEKXP	NO AVAILABLE DEFINITION (/PSUTEK/)	I
CI	TEKYMN	NO AVAILABLE DEFINITION (/PSUTEK/)	I
CI	TEKYMX	NO AVAILABLE DEFINITION (/PSUTEK/)	I
CI	TEKYP	NO AVAILABLE DEFINITION (/PSUTEK/)	I
CI	TENTTR	AVERAGE TEMPERATURE RISE OF TRANSPIRATION COOLANT UP TO THE INJECTION POINT (DEGR --- \$--- /TRANCO/)	I
CI	TEXBOU	EXTERNAL BOUNDARY TEMPERATURE (KHXOPT=1) (DEGR 560. \$TANKHX /INSLHX/)	I
CI	TF1	TEMPERATURE OF COLD GAS PRESSURANT IN TANK 1 AFTER EXPANSION (DEGF --- \$--- /COLDGP/)	I
CI	TF2	TEMPERATURE OF COLD GAS PRESSURANT IN TANK 2 AFTER EXPANSION (DEGF --- \$--- /COLDGP/)	I
CI	TFACFL	FUEL TEMPERATURE AT TCA INJECTOR FACE (DEGR --- \$--- /TEMSCH/)	I
CI	TFACOX	OX TEMPERATURE AT TCA INJECTOR FACE (DEGR --- \$--- /TEMSCH/)	I
CI	TFB	TEMPERATURE OF COLD GAS PRESSURANT IN PRESSURE TANK AFTER EXPANSION INTO PROPELLANT TANKS (DEGF --- \$--- /COLDGP/)	I
CI	TFLPIN	FUEL TEMPERATURE AT PUMP INLET (DEGR --- \$--- /TEMSCH/)	I
CI	TGAS	REGEN STATION LOCAL COMBUSTION GAS TEMPERATURE (DEGR --- \$--- /RGNSUM/)	I
CI	TGE0H	PLATELET THICKNESS OF TRANSPIRATION COOLED SECTION (IN .08 \$INREGN /TRANCO/)	I
CI	TGE0L	PLATELET LAND THICKNESS OF TRANSPIRATION COOLED SECTION (IN .1 \$INREGN /TRANCO/)	I
CI	TGE0S	SEPARATOR PLATELET THICKNESS IN TRANSPIRATION COOLED SECTION (IN .04 \$INREGN /TRANCO/)	I
CI	TGE0W	PLATELET FLOW PASSAGE WIDTHS IN TRANSPIRATION COOLED SECTION (IN .14 \$INREGN /TRANCO/)	I
CI	TGW	REGEN STATION LOCAL GAS WALL TEMPERATURE (DEGR --- \$--- /RGNSUM/)	I
CI	TGWNOM	NOMINAL GAS WALL TEMPERATURE (NOT TO BE EXCEEDED) (DEGR 2000. \$INREGN /COOLNT/)	I
CI	THATHD	AFT TANK DOME THICKNESS (IN --- \$--- /TANKS/)	I
CI	THFTHD	FORWARD TANK DOME THICKNESS (IN --- \$--- /TANKS/)	I
CI	THIKNS	NO AVAILABLE DEFINITION (/SSCOM/)	I
CI	THKBLA	AFT BLADDER MATERIAL THICKNESS (KBLAT = 1) (IN 0.025 \$--- /TANKS/)	I
CI	THKBLF	FORWARD BLADDER MATERIAL THICKNESS (KBLFT = 1) (IN 0.025 \$--- /TANKS/)	I
CI	THKCYL	NO AVAILABLE DEFINITION (/NCTOUT/)	I
CI	THKEND	NO AVAILABLE DEFINITION (/NCTOUT/)	I
CI	THPTCH	PRESSURE TANK COMMON HEAD THICKNESS (IN --- \$--- /TANKS/)	I
CI	THPTHD	PRESSURE TANK DOME THICKNESS (IN --- \$--- /TANKS/)	I
CI	THR0C	TABLE OF CHAMBER PRESSURE FRACTIONS FOR CORRE- SPONDING VALUES OF ERETHR AND ECFTHR (--- --- \$THROT /THREFF/)	I

Figure 5.1. Common Block Variables (Sheet 35 of 46)

CI	THRVC	VACUUM DELIVERED THRUST (LBF ---- \$---- /SSCOM/)	I
CI	TIMPCG	TIME AT WHICH POLYTROPIC GAMMA EQUALS 1.1 (SEC 240. \$COLDG /COLDGP/)	I
CI	TIMTHR	TIME INTERVALS FOR ENGINE THROTTLING (SEC 0.0 \$THROT /THROTL/)	I
CI	TINADM	INSULATION THICKNESS IN AFT DOME SECTION (IN 0. \$MATER /MOTOR/)	I
CI	TINFDM	INSULATION THICKNESS IN FORWARD DOME SECTION (IN 0. \$MATER /MOTOR/)	I
CI	TINJFL	FUEL TEMPERATURE AT TCA INJECTOR INLET (DEGR ---- \$---- /TEMSCH/)	I
CI	TINJOX	OX TEMPERATURE AT TCA INJECTOR INLET (DEGR ---- \$---- /TEMSCH/)	I
CI	TINSCS	INSULATION THICKNESS IN CYLINDRICAL SECTION OF THE MOTOR CASE (LC) (IN .1 \$MATER /MOTOR/)	I
CI	TINSTG	NO AVAILABLE DEFINITION (/LSCOM/)	I
CI	TINSUL	INSULATION THICKNESS FOR PRESSURE TANK (IN 0.0 \$LIQMAT /TANKS/)	I
CI	TISEFF	GAS GENERATOR BLEED TURBINE EXHAUST ISP EFFICIENCY (--- ---- \$---- /TPAOUT/)	I
CI	TKDAL	TANK OVERALL LENGTH (IN --- \$---- /TANKS/)	I
CI	TKRCHM	REFERENCE CHAMBER THICKNESS OF ABLATIVE (IN 0.22 \$ABLATE /TCA/)	I
CI	TLIMIT	MAXIMUM RUN TIME IN C.P. SECONDS (SEC 4000 \$INPOPT /OPTIM/)	I
CI	TLNADM	THICKNESS OF LINER IN AFT DOME SECTION (IN 0. \$MATER /MOTOR/)	I
CI	TLNFDM	LINER THICKNESS (FORWARD DOME) (IN --- \$MATER /MOTOR/)	I
CI	TLNRCS	THICKNESS OF LINER IN CYLINDRICAL SECTION (IN 0. \$MATER /MOTOR/)	I
CI	TMAX	MAXIMUM VEHICLE OPERATING TEMPERATURE (DEGF 90.0 \$LIQUID /TEMPS/)	I
CI	TMIN	MINIMUM VEHICLE OPERATING TEMPERATURE (DEGF 60.0 \$LIQUID /TEMPS/)	I
CI	TMING	MINIMUM GUAGE THICKNESS OF TANKS (IN 0.035 \$LIQMAT /TANKS/)	I
CI	TMINGL	MINIMUM GUAGE THICKNESS OF LINES (IN 0.065 \$LIQMAT /TANKS/)	I
CI	TMINGS	MINIMUM GUAGE THICKNESS OF STRUCTURAL WALL (IN 0.035 \$LIQMAT /TANKS/)	I
CI	TMLIF	MULTILAYER INSULATION (MLI) THICKNESS FOR FUEL TANK(S) (IN 0. \$TANKHX /INSLHX/)	I
CI	TMLIO	MULTILAYER INSULATION (MLI) THICKNESS FOR OXIDIZER TANK(S) (IN 0. \$TANKHX /INSLHX/)	I
CI	TMNTNK	NO AVAILABLE DEFINITION (/NCTOUT/)	I
CI	TMPCHF	FUEL TEMPERATURE USED IN VAPORIZATION CALCULATION (DEGR ---- \$---- /TEMSCH/)	I
CI	TMPCHO	OX TEMPERATURE USED IN VAPORIZATION CALCULATION (DEGR ---- \$---- /TEMSCH/)	I
CI	TMPRA	NO AVAILABLE DEFINITION (/MOTOR/)	I
CI	TNENOM	NOZZLE EXTENSION DESIGN TEMPERATURE (DEGR 2000 \$LIQENG /COOLNT/)	I
CI	TNKODA	AFT TANK OUTSIDE DIAMETER (IN --- \$---- /TANKS/)	I

Figure 5.1. Common Block Variables (Sheet 36 of 46)

CI	TNKODF	FORWARD TANK OUTSIDE DIAMETER (IN --- \$--- /TANKS/)	I
CI	TNKODP	PRESSURE TANK OUTSIDE DIAMETER (IN --- \$--- /TANKS/)	I
CI	TNOZAB	NOZZLE AVERAGE ABLATIVE THICKNESS (IN O. \$--- /TCA/)	I
CI	TNOZZL	NOZZLE EXTENSION MATERIAL THICKNESS (IN --- \$--- /TCA/)	I
CI	TNZMIN	MINIMUM NOZZLE EXTENSION THICKNESS (IN O. 01 \$LIQENG /TCA/)	I
CI	TNZREF	REFERENCE NOZZLE EXTENSION THICKNESS (IN O. 019 \$LIQENG /TCA/)	I
CI	TOP	NOMINAL VEHICLE OPERATING TEMPERATURE (DEGF 75.0 \$LIQUID /TEMPS/)	I
CI	TOXPIN	OX TEMPERATURE AT MAIN PUMP INLET (DEGR --- \$--- /TEMSCH/)	I
CI	TP	PERIOD OF DESTINATION ORBIT (SEC O. O \$ORB ///EQ///)	I
CI	TPARAM	NO AVAILABLE DEFINITION (///EQ///)	I
CI	TPARAM	NO AVAILABLE DEFINITION (/TRAJ/)	I
CI	TPAWT	TPA WEIGHT (LBM --- \$--- /TPOUT2/)	I
CI	TPHSE	NO AVAILABLE DEFINITION (/TRAJ/)	I
CI	TPLQBS	PLUG CLUSTER BASE THICKNESS (IN O. 5 \$LIQUID /PLGBAS/)	I
CI	TPMAXF	MAX FUEL TEMPERATURE IN TANK (DEGR --- \$LFUEL /TEMSCH/)	I
CI	TPMAXO	MAX OX TEMPERATURE IN TANK (DEGR --- \$LOXID /TEMSCH/)	I
CI	TPMINF	MIN FUEL TEMPERATURE IN TANK (DEGR --- \$LFUEL /TEMSCH/)	I
CI	TPMINO	MIN OX TEMPERATURE IN TANK (DEGR --- \$LOXID /TEMSCH/)	I
CI	TPNOMF	NOMINAL FUEL TEMPERATURE IN TANK (DEGR --- \$LFUEL /TEMSCH/)	I
CI	TPNOMO	NOMINAL OX TEMPERATURE IN TANK (DEGR --- \$LOXID /TEMSCH/)	I
CI	TRANKM	PLATELET MATERIAL THERMAL CONDUCTIVITY IN TRANSPIRATION COOLED SECTION (BTU/IN/SEC/DEGR . 0004 \$INREGN /TRANCO/)	I
CI	TREF	TEMPERATURE AT WHICH REFERENCE PROPERTIES APPLY (DEGR 530. \$LPROP /COOLNT/)	I
CI	TREFFL	FUEL REFERENCE TEMPERATURE FOR REFERENCE PROPERTIES (DEGR --- \$LFUEL /PROPRO/)	I
CI	TREFGG	REFERENCE TEMPERATURE FOR BURN RATE COEFFICIENT OF GAS GENERATOR'S SOLID GRAIN (DEGF 80. \$SOLDGG /GASGEN/)	I
CI	TREFOX	OX REFERENCE TEMPERATURE FOR REFERENCE PROPERTIES (DEGR --- \$LOXID /PROPRO/)	I
CI	TREGFO	FUEL TEMPERATURE AT REGEN JACKET OUTLET (DEGR --- \$--- /TEMSCH/)	I
CI	TREGOO	OX TEMPERATURE AT REGEN JACKET OUTLET (DEGR --- \$--- /TEMSCH/)	I
CI	TRINST	THICKNESS OF TRANSPIRATION COOLING THROAT INSERT (IN O. 3 \$LIQMAT /TRANCO/)	I
CI	TRMX	CHAMBER TEMPERATURE OF NEW PROPELLANT AT PC=500 AND OFRMX (IPROP = 0) (DEGR 5934. \$LPROP /EQUIVR/)	I
CI	TSH	THERMODYNAMIC SUPPRESSION HEAD (NON-ZERO FOR HYDROGEN) (IE EFFECTIVE NPSH FOR PUMP)	I

Figure 5.1. Common Block Variables (Sheet 37 of 46)

CI		(FT 0-OR-90 \$---- /TPAIN/)	I
CI	TSIDE	NO AVAILABLE DEFINITION (/NCTOUT/)	I
CI	TSMMX	COMBUSTION TEMP OF LIBRARY PROPELLANT AT MAX ISP FOR PC=500 E=20	I
CI		(DEGR ---- \$---- /EQUIVR/)	I
CI	TSOFIF	SPRAY ON FOAM INSULATION (SOFI) THICKNESS FOR FUEL TANK(S)	I
CI	TSOFIO	SPRAY ON FOAM INSULATION (SOFI) THICKNESS FOR OXIDIZER TANK(S)	I
CI	TSPCA	(IN 0. \$TANKHX /INSLHX/) SPACE BETWEEN AFT TANK AND VEHICLE SKIN	I
CI	TSPCF	(IN 0.0 \$LTANK /TANKS/) SPACE BETWEEN FORWARD TAN AND VEHICLE SKIN	I
CI	TSPCP	(IN 0.0 \$LTANK /TANKS/) SPACE BETWEEN PRESSURE TANK AND VEHICLE SKIN	I
CI	TSPEED	NO AVAILABLE DEFINITION (/TPOUT2/)	I
CI	TSPH	START SYSTEM SPHERE TEMPERATURE (ISTART=1) (DEGR 210. \$PUMP /TPAIN/)	I
CI	TSTAG1	NO AVAILABLE DEFINITION (/TPOUT2/)	I
CI	TSTAG2	NO AVAILABLE DEFINITION (/TPOUT2/)	I
CI	TSTAG3	NO AVAILABLE DEFINITION (/TPOUT2/)	I
CI	TSTAG4	NO AVAILABLE DEFINITION (/TPOUT2/)	I
CI	TSTAG5	NO AVAILABLE DEFINITION (/TPOUT2/)	I
CI	TSTAGE	NO AVAILABLE DEFINITION (/PERF/)	I
CI	TSTRC	STRUCTURAL WALL THICKNESS (IN --- \$LIQUID /TANKS/)	I
CI	TTEFL1	NO AVAILABLE DEFINITION (/TPOUT2/)	I
CI	TTEOX1	NO AVAILABLE DEFINITION (/TPOUT2/)	I
CI	TTHRAB	ABLATIVE THICKNESS AT THROAT (IN --- \$---- /TCA/)	I
CI	TTOFL	NO AVAILABLE DEFINITION (/TPOUT2/)	I
CI	TTOOX	NO AVAILABLE DEFINITION (/TPOUT2/)	I
CI	TTOP	NO AVAILABLE DEFINITION (/NCTOUT/)	I
CI	TTORMN	NO AVAILABLE DEFINITION (/NCTOUT/)	I
CI	TTORMX	NO AVAILABLE DEFINITION (/NCTOUT/)	I
CI	TTOTP	NO AVAILABLE DEFINITION (/MOTOR/)	I
CI	TTURBI	GAS TEMPERATURE AT TURBINE INLET (DEGR --- \$PUMP /TEMSCH/)	I
CI	TTURBO	GAS TEMPERATURE AT TURBINE OUTLET (DEGR --- \$---- /TEMSCH/)	I
CI	TTWAFT	THICKNESS OF AFT TANK WALL (IN --- \$---- /TANKS/)	I
CI	TTWFWD	THICKNESS OF FORWARD TANK WALL (IN --- \$---- /TANKS/)	I
CI	TTWPRS	THICKNESS OF PRESSURE TANK WALL (IN --- \$---- /TANKS/)	I
CI	TULLFL	NO AVAILABLE DEFINITION (/TEMSCH/)	I
CI	TULLOX	NO AVAILABLE DEFINITION (/TEMSCH/)	I
CI	TURBHP	NO AVAILABLE DEFINITION (/TPAOUT/)	I
CI	TURBPR	TURBINE PRESSURE RATIO (--- 2 \$PUMP /PRESCH/)	I
CI	TUREFF	TURBINE EFFICIENCY (--- --- \$---- /TPAOUT/)	I
CI	TUREFO	NO AVAILABLE DEFINITION (/TPAOUT/)	I
CI	TUREFU	NO AVAILABLE DEFINITION (/TPAOUT/)	I
CI	TURHPF	NO AVAILABLE DEFINITION (/TPAOUT/)	I
CI	TURHPO	NO AVAILABLE DEFINITION (/TPAOUT/)	I
CI	TVLVFL	FUEL TEMPERATURE AT BIPROP VALVE INLET	I

Figure 5.1. Common Block Variables (Sheet 38 of 46)

CI		(DEGR ---- \$---- /TEMSCH/)	I
CI	TVLVFO	FUEL TEMPERATURE AT BIPROP VALVE OUTLET	I
CI		(DEGR ---- \$---- /TEMSCH/)	I
CI	TVLVOO	OX TEMPERATURE AT BIPROP VALVE OUTLET	I
CI		(DEGR ---- \$---- /TEMSCH/)	I
CI	TVLVOX	OX TEMPERATURE AT BIPROP VALVE INLET	I
CI		(DEGR ---- \$---- /TEMSCH/)	I
CI	TWDOTF	TOTAL FUEL FLOWRATE	I
CI		(LBM/SEC --- \$---- /LFLOW/)	I
CI	TWDOTL	TOTAL FLOWRATE	I
CI		(LBM/SEC --- \$---- /LFLOW/)	I
CI	TWDOTO	TOTAL OXIDIZER FLOWRATE	I
CI		(LBM/SEC --- \$---- /LFLOW/)	I
CI	TWOPI	NO AVAILABLE DEFINITION (/CONST/)	I
CI	TXINS	THICKNESS OF EXTERNAL ENSULATION	I
CI		(IN 0. \$MATER /MOTOR/)	I
CI	ULFRHA	ULLAGE FRACTION OF AFT TANK AT TMAX	I
CI		(--- 0.045 \$---- /TANKS/)	I
CI	ULFRHF	ULLAGE FRACTION OF FORWARD TANK AT TMAX	I
CI		(--- 0.045 \$---- /TANKS/)	I
CI	ULLFFL	FUEL TANK ULLAGE FRACTION	I
CI		(--- 0.02 \$LTANK /TANKS2/)	I
CI	ULLFOX	OXIDIZER TANK ULLAGE FRACTION	I
CI		(--- 0.02 \$LTANK /TANKS2/)	I
CI	UOVCFL	NO AVAILABLE DEFINITION (/TPAOUT/)	I
CI	UOVCOX	NO AVAILABLE DEFINITION (/TPAOUT/)	I
CI	UOVERC	TURBINE PITCH LINE VELOCITY DIVIDED BY ISENTROPIC	I
CI		SPOUTING VELOCITY	I
CI		(--- 0.4 \$PUMP /TPAIN/)	I
CI	US	TURBINE BLADE ULTIMATE STRENGTH	I
CI		(PSI 127000 \$PUMP /TPAIN/)	I
CI	V	REGEN STATION LOCAL COOLANT VELOCITY	I
CI		(IN/SEC --- \$---- /RGNSUM/)	I
CI	V65	VISCOOSITY OF REGEN COOLANT AT TR=0.65 PR=1.0	I
CI		(LB*SEC/IN**2 --- \$---- /COOLNT/)	I
CI	V65FL	NO AVAILABLE DEFINITION (/PROPRO/)	I
CI	V65OX	NO AVAILABLE DEFINITION (/PROPRO/)	I
CI	VACQFL	FUEL ACQUISITION SYSTEM VOLUME	I
CI		(IN**3 --- \$---- /TANKS2/)	I
CI	VACQOX	OXIDIZER ACQUISITION SYSTEM VOLUME	I
CI		(IN**3 --- \$---- /TANKS2/)	I
CI	VBAR	NO AVAILABLE DEFINITION (///EQ///)	I
CI	VBO	NO AVAILABLE DEFINITION (///EQ///)	I
CI	VCONE	NO AVAILABLE DEFINITION (/SSCOM/)	I
CI	VCRIT	CRITICAL VISCOOSITY OF REGEN COOLANT	I
CI		(LB*SEC/IN**2 --- \$---- /COOLNT/)	I
CI	VCRITF	FUEL CRITICAL VISCOOSITY	I
CI		(LB*SEC/IN**2 --- \$---- /PROPRO/)	I
CI	VCRITO	OX CRITICAL VISCOOSITY	I
CI		(LB*SEC/IN**2 --- \$---- /PROPRO/)	I
CI	VELI	INITIAL VELOCITY AT IGNITION	I
CI		(FT/SEC 0 \$INTRAJ ///EQ///)	I
CI	VFL	VELOCITY OF FUEL THROUGH INJECTOR ORIFICES	I
CI		(IN/SEC --- \$---- /LIQUID/)	I
CI	VFLTNK	FUEL TANK VOLUME	I
CI		(IN**3 --- \$---- /TANKS2/)	I
CI	VGAS	VISCOOSITY OF CHAMBER COMBUSTION PRODUCTS	I
CI		(LB*SEC/IN**2 --- \$---- /TANKS/)	I
CI	VINSTG	NO AVAILABLE DEFINITION (/LSCOM/)	I
CI	VLNGTH	NO AVAILABLE DEFINITION (/NCTOUT/)	I

Figure 5.1. Common Block Variables (Sheet 39 of 46)

CI	VOLAND	TOTAL MATERIAL VOLUME OF THE LANDS BETWEEN COOLING CHANNELS IN THE REGEN CHAMBER (IN**3 --- \$--- /WTREGN/)	I
CI	VOX	VELOCITY OF OXIDIZER THROUGH INJECTOR ORIFICES (IN/SEC --- \$--- /LIQUID/)	I
CI	VOXTNK	OXIDIZER TANK VOLUME (IN**3 --- \$--- /TANKS2/)	I
CI	VPRTNK	NO AVAILABLE DEFINITION (/TANKS2/)	I
CI	VRE	NO AVAILABLE DEFINITION (///EQ///)	I
CI	VRE1	NO AVAILABLE DEFINITION (/TRAJ/)	I
CI	VRE3	NO AVAILABLE DEFINITION (/TRAJ/)	I
CI	VRE4	NO AVAILABLE DEFINITION (/TRAJ/)	I
CI	VREF	REFERENCE VALUE OF VISCOSITY FOR COOLANT (LBM/IN/SEC 5.17E-5 \$LPROP /COOLNT/)	I
CI	VREFFL	FUEL REFERENCE VISCOSITY (LB*SEC/IN**2 --- \$LFUEL /PROPRO/)	I
CI	VREFOX	OX REFERENCE VISCOSITY (LB*SEC/IN**2 --- \$LOXID /PROPRO/)	I
CI	VS	NO AVAILABLE DEFINITION (/MOTOR/)	I
CI	VSTG	NO AVAILABLE DEFINITION (/TRAJ/)	I
CI	VTANKS	NO AVAILABLE DEFINITION (/NCTIN/)	I
CI	VTERM	NO AVAILABLE DEFINITION (///EQ///)	I
CI	VTOT	NO AVAILABLE DEFINITION (/TRAJ/)	I
CI	VULLA	ULLAGE VOLUME OF AFT TANK (IN**3 --- \$--- /TANKS/)	I
CI	VULLF	ULLAGE VOLUME OF FORWARD TANK (IN**3 --- \$--- /TANKS/)	I
CI	VX	NO AVAILABLE DEFINITION (/TRAJ/)	I
CI	VXACFT	HORIZONTAL VELOCITY OF LAUNCH AIRCRAFT (ASSUMED CONSTANT AND USED FOR COMPUTING MISSILE SEPARATION RANGE) (FT/SEC 0 \$INTRAJ /TRAJ/)	I
CI	VY	NO AVAILABLE DEFINITION (/TRAJ/)	I
CI	W	REGEN STATION LOCAL CHANNEL WIDTH (IN --- \$--- /RGNSUM/)	I
CI	WACQFL	FUEL ACQUISITION SYSTEM WEIGHT (LB --- \$--- /TANKS2/)	I
CI	WACQOX	OXIDIZER ACQUISITION SYSTEM WEIGHT (LB --- \$--- /TANKS2/)	I
CI	WAFCSK	AFT SKIRT WEIGHT (LBM --- \$--- /SSCOM/)	I
CI	WAFDOM	DOME WEIGHT (AFT) (LBM --- \$--- /SSCOM/)	I
CI	WAINST	NO AVAILABLE DEFINITION (/MOTOR/)	I
CI	WALLK	THERMAL CONDUCTIVITY OF CHAMBER WALL MATERIAL (AT AVERAGE WALL OPERATING TEMPERATURE)	I
CI	WALLTH	(BTU/IN/SEC/DEGR 0.00039 \$INREGN /COOLNT/) CHAMBER WALL THICKNESS (IN 0.025 \$--- /COOLNT/)	I
CI	WATL	AFT TANK LINES WEIGHT (LBM --- \$--- /TANKS/)	I
CI	WBNDUT	GROSS BURNOUT WEIGHT (LBM --- \$--- /LSCOM/)	I
CI	WBOILF	NO AVAILABLE DEFINITION (/TANKS2/)	I
CI	WBOILO	NO AVAILABLE DEFINITION (/TANKS2/)	I
CI	WCASE	NO AVAILABLE DEFINITION (/SSCOM/)	I
CI	WCAT	MISCELLANEOUS CASE WEIGHT (LBM --- \$--- /MOTOR/)	I
CI	WCCYL	CYLINDRICAL CASE WEIGHT (LBM --- \$--- /SSCOM/)	I

Figure 5.1. Common Block Variables (Sheet 40 of 46)

CI	WCONE	NO AVAILABLE DEFINITION (/SSCOM/)
CI	WDAUTF	FUEL TANK AUTOGENOUS PRESSURANT FLOWRATE (LB/SEC --- \$--- /SCHEDW/)
CI	WDAUTO	OX TANK AUTOGENOUS PRESSURANT FLOWRATE (LB/SEC --- \$--- /SCHEDW/)
CI	WDBLNZ	GAS GENERATOR BLEED NOZZLE FLOWRATE (LB/SEC --- \$--- /SCHEDW/)
CI	WDBYPF	FUEL TURBINE BYPASS FLOWRATE (LB/SEC --- \$--- /SCHEDW/)
CI	WDBYPO	OX TURBINE BYPASS FLOWRATE (LB/SEC --- \$--- /SCHEDW/)
CI	WDBYRF	FUEL REGEN JACKET BYPASS FLOWRATE (LB/SEC --- \$--- /SCHEDW/)
CI	WDBYRO	OX REGEN JACKET BYPASS FLOWRATE (LB/SEC --- \$--- /SCHEDW/)
CI	WDINJF	FUEL FLOWRATE THROUGH TCA INJECTOR (LB/SEC --- \$--- /SCHEDW/)
CI	WDINJO	OX FLOWRATE THROUGH TCA INJECTOR (LB/SEC --- \$--- /SCHEDW/)
CI	WDOT	TABLE OF WEIGHT FLOW RATE FOR VARIABLE THRUST-TIME TRACE (LBF/SEC 0.0 \$THVST /PERF/)
CI	WDOTF	FUEL FLOWRATE THROUGH A SINGLE TCA (LB/SEC --- \$--- /LIQUID/)
CI	WDOTL	PROPELLANT FLOW RATE (LBM/SEC --- \$--- /LIQUID/)
CI	WDOTO	OXIDIZER FLOWRATE THROUGH A SINGLE TCA (LB/SEC --- \$--- /LIQUID/)
CI	WDOTTR	TOTAL TRANSPERSION COOLANT FLOWRATE (LB/SEC --- \$--- /TRANCO/)
CI	WDPMPPF	FUEL FLOWRATE THROUGH MAIN PUMP (LB/SEC --- \$--- /SCHEDW/)
CI	WDPMPO	OX FLOWRATE THROUGH MAIN PUMP (LB/SEC --- \$--- /SCHEDW/)
CI	WDREGF	FUEL FLOWRATE THROUGH REGEN JACKET (LB/SEC --- \$--- /SCHEDW/)
CI	WDREGO	OX FLOWRATE THROUGH REGEN JACKET (LB/SEC --- \$--- /SCHEDW/)
CI	WDRGN	FLOW RATE EXITING REGEN JACKET (IE. MINUS THE TRANSPERSION COOLANT FLOWRATE) (LB/SEC --- \$--- /RGNSUM/)
CI	WDTANF	FUEL TRANSPERSION COOLING FLOWRATE (LB/SEC --- \$--- /SCHEDW/)
CI	WDTANO	OX TRANSPERSION COOLING FLOWRATE (LB/SEC --- \$--- /SCHEDW/)
CI	WDXEXP	NO AVAILABLE DEFINITION (/LSCOM/)
CI	WDTKOF	FUEL FLOWRATE OUT OF TANK (LB/SEC --- \$--- /SCHEDW/)
CI	WDTKOO	OX FLOWRATE OUT OF TANK (LB/SEC --- \$--- /SCHEDW/)
CI	WDTRIF	FUEL FLOWRATE INTO PREBURNER (LB/SEC --- \$--- /SCHEDW/)
CI	WDTRIO	OX FLOWRATE INTO PREBURNER (LB/SEC --- \$--- /SCHEDW/)
CI	WDTROF	NO AVAILABLE DEFINITION (/SCHEDW/)
CI	WDTROO	NO AVAILABLE DEFINITION (/SCHEDW/)
CI	WDTURB	TURBINE FLOWRATE (LB/SEC --- \$--- /SCHEDW/)
CI	WDVLVF	FUEL FLOWRATE THROUGH BIPROP VALVE (LB/SEC --- \$--- /SCHEDW/)

Figure 5.1. Common Block Variables (Sheet 41 of 46)

CI	WDVLVO	OX FLOWRATE THROUGH BIPROP VALVE (LB/SEC ---- \$---- /SCHEDW/)	I
CI	WEXPND	WEIGHT OF EXPENDABLE INERTS FOR EACH STAGE (EXPENDED LINERLY WITH BURN TIME) (LBM O. O \$INPGEN /GENRL/)	I
CI	WFINST	NO AVAILABLE DEFINITION (/MOTOR/)	I
CI	WFTL	FORWARD TANK LINES WEIGHT (LBM --- \$---- /TANKS/)	I
CI	WFUEL	PROPELLANT WEIGHT (LBM --- \$---- /GENRL/)	I
CI	WFUELR	NO AVAILABLE DEFINITION (/SSCOM/)	I
CI	WFWCSK	FORWARD SKIRT WEIGHT (LBM --- \$---- /SSCOM/)	I
CI	WFWDOM	DOME WEIGHT (FORWARD) (LBM --- \$---- /SSCOM/)	I
CI	WGAS	PRESSURANT WEIGHT (LBM --- \$---- /TANKS/)	I
CI	WGGBPB	NO AVAILABLE DEFINITION (/TPDOUT2/)	I
CI	WGL	GAS LINES WEIGHT (LBM --- \$---- /TANKS/)	I
CI	WGRES	WEIGHT OF RESIDUAL GAS IN PRESSURANT TANK (LBM --- \$---- /COLDGP/)	I
CI	WHGMF	NO AVAILABLE DEFINITION (/TPDOUT2/)	I
CI	WIGN	STAGE IGNITION WEIGHT (LBM --- \$---- /GENRL/)	I
CI	WIGNIT	NO AVAILABLE DEFINITION (/TPDOUT2/)	I
CI	WINERT	INTERSTAGE WEIGHT (LBM --- \$---- /GENRL/)	I
CI	WINSFL	FUEL TANK INSULATION WEIGHT (LB --- \$---- /INSLHX/)	I
CI	WINSOX	OXIDIZER TANK INSULATION WEIGHT (LB --- \$---- /INSLHX/)	I
CI	WINSTG	NO AVAILABLE DEFINITION (/LSCOM/)	I
CI	WINSUL	INTERNAL INSULATION WEIGHT (LBM --- \$---- /LSCOM/)	I
CI	WLINER	LINER WEIGHT (LBM --- \$---- /SSCOM/)	I
CI	WLTHR	LAND WIDTH BETWEEN COOLANT CHANNELS AT THROAT (IN 0.03 \$INREGN /COOLNT/)	I
CI	WM1	NO AVAILABLE DEFINITION (/PERF/)	I
CI	WMGGPB	MOLECULAR WEIGHT OF GAS GENERATOR/PREBURNER COMBUSTION GAS (--- 14 \$PUMP /TPAIN/)	I
CI	WMI	NO AVAILABLE DEFINITION (/PERF/)	I
CI	WMISCC	MISCELLANEOUS WEIGHT PER STAGE EXCLUDING PAYLOAD (LBM O \$INPGEN /GENRL/)	I
CI	WMISFL	MISCELLANEOUS FUEL ADDED TO STAGE (REMAINS ON STAGE AT BURNOUT) (LBM O \$INPGEN /GENRL/)	I
CI	WMISOX	MISCELLANEOUS OXIDIZER ADDED TO STAGE (REMAINS ON STAGE AT BURNOUT) (LBM O \$INPGEN /GENRL/)	I
CI	WMOUNT	THRUST MOUNT WEIGHT (LBM --- \$---- /TCA/)	I
CI	WNCTLN	NO AVAILABLE DEFINITION (/NCTOUT/)	I
CI	WNDMPH	WIND VELOCITY AROUND VEHICLE FOR HEAT TRANSFER OPTION (KHXOPT=3) (MPH 10 \$TANKHX /INSLHX/)	I
CI	WNOZ	NOZZLE ASSEMBLY WEIGHT (LBM --- \$---- /SSCOM/)	I

Figure 5.1. Common Block Variables (Sheet 42 of 46)

CI	WPAY	NO AVAILABLE DEFINITION (/GENRL/)	I
CI	WPAYLD	PAYOUT WEIGHT FORWARD OF THE FINAL PROPULSIVE STAGE	I
CI	WPAYR	(LBM 0 \$INPGEN ///EQ///)	I
CI	WPBODGG	NO AVAILABLE DEFINITION (/SSCOM/)	I
CI		WEIGHT OF PRESSURANT IN PROPELLANT TANKS	I
CI	WPCH	(LBM --- \$--- /GASGEN/)	I
CI	WPDOT	PRESSURANT CONTROL HARDWARE WEIGHT	I
CI		(LBM --- \$--- /TANKS/)	I
CI	WPERC	PROPELLANT FLOW RATE	I
CI		(LBM/SEC --- \$--- /PERF/)	I
CI	WPEXPL	PERCENT STAGE WEIGHT USED AS MISC	I
CI		(--- 0. \$INPGEN /MOTOR/)	I
CI	WPLEFT	NO AVAILABLE DEFINITION (/PERF/)	I
CI	WPLGBS	NO AVAILABLE DEFINITION (/PERF/)	I
CI		PLUG CLUSTER BASE WEIGHT	I
CI	WPROP	(LBM --- \$--- /PLGBAS/)	I
CI		WEIGHT OF STAGE PROPELLANT (THRUST-TIME OPTION)	I
CI		(LBM 0.0 \$THVST ///EQ///)	I
CI	WRESFL	NO AVAILABLE DEFINITION (/TANKS2/)	I
CI	WRESOX	NO AVAILABLE DEFINITION (/TANKS2/)	I
CI	WSHTNK	NO AVAILABLE DEFINITION (/NCTOUT/)	I
CI	WSTART	NO AVAILABLE DEFINITION (/TPOUT2/)	I
CI	WSUPHD	THRUST CHAMBER ASSY SUPPORT HARDWARE WEIGHT	I
CI		(LBM --- \$--- /TCA/)	I
CI	WTANKS	TOTAL STAGE TANK WEIGHT	I
CI		(LBM --- \$--- /TANKS/)	I
CI	WTATJT	WEIGHT OF AFT TANK JOINTS	I
CI		(LBM --- \$--- /LQTLPR/)	I
CI	WTATNK	AFT TANK WEIGHT	I
CI		(LBM --- \$--- /LQTLPR/)	I
CI	WTBLDA	AFT BLADDER WEIGHT	I
CI		(LBM --- \$--- /TANKS/)	I
CI	WTBLDF	FORWARD BLADDER WEIGHT	I
CI		(LBM --- \$--- /TANKS/)	I
CI	WTBNDA	AFT BOND WEIGHT	I
CI		(LBM --- \$--- /TANKS/)	I
CI	WTBNDF	FORWARD BOND WEIGHT	I
CI		(LBM --- \$--- /TANKS/)	I
CI	WTCHAM	CHAMBER WEIGHT	I
CI		(LBM --- \$--- /TCA/)	I
CI	WTFTJT	WEIGHT OF FORWARD TANK JOINTS	I
CI		(LBM --- \$--- /LQTLPR/)	I
CI	WTFTNK	FORWARD TANK WEIGHT	I
CI		(LBM --- \$--- /LQTLPR/)	I
CI	WTGIMB	GIMBAL SYSTEM WEIGHT	I
CI		(LBM --- \$--- /GIMBAL/)	I
CI	WTHR	COOLANT CHANNEL WIDTH AT CHAMBER THROAT	I
CI		(IN 0.03 \$INREGN /COOLNT/)	I
CI	WTHTX	AUTOGENDOUS PRESSURIZATION HEAT EXCHANGER WEIGHT	I
CI		(LBM --- \$--- /TPOUT2/)	I
CI	WTINJ	INJECTOR WEIGHT	I
CI		(LBM --- \$--- /TCA/)	I
CI	WTJET	AMOUNT OF INERT WEIGHT JETTISONED DURING THE CURRENT MOTOR SECTION	I
CI		(LBM 0. \$GUIDA /PERF/)	I
CI	WTKMNT	TANK MOUNT WEIGHT	I
CI		(LBM --- \$--- /TANKS/)	I
CI	WTLPRP	WEIGHT OF BURNED LIQUID PROPELLANT	I
CI		(LBM 13250. \$LIQUID ///EQ///)	I

Figure 5.1. Common Block Variables (Sheet 43 of 46)

CI	WTLTCA	WEIGHT OF LIQUID TCA (KWTMOD = -1) (LBM 184.1 \$LIQENG /TCA/)	I
CI	WTM	WEIGHT OF TOTAL MISSILE SYSTEM (LBM --- \$THVST /PERF/)	I
CI	WTMCG	MOLECULAR WEIGHT OF COLD GAS PRESSURANT (LB/LBMOLE 4. \$COLDG /COLDGP/)	I
CI	WTMGG	MOLECULAR WEIGHT OF GAS GENERATOR PRESSURANT (LB/LBMOLE 19.0 \$SOLDGG /GASGEN/)	I
CI	WTMOLF	(MOLECULAR WEIGHT OF COOLANT \$LPROP /COOLNT/) FUEL MOLECULAR WEIGHT (LB/LBMOLE --- \$LFUEL /PROPRO/)	I
CI	WTMOLO	OX MOLECULAR WEIGHT (LB/LBMOLE --- \$LOXID /PROPRO/)	I
CI	WTMOUT	NO AVAILABLE DEFINITION (//EQ//)	I
CI	WTNZEX	NOZZLE EXTENSION WEIGHT (LBM --- \$--- /TCA/)	I
CI	WTPLIN	NO AVAILABLE DEFINITION (/TPOUT2/)	I
CI	WTPOW	GIMBAL POWER SUPPLY WEIGHT (LBM 0. \$--- /GIMBAL/)	I
CI	WTPTJT	WEIGHT OF PRESSURANT TANK JOINTS (LBM --- \$--- /LQTLPR/)	I
CI	WTPTNK	PRESSURE TANK WEIGHT (LBM --- \$--- /LQTLPR/)	I
CI	WTRHSA	AFT TANK REVERSE HEAD STIFFENER WEIGHT (LBM --- \$--- /LQTLPR/)	I
CI	WTRHSF	FORWARD TANK REVERSE HEAD STIFFENER WEIGHT (LBM --- \$--- /LQTLPR/)	I
CI	WTRNOZ	WEIGHT OF TRANSLATING NOZZLE (LBM --- \$--- /TRANOZ/)	I
CI	WTSKTA	AFT SKIRT WEIGHT (LBM --- \$--- /TANKS/)	I
CI	WTSKTF	FORWARD SKIRT WEIGHT (LBM --- \$--- /TANKS/)	I
CI	WTSTAG	TOTAL INERT WEIGHT OF THE STAGE (LBM 0.0 \$THVST /PERF/)	I
CI	WTSTW	STRUCTURAL WALL WEIGHT (LBM --- \$--- /TANKS/)	I
CI	WTURBF	NO AVAILABLE DEFINITION (/TPAOUT/)	I
CI	WTURBO	NO AVAILABLE DEFINITION (/TPAOUT/)	I
CI	WTVLVS	VALVE WEIGHT (LBM --- \$--- /TCA/) (LBM EXTERNAL INSULATION WEIGHT \$--- /SSCOM/)	I
CI	WZERO	GROSS IGNITION WEIGHT (LBM --- \$--- /LSCOM/)	I
CI	WZEROS	TOTAL STAGE WEIGHT (LBM --- \$--- /LSCOM/)	I
CI	XA	NO AVAILABLE DEFINITION (/SSCOM/)	I
CI	XACCFL	NO AVAILABLE DEFINITION (/TPOUT2/)	I
CI	XACCOX	NO AVAILABLE DEFINITION (/TPOUT2/)	I
CI	XAFSKT	LENGTH OF AFT SKIRT (IN 0.0 \$INTSTG //EQ//)	I
CI	XCYL	LENGTH OF CYLINDRICAL SECTION OF MOTOR CASE (IN 10. \$INPGEN //EQ//)	I
CI	XDOME	NO AVAILABLE DEFINITION (/SSCOM/)	I
CI	XE	NO AVAILABLE DEFINITION (/SSCOM/)	I
CI	XENG	NO AVAILABLE DEFINITION (/NCTOUT/)	I
CI	XFWSKT	LENGTH OF FWD SKIRT (IN 0.0 \$INTSTG //EQ//)	I
CI	XINJFF	LENGTH FROM INJECTOR FACE TO ENGINE GIMBAL POINT (IN --- \$--- /LIQUID/)	I

Figure 5.1. Common Block Variables (Sheet 44 of 46)

CI	XINSTG	INTERSTAGE LENGTH (IN --- \$--- /LSCOM/)	I
CI	XISODE	IDEAL ONE DIMENSIONAL EQUILIBRIUM ISP (VACUUM) (SEC --- \$--- /LIQUID/)	I
CI	XISP	DELIVERED VACUUM SPECIFIC IMPULSE (KPERF=0) (SEC 314.1 \$LQPERF /LIQUID/)	I
CI	XISPR	REFERENCE SPECIFIC IMPULSE: INPUT AS A FUNCTION OF REFERENCE CHAMBER PRESSURE (SEC 265. \$PROPEL /MOTOR/)	I
CI	XISVAC	VACUUM DELIVERED ISP (SEC --- \$--- /SSCOM/)	I
CI	XITOT	INPUT TOTAL IMPULSE CORRECTION FACTOR FOR VARIABLE THRUST-TIME TRACE (LBF/SEC 0.0 \$THVST ///EQ///)	I
CI	XITVAC	NO AVAILABLE DEFINITION (/SSCOM/)	I
CI	XKALFA	HELICAL BULK FACTOR (--- 1.9 \$FILMNT /MOTOR/)	I
CI	XKN	NO AVAILABLE DEFINITION (/MOTOR/)	I
CI	XKTH	HOOP BULK FACTOR (--- 1.6 \$FILMNT /MOTOR/)	I
CI	XLC	AXIAL CHAMBER CYLINDRICAL LENGTH (IN 0.0 \$LIQENG /LIQUID/)	I
CI	XLDOME	NO AVAILABLE DEFINITION (/MOTOR/)	I
CI	XLDUCB	NO AVAILABLE DEFINITION (/TPOUT2/)	I
CI	XLDUCF	NO AVAILABLE DEFINITION (/TPOUT2/)	I
CI	XLDUCI	NO AVAILABLE DEFINITION (/TPOUT2/)	I
CI	XLDUCO	NO AVAILABLE DEFINITION (/TPOUT2/)	I
CI	XLDUCT	NO AVAILABLE DEFINITION (/TPOUT2/)	I
CI	XLEEXP	ENEC-NOZZLE LENGTH RATIO (--- --- \$--- /MOTOR/)	I
CI	XLFL	BARRIER LIQUID FILM LENGTH (IN 1.0 \$LQPERF ///EQ///)	I
CI	XLGGPB	NO AVAILABLE DEFINITION (/TPOUT2/)	I
CI	XLLBPF	NO AVAILABLE DEFINITION (/TPOUT2/)	I
CI	XLLBPO	NO AVAILABLE DEFINITION (/TPOUT2/)	I
CI	XLLMPF	NO AVAILABLE DEFINITION (/TPOUT2/)	I
CI	XLLMPO	NO AVAILABLE DEFINITION (/TPOUT2/)	I
CI	XLN	AXIAL CHAMBER CONVERGENT LENGTH (IN 18.7 \$LIQENG /LIQUID/)	I
CI	XLNEXP	NOZZLE EXPOSED LENGTH (IN --- \$--- ///EQ///)	I
CI	XLNOZ	LENGTH OF NOZZLE FROM THROAT TO EXIT PLANE (KWTMOD = -1)	I
CI	XLSTG	(IN 76.04 \$LIQENG /LSCOM/)	I
CI	STAGE LENGTH (IN --- \$--- ///EQ///)	I	
CI	XLSUB	NOZZLE SUBMERGED LENGTH (IN --- \$--- ///EQ///)	I
CI	XLTOTL	TOTAL VEHICLE LENGTH (IN --- \$--- ///EQ///)	I
CI	XLTPA	NO AVAILABLE DEFINITION (/TPOUT2/)	I
CI	XLTPAF	NO AVAILABLE DEFINITION (/TPOUT2/)	I
CI	XLTPAO	NO AVAILABLE DEFINITION (/TPOUT2/)	I
CI	XLTUBE	NO AVAILABLE DEFINITION (/TPOUT2/)	I
CI	XM	NO AVAILABLE DEFINITION (/MOTOR/)	I
CI	XMACH	NO AVAILABLE DEFINITION (/TRAJ/)	I
CI	XMOUNT	LENGTH FROM TANK TO ENGINE GIMBAL POINT (IN 2. \$LIQENG /LIQUID/)	I
CI	XMU	NO AVAILABLE DEFINITION (/CONST/)	I
CI	XNORD	NUMBER OF ROVINGS	I

Figure 5.1. Common Block Variables (Sheet 45 of 46)

CI	XNOZ	(--- 8.0 \$FILMNT /MOTOR/)	I
CI	XNRATE	NO AVAILABLE DEFINITION (/NCTIN/)	I
CI		PROPELLANT BURNING RATE PRESSURE EXPONENT IN THE	I
CI		ST. ROGERTS BURNING RATE LAW	I
CI	XNUASK	(--- 40 \$PROPEL /MOTOR/)	I
CI	XNUCSE	POISSON'S RATIO OF STAGE AFT SKIRT	I
CI		(--- .25 \$INTSTG /MOTOR/)	I
CI	XNUINS	POISSON'S RATIO FOR THE CASE MATERIAL	I
CI		(--- .25 \$MATER /MOTOR/)	I
CI	XREGCN	POISSON'S RATIO FOR THE INTERSTAGE MATERIAL	I
CI		(--- .25 \$INTSTG /MOTOR/)	I
CI	XREGCY	NO AVAILABLE DEFINITION (/REGOUT/)	I
CI	XREGNZ	NO AVAILABLE DEFINITION (/REGOUT/)	I
CI	XSHTNK	NO AVAILABLE DEFINITION (/REGOUT/)	I
CI	XTAR	NO AVAILABLE DEFINITION (/NCTOUT/)	I
CI		INTERMEDIATE AREA RATIO ARRAY IN PERFORMANCE	I
CI		ROUTINES	I
CI		(--- --- \$--- /OPCOND/)	I
CI	XTNK	NO AVAILABLE DEFINITION (/NCTOUT/)	I
CI	XTPC	INTERMEDIATE CHAMBER PRESSURE ARRAY IN PERFORMANCE	I
CI		ROUTINES	I
CI		(--- --- \$--- /OPCOND/)	I
CI	XX	NO AVAILABLE DEFINITION (/XSTOR/)	I
CI	Y1	AXIAL LENGTH FROM AFT DOME TANGENT POINT TO NOZZLE	I
CI		ATTACH POINT	I
CI	Y2	(IN --- \$--- /GENRL/)	I
CI		AXIAL LENGTH FROM FORWARD DOME TANGENT POINT TO A	I
CI		POINT ON THE DOME IMMEDIATELY AFT OF THE NEXT	I
CI		UPPER STAGE NOZZLE EXIT (FINAL STAGE USES DOME	I
CI		AXIAL LENGTH PLUS 1.0 INCH)	I
CI		(IN --- \$--- /GENRL/)	I
CI	YENG	NO AVAILABLE DEFINITION (/NCTOUT/)	I
CI	YHITNK	NO AVAILABLE DEFINITION (/NCTOUT/)	I
CI	YLOTNK	NO AVAILABLE DEFINITION (/NCTOUT/)	I
CI	YMOD	MATERIAL ELASTIC MODULUS TABLE	I
CI		(PSI 29E6, 17E6, 8*0 \$LIQMAT /MTPROP/)	I
CI	YS	TURBINE BLADE YIELD STRENGTH	I
CI		(PSI 104000 \$PUMP /TPAIN/)	I
CI	YVMR	INTERMEDIATE MIXTURE RATIO ARRAY IN PERFORMANCE	I
CI		ROUTINES	I
CI		(--- --- \$--- /OPCOND/)	I
CI	ZENG	NO AVAILABLE DEFINITION (/NCTOUT/)	I
CI	ZTNK	NO AVAILABLE DEFINITION (/NCTOUT/)	I
CI	ZTTC	INTERMEDIATE CHAMBER TEMPERATURE ARRAY IN	I
CI		PERFORMANCE ROUTINES	I
CI		(--- --- \$--- /OPCOND/)	I
CI	ZTVAR	INTERMEDIATE VALUE ARRAY IN PERFORMANCE ROUTINES	I
CI		(--- --- \$--- /OPCOND/)	I

Figure 5.1. Common Block Variables (Sheet 45 of 46)

6.0 PROPELLANT LIBRARY

The calculation of liquid engine performance begins with the ideal one dimensional equilibrium performance. The ideal performance is provided to ELES through internal data arrays for specific impulse, characteristic velocity, and combustion temperature. A part of the ELES initialization procedure is the loading of those data arrays from the direct access file called PROPLIB.

In PROPLIB the first block of information lists the propellant combinations for which data exists in the file, the corresponding propellant flag (IPROP) value, and the line location where the data begins. As new propellant combinations are added to the file, the first blank card after the propellant list must be replaced with a card that identifies the propellant data location (See Figure 6.1). The line numbers along the left hand margin of Figure 6.1 are for convenience only. They are not a part of the file.

Notice that on line 6 of Figure 6.1 the flag IPROP=1 corresponds to the propellant combination N_2O_4/MMH , and that line 31 is where the data for N_2O_4/MMH begins. Looking at line 31, there is a header for the propellant combination, followed by comment cards, and finally the beginning of the data itself.

The structure of the propellant data is shown in Figure 6.2. It is read into ELES by the subroutine MAKCAS. MAKCAS opens the data file PROPLIB and reads the performance data. The subroutine locates the proper data block and loads the data into the appropriate data array. These data arrays are passed to the appropriate subroutines via COMMON blocks. The arrays have been sized to hold data for a maximum of 4 stages, 8 chamber pressures, 10 mixture ratios, and 17 area ratios.

MAKCAS reads all the comment cards looking for the key identifier that proceeds each data group. If the key identifier is not found, MAKCAS will print an error message identifying which data was not found, and then terminate execution.

When the data is required by some design routine within ELES, it is accessed through the routines MAKODE, MAKODK, and MAKCSR. MAKODE finds the ODE specific impulse and combustion temperature. MAKODK calculates the kinetic specific

1) C
 2) C PROPELLANT COMBINATIONS AND DATA LOCATION
 3) C
 4) C
 5) FLAG PROPELLANTS LINE
 6) IPROP=1 N204/MMH 31
 7) IPROP=2 MON-25/MHF-3 431
 8) IPROP=3 CLF5/MHF-3 831
 9) IPROP=4 MON-25/60%MFH-3+40%AL 1231
 10) IPROP=5 LOX/LH2 1631
 11) IPROP=6 LOX/RP-1 2031
 12) IPROP=7 LOX/CH4 2431
 13) IPROP=8 LF2/LH2 2831
 14) IPROP=9 LF2/N2H4 3231
 15) C
 16) C
 17) C
 18) C
 19) C
 20) CC
 21) C
 22) C
 23) C
 24) C
 25) C
 26) C
 27) C
 28) C
 29) C
 30) C
 31) C PROPELLANTS: N204/MMH
 32) C
 33) C ASSUMPTIONS ENTHALPY TEMP STATE
 34) C N204
 35) C MMH
 36) C
 37) C
 38) C
 39) C C-STAR & CHAMBER TEMP DATA EVALUATED AT ODE PC & ODE MR VALUESC
 40) C
 41) C
 42) C
 43) SIZE OF VARIOUS DATA ARRAYS
 44) ODE PC ODE MR ODE EPS ODK PC ODK MR ODK EPS
 45) 4 7 10 0 0 0
 46) C
 47) ODE MIXTURE RATIO VALUES
 48) MR= 0.0 0.5 1.0 1.5 2.0 2.3 2.8
 49) C
 50) EPS CHAMBER PRESSURE = 50.0 ODE SPECIFIC IMPULSE
 51) 1. 155.8 175.2 208.9 218.0 214.8 210.8 203.9
 52) 2. 184.4 206.2 244.1 257.8 256.4 251.9 243.7
 53) 4. 202.9 226.6 264.8 282.1 283.7 279.6 270.5
 54) 10. 221.3 247.2 283.4 304.4 310.0 307.4 297.4
 55) 20. 232.2 259.8 293.8 316.6 324.7 323.9 313.5
 56) 40. 240.4 270.6 302.6 326.3 336.3 337.1 326.6
 57) 70. 245.6 278.2 308.9 332.6 344.0 345.9 335.3
 58) 100. 248.4 282.6 312.7 336.2 348.2 350.7 340.2
 59) 150. 251.4 287.2 316.6 339.7 352.5 355.7 345.0
 60) 200. 253.3 290.3 319.3 342.0 355.2 358.8 348.2

Figure 6.1. Beginning of Propellant Library (PROPLIB)

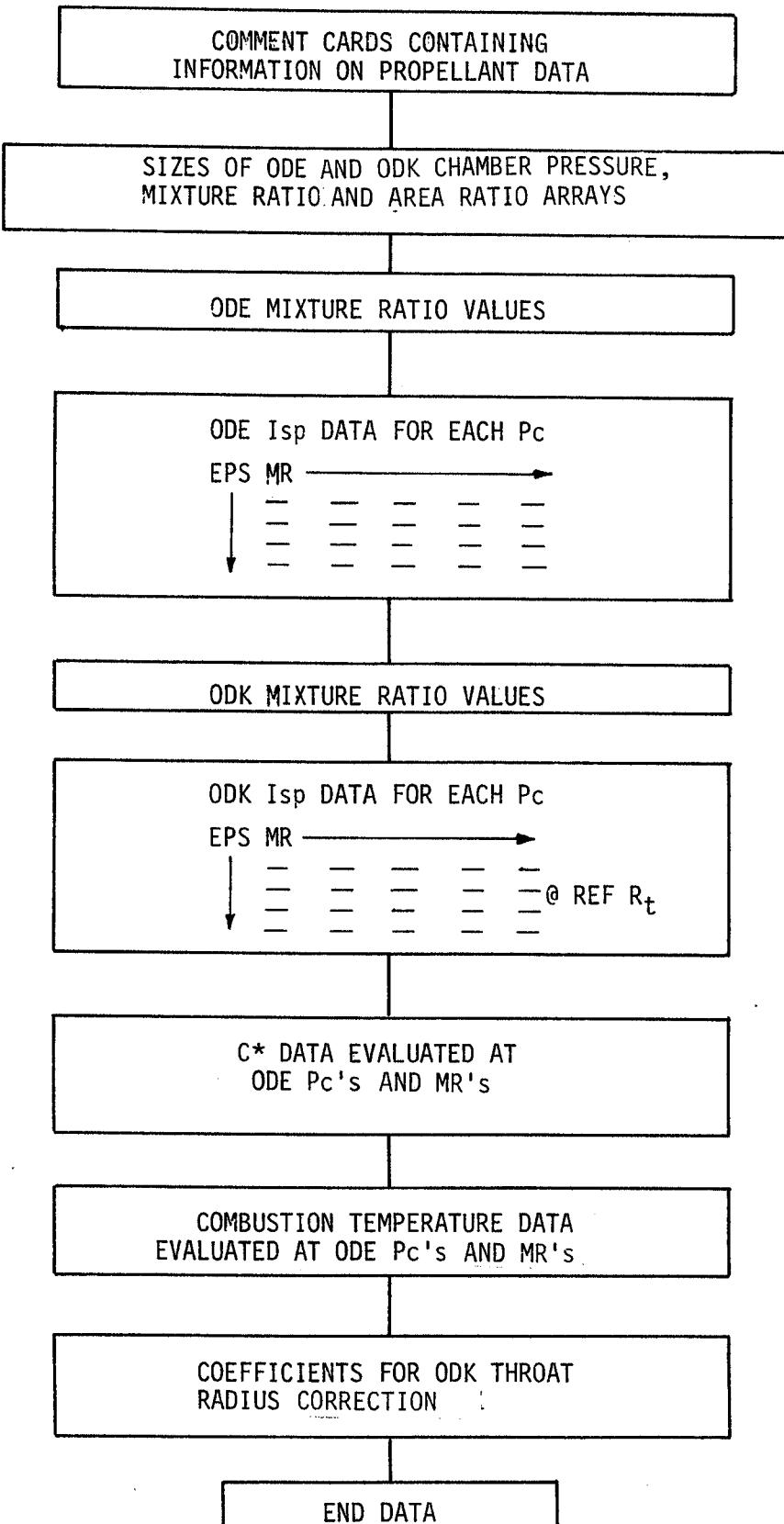


Figure 6.2. Propellant Data Structure

6.0, Propellant Library (cont.)

impulse for the desired operating point. MAKCSR calculates the characteristic velocity for a desired chamber pressure and mixture ratio.

These routines use standardized double (DBTINT) and single (GENTRP) interpolation routines that have been used at Aerojet for several years. The interpolation order can be varied from 1 to 5 in these routines. Experience has shown a second order interpolation to provide the most accurate results and therefore is selected for use in these subroutines. If any of the specified operating points are outside the range of the data provided, a linear extrapolation will be performed using the two closest data points.

Figure 6.3 is a complete listing of the propellant library.

C PROPELLANT COMBINATIONS AND DATA LOCATION

FLAG	PROPELLANTS	LINE
IPROP=1	N204/MMH	31
IFRGP=2	MON-25/MHF-3	431
IPROP=3	CLF5/MHF-3	831
IPROP=4	MON-25/60%MFH-3+40%AL	1231
IPROP=5	LOX/LH2	1631
IPROP=6	LOX/RP-1	2031
IPROP=7	LOX/CH4	2431
IPROP=8	LF2/LH2	2831
IPROP=9	LF2/N2H4	3231

C PROPELLANTS: N204/MMH

ASSUMPTIONS	ENTHALPY	TEMP	STATE
N204			
MMH			

C -STAR & CHAMBER TEMP DATA EVALUATED AT CDE PC & CDE MR VALUES

SIZE OF VARIOUS DATA ARRAYS

CDE PC	CDE MR	CDE EPS	ODK PC	CDE MR	ODK EPS
4	7	10	6	0	0

CDE MIXTURE RATIO VALUES

MRE	0.0	0.5	1.0	1.5	2.0	2.3	2.8
-----	-----	-----	-----	-----	-----	-----	-----

EPS	CHAMBER PRESSURE =	50.0	CDE SPECIFIC IMPULSE	
1.	165.8	175.2	208.9	218.0 214.8 210.8 203.9
2.	184.4	206.2	244.1	257.8 256.4 251.9 243.7
4.	202.9	226.6	264.8	282.1 283.7 279.6 270.5
10.	221.3	247.2	283.4	304.4 310.0 307.4 297.4
20.	232.2	259.8	293.8	316.6 324.7 323.9 313.5
40.	243.4	273.6	302.6	326.3 336.3 337.1 326.6
70.	248.1	278.2	308.9	332.6 344.0 345.9 335.3
100.	248.4	282.6	312.7	336.2 348.2 350.7 340.2
150.	251.4	287.2	316.6	339.7 352.5 355.7 345.0
200.	253.3	293.3	319.3	342.0 355.2 358.8 348.2

Figure 6.3. Propellant Library (PROPLIB) (Sheet 1 of 32)

C

EPS	CHAMBER PRESSURE = 500.0				ODE SPECIFIC IMPULSE		
1.	161.5	180.3	209.1	220.5	219.9	216.2	208.9
2.	190.9	212.4	244.2	259.6	261.6	257.9	249.2
4.	239.8	233.3	264.9	283.5	288.2	285.5	275.9
10.	227.5	254.2	283.6	305.3	313.3	312.6	302.3
20.	236.9	266.9	294.6	317.3	327.3	328.2	317.7
40.	244.3	277.6	304.0	326.8	338.4	340.6	330.0
70.	249.2	285.2	310.7	333.1	345.7	348.8	338.2
100.	252.1	289.5	314.6	336.6	349.8	353.4	342.8
150.	255.0	294.1	318.7	340.3	353.9	358.0	347.3
200.	257.0	297.2	321.5	342.6	356.5	360.9	350.3

C

EPS	CHAMBER PRESSURE = 1000.0				ODE SPECIFIC IMPULSE		
1.	182.2	181.2	209.1	220.7	220.6	217.0	209.6
2.	191.7	213.5	244.2	259.7	262.2	258.7	250.0
4.	210.5	234.5	264.9	283.6	288.7	286.3	276.6
10.	228.0	255.4	283.8	305.3	313.6	313.2	302.9
20.	237.4	268.1	294.5	317.4	327.5	328.7	318.2
40.	244.7	278.8	304.3	326.5	338.6	341.0	330.4
70.	249.7	286.3	311.1	333.2	345.9	349.1	338.6
100.	252.5	290.7	315.0	336.7	349.9	353.7	343.1
150.	255.5	295.3	319.2	340.4	354.0	358.2	347.6
200.	257.5	298.3	322.0	342.8	356.6	361.2	350.5

C

EPS	CHAMBER PRESSURE = 3000.0				ODE SPECIFIC IMPULSE		
1.	148.1	185.1	209.2	221.4	223.1	220.0	212.4
2.	148.8	218.1	244.2	260.3	264.5	261.9	252.9
4.	213.3	239.2	265.0	283.9	290.6	289.3	279.4
10.	229.9	260.2	284.4	305.6	314.9	315.6	305.3
20.	239.1	272.8	295.9	317.6	328.6	330.6	320.1
40.	246.5	283.5	305.8	327.0	339.4	342.5	332.6
70.	251.5	291.0	312.7	333.4	346.6	350.4	339.9
100.	254.4	295.3	316.8	337.0	350.6	354.8	344.2
150.	257.4	299.5	321.1	340.8	354.6	359.3	348.6
200.	259.4	302.8	323.9	343.3	357.1	362.1	351.5

C ODK MIXTURE RATIOS

C THERE IS NO ODK DATA. SIMPLIFIED METHOD USED

C

MR=	0.0	0.5	1.0	1.5	2.0	2.3	2.8
PC	CHARACTERISTIC VELOCITY (FT/SEC)						
50.	4140.	4502.	5381.	5670.	5612.	5509.	5330.
500.	4185.	4650.	5380.	5714.	5734.	5644.	5454.
1000.	4204.	4678.	5380.	5717.	5748.	5662.	5471.
3000.	4280.	4779.	5379.	5728.	5805.	5735.	5538.

C

MR=	0.0	0.5	1.0	1.5	2.0	2.3	2.8
FC	COMBUSTION TEMPERATURE (DEG - R)						
50.	1787.	2386.	4224.	5215.	5513.	5529.	5463.
500.	2058.	2569.	4255.	5456.	5940.	5983.	5893.
1000.	2105.	2619.	4257.	5479.	6000.	6051.	5957.
3000.	2295.	2819.	4265.	5572.	6239.	6325.	6214.

C

C

ENL DATA

C

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C

Figure 6.3. Propellant Library (PROPLIB) Sheet 2 of 32)

C
C
C
C PROPELLANTS: MON-25/MHF-3

C ASSUMPTIONS ENTHALPY TEMP STATE
C MON-25
C MHF-3

C C-STAR & CHAMBER TEMP DATA EVALUATED AT ODE PC & ODE MR VALUES

C SIZE OF VARIOUS DATA ARRAYS

ODE PC	ODE MR	ODE EPS	ODK PC	ODK MR	ODK EPS
4	7	10	9	8	0

C ODE MIXTURE RATIO VALUES

MRE =	3.0	0.5	1.0	1.5	2.0	2.3	2.8
-------	-----	-----	-----	-----	-----	-----	-----

EPS	CHAMBER PRESSURE = 50.0				ODE SPECIFIC	IMPULSE
1.	157.8	179.8	212.2	215.8	216.4	212.5
2.	186.6	210.4	248.1	260.1	258.2	253.9
4.	205.2	230.5	269.2	284.8	285.8	281.7
10.	223.1	250.9	288.2	307.4	312.2	309.6
20.	232.5	263.3	298.6	319.8	327.1	326.2
40.	239.6	274.0	307.3	329.5	338.8	339.5
70.	244.4	281.5	313.4	335.9	346.5	348.3
100.	247.2	285.8	317.0	339.4	350.7	353.1
150.	254.1	290.4	320.9	343.0	355.0	358.0
200.	252.9	293.4	323.4	345.3	357.7	361.1

EPS	CHAMBER PRESSURE = 500.0				ODE SPECIFIC	IMPULSE
1.	163.6	183.5	212.5	222.6	221.6	218.0
2.	193.2	215.8	248.2	262.2	263.6	260.0
4.	211.3	236.6	269.4	286.4	290.5	287.7
10.	227.3	257.4	288.3	308.5	315.7	315.0
20.	236.0	270.0	299.2	320.6	329.8	330.6
40.	243.1	280.6	308.4	330.2	341.0	343.0
70.	248.0	288.1	314.9	336.5	348.3	351.2
100.	250.8	292.5	318.7	339.9	352.4	355.8
150.	253.7	297.0	322.8	343.5	356.4	360.3
200.	255.7	300.0	325.5	345.9	355.1	363.3

EPS	CHAMBER PRESSURE = 1000.0				ODE SPECIFIC	IMPULSE
1.	184.2	184.4	212.5	222.8	222.3	218.8
2.	193.7	216.9	248.2	262.4	264.2	260.8
4.	211.6	237.8	269.4	286.5	291.0	288.5
10.	227.6	258.6	288.4	308.5	316.1	315.6
20.	236.4	271.2	299.4	320.7	330.1	331.1
40.	243.5	281.8	308.7	330.2	341.2	343.4
70.	248.4	289.3	315.3	336.5	348.5	351.6

Figure 6.3. Propellant Library (PROBLIB) (Sheet 3 of 32)

C

PROLIB

100.	251.2	293.6	319.1	340.0	352.5	356.0	346.0
150.	214.2	298.2	323.2	343.6	356.6	360.6	350.6
200.	256.2	301.2	325.9	346.0	359.2	363.5	353.4

C

EPS	CHAMBER PRESSURE = 3000.0	ODE SPECIFIC IMPULSE					
1.	166.6	188.0	212.6	223.7	224.9	221.9	214.7
2.	195.5	221.3	248.3	263.0	266.6	264.0	255.5
4.	213.0	242.5	269.4	287.0	292.9	291.6	282.3
10.	228.9	263.4	288.8	308.9	317.5	318.1	308.2
20.	237.6	276.0	300.2	320.9	331.2	333.0	323.1
40.	245.1	286.6	309.9	330.4	342.1	345.0	335.0
70.	250.2	294.0	316.7	336.7	349.2	352.9	342.9
100.	255.1	298.3	320.7	340.3	353.2	357.2	347.2
150.	256.2	302.8	324.9	344.0	357.2	361.6	351.6
200.	258.2	305.7	327.7	346.5	359.7	364.4	354.4

C

ODK MIXTURE RATIOS

C THERE IS NO ODK DATA. SIMPLIFIED METHOD USED

C

MR =	0.5	0.5	1.0	1.5	2.0	2.3	2.8
PC	CHARACTERISTIC VELOCITY (FT/SEC)						
50.	4088.	4621.	5470.	5719.	5651.	5553.	5384.
500.	4237.	4724.	5470.	5772.	5777.	5690.	5511.
1000.	4250.	4749.	5470.	5775.	5792.	5709.	5528.
3000.	4304.	4849.	5470.	5789.	5852.	5783.	5596.

C

MR =	0.5	0.5	1.0	1.5	2.0	2.3	2.8
PC	COMBUSTION TEMPERATURE (DEG - R)						
50.	1799.	2554.	4365.	5274.	5546.	5564.	5509.
500.	2371.	2651.	4409.	5540.	5984.	6026.	5949.
1000.	2119.	2696.	4412.	5566.	6045.	6095.	6015.
3000.	2711.	2875.	4423.	5673.	6293.	6374.	6279.

C

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END DATA

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C

C PROPELLANTS: CLF5/MHF-3

ASSUMPTIONS	ENTHALPY	TEMP	STATE
CLF5			
MHF-3			

C-STAR & CHAMBER TEMP DATA EVALUATED AT ODE FC & CDE MR VALUE

Figure 6.3. Propellant Library (PROPLIB) (Sheet 4 of 32)

C
SIZE OF VARIOUS DATA ARRAYS
 ODE PC ODE MR ODE EPS ODK PC ODK MR ODK EPS
 4 5 10 0 0 0

C
ODE MIXTURE RATIO VALUES

MR= 0.0 1.0 2.0 3.0 4.0 5.0

C
EPS CHAMBER PRESSURE = 50.0 ODE SPECIFIC IMPULSE
 1. 157.8 217.5 223.9 223.3 213.9 201.4
 2. 186.6 256.5 266.9 267.0 253.8 239.3
 4. 205.2 279.7 294.6 295.7 279.1 264.7
 10. 223.1 300.2 320.7 323.0 304.4 290.4
 20. 232.5 311.1 334.8 338.0 319.4 306.1
 40. 239.6 319.4 345.6 349.5 331.7 319.3
 70. 244.4 324.8 352.4 357.2 340.1 328.4
 100. 247.2 327.8 356.0 361.5 345.0 333.5
 150. 250.1 331.0 359.5 366.0 350.0 338.9
 200. 252.0 333.2 361.7 368.9 353.4 342.4

C
EPS CHAMBER PRESSURE = 500.0 ODE SPECIFIC IMPULSE
 1. 163.6 218.4 227.8 228.4 217.7 207.5
 2. 193.2 257.1 271.0 272.6 258.0 246.6
 4. 211.3 280.1 298.3 301.1 283.9 272.4
 10. 227.3 300.6 323.4 327.2 309.3 298.1
 20. 236.0 311.5 336.9 341.4 324.3 313.5
 40. 243.1 320.0 347.1 352.7 336.6 326.2
 70. 248.0 325.7 353.6 360.3 345.0 335.0
 100. 250.8 329.0 357.1 364.5 349.9 340.0
 150. 253.7 332.4 360.5 368.7 354.9 345.3
 200. 255.7 334.6 362.6 371.4 358.2 348.7

C
EPS CHAMBER PRESSURE = 1000.0 ODE SPECIFIC IMPULSE
 1. 164.2 218.4 228.3 229.1 218.2 208.6
 2. 193.7 257.1 271.4 273.3 258.6 247.8
 4. 211.6 280.2 298.6 301.7 284.6 273.7
 10. 227.6 300.6 323.6 327.7 310.1 299.3
 20. 236.4 311.6 337.1 341.8 325.1 314.6
 40. 243.5 320.1 347.3 353.1 337.3 327.3
 70. 248.4 325.9 353.7 360.7 345.8 336.1
 100. 251.2 329.2 357.2 364.8 350.6 341.0
 150. 254.2 332.7 360.5 369.0 355.6 346.3
 200. 256.2 334.9 362.7 371.6 358.9 349.7

C
EPS CHAMBER PRESSURE = 3000.0 ODE SPECIFIC IMPULSE
 1. 164.6 218.6 230.0 231.8 220.2 212.9
 2. 195.5 257.2 273.1 276.2 261.1 252.6
 4. 213.0 280.3 300.0 304.2 287.4 278.6
 10. 228.9 300.8 324.6 329.5 313.0 304.2
 20. 237.8 311.9 337.8 343.6 328.1 319.2
 40. 245.1 320.8 347.8 354.9 340.4 331.7
 70. 250.2 326.8 354.2 362.3 348.8 340.3
 100. 253.1 330.2 357.6 366.3 353.5 345.1
 150. 256.2 333.8 360.9 370.3 358.4 350.2
 200. 258.2 336.1 363.0 372.8 361.6 353.4

C
ODK MIXTURE RATIOS

C THERE IS NO ODK DATA. SIMPLIFIED METHOD USED

C
MR= 0.0 1.0 2.0 3.0 4.0 5.0

Figure 6.3. Propellant Library (PROPLIB) (Sheet 5 of 32)

C
C
C
C



PC CHARACTERISTIC VELOCITY (FT/SEC)
50. 4088. 5552. 5852. 5848. 5584. 5231.
500. 4237. 5668. 5948. 5976. 5675. 5394.
1000. 425.. 5669. 5958. 5993. 5683. 5421.
3000. 4304. 5671. 5998. 6060. 5713. 5531.

C

MR= 0.0 1.0 2.0 3.0 4.0 5.0
PC COMBUSTION TEMPERATURE (DEG - R)
50. 1799. 4756. 5861. 6275. 6137. 5773.
500. 2171. 4838. 6226. 6738. 6578. 6251.
1000. 2119. 4845. 6273. 6808. 6663. 6353.
3000. 2311. 4872. 6459. 7088. 7004. 6762.

C

C END DATA

C

C

C

C

C PROPELLANTS: MON-25/60%MHF-3+40%AL

C

ASSUMPTIONS ENTHALPY TEMP STATE
MON-25
MHF-3
AL

C C STAR & CHAMBER TEMP DATA EVALUATED AT ODE FC & ODE MR VALUES

C

C

C

SIZE OF VARIOUS DATA ARRAYS

ODE PC	ODE MR	ODE EPS	ODK PC	ODK MR	ODK EPS
4	8	10	0	0	0

C

ODE MIXTURE RATIO VALUES

MR=	0.1	0.4	0.6	0.8	1.0	1.2	1.6	2.0
-----	-----	-----	-----	-----	-----	-----	-----	-----

C

EPS CHAMBER PRESSURE = 50.0 ODE SPECIFIC IMPULSE

1.	143.2	199.9	201.5	216.0	216.2	213.7	208.0	202.6
2.	230.3	240.1	242.1	258.2	258.4	255.7	249.0	242.6
4.	264.1	267.3	270.4	286.3	286.7	283.9	276.8	269.7
10.	277.5	293.7	299.6	315.1	315.1	312.5	305.3	297.6
20.	292.3	308.8	317.6	333.1	333.2	330.2	323.1	315.0
40.	315.1	322.2	332.5	347.9	348.7	345.9	338.5	330.2
70.	314.2	331.9	342.4	358.3	359.4	357.0	349.9	341.5
100.	319.4	337.7	348.1	364.1	365.5	363.3	356.6	348.1
150.	324.9	344.0	354.3	370.0	371.7	370.0	363.7	355.2
200.	328.4	348.2	358.4	373.9	375.7	374.3	368.5	360.0

Figure 6.3. Propellant Library (PROPLIB) (Sheet 6 of 32)

EPS CHAMBER PRESSURE = 500.0 ODE SPECIFIC IMPULSE
 1. 194.5 206.2 208.6 220.5 221.3 219.3 213.9 208.3
 2. 231.3 246.4 249.9 262.9 264.0 261.8 255.7 249.1
 4. 255.1 272.9 278.0 290.9 292.2 290.1 283.8 276.6
 10. 279.6 298.1 307.2 319.1 320.2 318.5 312.5 304.8
 20. 294.7 313.8 324.3 336.8 337.8 335.7 330.1 322.2
 40. 307.6 327.5 338.1 351.4 352.9 351.0 345.2 337.3
 70. 312.5 337.5 347.9 361.3 363.1 361.7 356.2 348.2
 100. 321.6 343.4 353.8 366.9 368.8 367.7 362.8 354.8
 150. 326.8 349.7 360.1 372.7 374.7 374.0 369.7 361.9
 200. 330.2 354.0 364.3 376.5 378.6 378.0 374.2 366.6

C

EPS CHAMBER PRESSURE = 1000.0 ODE SPECIFIC IMPULSE
 1. 194.5 206.9 209.6 221.1 222.0 220.0 214.7 209.1
 2. 231.3 247.0 251.1 263.5 264.7 262.5 256.6 250.0
 4. 255.7 273.4 279.0 291.4 292.9 290.8 284.8 277.6
 10. 279.9 298.7 308.1 319.5 320.8 319.2 313.4 305.7
 20. 295.1 314.5 325.0 337.2 338.3 336.3 331.0 323.2
 40. 307.9 328.3 338.8 351.8 353.3 351.5 346.0 338.3
 70. 316.8 338.3 348.7 361.6 363.5 362.1 357.0 349.1
 100. 321.9 344.2 354.6 367.2 365.2 368.2 363.6 355.7
 150. 327.1 350.5 360.9 373.0 375.0 374.4 370.4 362.8
 200. 330.5 354.8 365.2 376.7 378.8 378.4 374.9 367.5

C

EPS CHAMBER PRESSURE = 3000.0 ODE SPECIFIC IMPULSE
 1. 194.4 209.9 213.8 223.2 224.5 222.8 218.0 212.4
 2. 231.2 245.5 255.6 265.7 267.3 265.6 260.2 253.6
 4. 255.0 275.4 283.3 293.4 295.3 293.8 288.5 281.4
 10. 281.1 301.1 311.6 321.2 322.9 321.8 317.1 309.7
 20. 296.4 317.3 327.9 338.9 340.2 338.7 334.5 327.1
 40. 309.2 331.4 341.8 353.3 355.0 353.7 349.3 342.1
 70. 317.9 341.5 351.9 363.0 364.9 364.1 360.1 352.9
 100. 322.9 347.5 357.9 368.5 370.5 369.9 366.5 359.3
 150. 328.0 353.8 364.3 374.2 376.2 376.0 373.1 366.3
 200. 331.4 358.1 368.6 377.8 379.9 379.9 377.4 371.0

C

ODK MIXTURE RATIOS

C THERE IS NO ODK DATA. SIMPLIFIED METHOD USED

C

MR=	0.1	0.4	0.6	0.8	1.0	1.2	1.6	2.0
PC	CHARACTERISTIC VELOCITY (FT/SEC)							
50.	5053.	5240.	5264.	5648.	5653.	5591.	5442.	5301.
500.	5078.	5395.	5462.	5757.	5780.	5729.	5591.	5446.
1000.	5077.	5412.	5488.	5770.	5795.	5746.	5611.	5466.
3000.	5075.	5480.	5592.	5820.	5855.	5814.	5693.	5547.

C

MR=	0.1	0.4	0.6	0.8	1.0	1.2	1.6	2.0
PC	COMBUSTION TEMPERATURE (DEG - R)							
50.	4372.	4484.	4705.	5790.	6106.	6227.	6271.	6206.
500.	4542.	4944.	5084.	6224.	6655.	6836.	6932.	6852.
1000.	4654.	5019.	5176.	6283.	6733.	6926.	7037.	6956.
3000.	4798.	5317.	5545.	6515.	7044.	7286.	7457.	7370.

C

C

C

END DATA

Figure 6.3. Propellant Library (PROPLIB) (Sheet 7 of 32)

PROPELLANTS LIQUID OXYGEN - LIQUID HYDROGEN
ASSUMPTIONS:

	TEMP	ENTHALPY
LOX	90.18 K	-3093. CAL/MOL
LH ₂	20.27 K	-2154. CAL/MOL

ODK VALUES CORRESPOND TO THROAT RADIUS=2.289 IN.

C-STAR & CHAMBER TEMP DATA EVALUATED AT ODE PC & ODE MR VALUES

SIZE OF VARIOUS DATA ARRAYS

ODE PC	ODE MR	ODE EPS	ODK PC	ODK MR	ODK EPS
7	10	14	7	10	14

ODE MIXTURE RATIO VALUES

ODE MR:	0.1	2.	3.	4.	5.	6.	7.	8.	9.	10.
---------	-----	----	----	----	----	----	----	----	----	-----

EPS	CHAMBER PRESSURE = 20.0	ODE SPECIFIC IMPULSE
1.	104.6	302.1, 307.6, 301.0, 289.9, 278.1, 267.0, 257.6, 248.3, 240.7,
2.	119.7	351.4, 360.7, 356.7, 345.8, 332.7, 319.7, 306.8, 295.0, 284.0,
4.	127.5	379.4, 392.3, 391.3, 382.2, 369.3, 355.4, 342.0, 329.0, 318.2,
10.	133.9	403.3, 420.0, 422.7, 417.1, 406.0, 392.0, 377.9, 364.9, 353.4,
20.	137.0	415.5, 434.6, 439.7, 436.5, 427.7, 414.6, 399.9, 386.1, 373.7,
40.	139.3	424.4, 445.4, 452.6, 451.7, 445.2, 433.8, 418.9, 404.3, 391.0,
100.	141.1	432.7, 455.7, 465.2, 466.9, 463.1, 454.5, 440.5, 424.7, 410.0,
200.	142.2	437.2, 461.3, 472.1, 475.5, 473.6, 467.0, 454.4, 437.5, 421.6,
300.	142.6	439.2, 463.9, 475.4, 479.7, 478.7, 473.3, 461.5, 442.0, 427.2,
400.	142.8	440.4, 465.5, 477.5, 482.3, 482.0, 477.3, 466.5, 448.2, 431.2,
600.	143.2	442.0, 467.5, 480.0, 485.5, 486.1, 482.4, 472.7, 453.6, 436.0,
800.	143.5	442.8, 468.3, 481.5, 487.5, 488.6, 485.6, 476.7, 457.0, 439.0,
1000.	143.6	443.4, 469.1, 482.6, 488.9, 490.5, 488.0, 479.6, 459.5, 441.2,
5000.	144.1	445.9, 472.1, 486.9, 494.4, 497.7, 497.4, 491.8, 470.8, 449.5

EPS	CHAMBER PRESSURE = 40.0	ODE SPECIFIC IMPULSE
1.	104.6	302.2, 307.9, 302.4, 292.0, 280.5, 269.4, 258.0, 250.5, 243.0,
2.	119.7	351.4, 361.0, 357.9, 347.9, 335.3, 322.5, 309.0, 298.0, 288.5,
4.	127.5	379.4, 392.4, 392.1, 384.1, 372.0, 358.3, 344.0, 332.0, 320.5,
10.	133.9	403.3, 420.1, 423.3, 418.5, 408.4, 394.9, 380.5, 367.0, 355.0,
20.	137.0	415.5, 434.7, 440.1, 437.6, 429.7, 417.4, 402.5, 388.6, 375.8,
40.	139.3	424.4, 445.5, 452.9, 452.6, 446.8, 436.3, 421.6, 406.6, 393.0,
100.	141.1	432.7, 455.7, 465.4, 467.5, 464.3, 456.5, 443.0, 426.8, 411.8,
200.	142.2	437.3, 461.3, 472.3, 476.0, 474.6, 468.7, 456.2, 439.3, 423.0,
300.	142.6	439.2, 463.9, 475.6, 480.1, 479.6, 474.7, 463.5, 445.2, 428.8,
400.	142.8	440.4, 465.5, 477.6, 482.6, 482.8, 478.6, 468.3, 449.7, 432.3,
600.	143.2	442.0, 467.5, 480.1, 485.8, 486.7, 483.6, 474.5, 454.8, 437.0,
800.	143.5	442.8, 468.5, 481.6, 487.8, 489.3, 486.7, 478.5, 458.0, 440.0,

Figure 6.3. Propellant Library (PROPLIB) (Sheet 8 of 32)

1000. 143.6 443.4, 469.4, 482.7, 489.2, 491.1, 489.0, 481.2, 460.6, 442.0,
 3000. 144.1 445.9, 472.1, 486.9, 494.6, 498.1, 498.1, 493.5, 471.8, 450.4

C

EPS	CHAMBER PRESSURE = 100.0			ODE	SPECIFIC IMPULSE		
1.	104.6	302.2	308.3	304.0	294.6	283.6	272.7
2.	119.7	351.4	361.2	359.2	350.5	338.7	326.1
4.	127.5	379.4	392.6	393.1	386.3	375.2	362.1
10.	133.9	403.3	420.2	423.9	420.1	411.2	398.6
20.	137.0	425.5	434.7	440.6	438.9	432.0	420.8
40.	139.3	424.4	445.5	453.3	453.6	448.7	439.3
100.	141.1	432.7	455.7	465.7	468.2	465.7	458.9
200.	142.2	437.2	461.3	472.5	476.6	475.7	470.6
300.	142.6	439.2	463.9	475.7	480.6	480.6	476.5
400.	142.8	440.4	465.5	477.7	483.1	483.7	480.2
600.	143.2	442.0	467.5	480.2	486.2	487.5	485.0
800.	143.5	442.8	468.5	481.8	488.1	490.0	488.0
1000.	143.6	443.4	469.5	482.8	489.5	491.7	490.2
3000.	144.1	445.9	472.2	487.0	494.8	498.6	498.9
C							
1.	104.6	302.2	308.5	305.4	297.3	287.1	276.4
2.	119.7	351.4	361.3	360.3	353.0	342.4	328.0
4.	127.5	379.4	392.7	393.9	388.5	378.7	365.0
10.	133.9	403.3	420.3	424.4	421.6	414.1	402.5
20.	137.0	415.5	434.8	441.0	440.1	434.4	424.3
40.	139.3	424.4	445.5	453.6	454.5	450.6	442.5
100.	141.1	432.7	455.8	465.9	468.9	467.1	461.4
200.	142.2	437.2	461.3	472.7	477.1	476.8	472.6
300.	142.6	439.2	463.9	475.9	481.0	481.6	478.2
400.	142.8	440.4	465.5	477.9	483.5	484.6	481.9
600.	143.2	441.8	467.5	480.3	486.5	488.3	486.4
800.	143.5	442.7	468.7	481.9	488.4	490.7	489.3
1000.	143.6	443.3	469.5	482.9	489.8	492.4	491.4
3000.	144.1	445.1	472.0	487.1	495.0	499.0	499.8
C							
1.	104.6	302.2	308.6	305.9	298.4	288.6	278.1
2.	119.7	351.4	361.4	360.7	354.0	343.9	331.0
4.	127.5	379.4	392.7	394.1	389.3	380.2	366.3
10.	133.9	403.3	420.3	424.6	422.2	415.3	404.4
20.	137.0	415.5	434.8	441.1	440.5	435.3	425.8
40.	139.3	424.4	445.6	453.7	454.9	451.3	443.8
100.	141.1	432.7	455.8	466.0	469.2	467.7	462.4
200.	142.2	437.2	461.3	472.7	477.3	477.3	473.5
300.	142.6	439.3	463.9	475.9	481.2	482.0	478.8
400.	142.8	440.5	465.5	477.9	483.6	484.9	482.5
600.	143.2	441.9	467.5	480.4	486.7	488.6	487.0
800.	143.5	442.8	468.7	481.9	488.6	491.0	489.9
1000.	143.6	443.4	469.5	483.0	489.9	492.6	491.9
3000.	144.1	445.2	471.9	487.1	495.1	499.2	499.9
C							
1.	104.6	302.2	308.7	306.5	299.7	290.5	280.3
2.	119.7	351.4	361.4	361.3	355.2	345.7	332.6
4.	127.5	379.4	392.7	394.2	390.2	382.2	367.7
10.	133.9	403.3	420.3	424.7	422.8	416.6	406.6
20.	137.0	415.5	434.8	441.2	441.1	436.4	427.7
40.	139.3	424.4	445.6	453.9	455.3	452.2	445.4
100.	141.1	432.7	455.8	466.0	469.5	468.4	468.4
200.	142.2	437.2	461.3	472.8	477.5	477.8	474.5

Figure 6.3. Propellant Library (PROPLIB) (Sheet 9 of 32)

C

3000. 144.1 445.0 471.8 488.6 494.4 497.8 497.1 485.7 466.6 447.8
 C

EPS CHAMBER PRESSURE = 5000.0 ODK SPECIFIC IMPULSE
 1. 104.6 302.1 308.7 308.6 302.9 295.5 286.1 276.1 266.1 255.9
 2. 119.7 351.4 361.4 359.0 351.5 343.5 331.0 318.0 307.0 296.0
 4. 127.5 379.4 392.7 396.5 393.5 383.0 370.0 356.0 343.0 331.0
 10. 133.9 403.3 420.2 428.5 423.5 419.0 410.0 396.0 381.0 367.0
 20. 137.0 415.4 434.7 443.7 441.4 437.6 431.0 418.9 402.9 388.0
 40. 139.3 424.4 445.3 456.0 455.4 453.0 447.7 436.5 419.3 403.4
 100. 141.1 432.7 455.7 468.6 469.5 468.8 465.2 455.1 436.6 419.4
 200. 142.2 437.1 461.2 476.0 477.5 478.1 475.6 466.4 447.1 429.1
 300. 142.6 439.1 463.8 478.8 481.4 482.6 481.0 472.0 452.2 434.0
 400. 142.8 440.3 463.8 480.3 483.7 485.4 484.2 475.7 455.7 437.0
 600. 143.2 441.7 467.4 482.5 486.6 489.0 488.4 480.4 460.0 440.9
 800. 143.5 442.6 468.6 484.0 488.5 491.2 491.1 483.5 462.8 443.4
 1000. 143.6 443.2 469.4 485.2 489.8 492.8 493.0 485.6 464.8 445.2
 3000. 144.1 445.0 471.8 488.9 495.2 499.8 502.5 494.0 473.5 452.3
 C

C MR: .1 2. 3. 4. 5. 6. 7. 8. 9. 10.
 PC CHARACTERISTIC VELOCITY (FT/SEC)
 20. 2641. 7752. 7955. 7837. 7572. 7274. 6986. 6728. 6499. 6300.
 40. 2641. 7752. 7958. 7867. 7622. 7334. 7048. 6788. 6555. 6349.
 100. 2641. 7752. 7960. 7898. 7683. 7410. 7129. 6867. 6630. 6420.
 300. 2641. 7752. 7961. 7925. 7745. 7495. 7222. 6958. 6717. 6502.
 500. 2641. 7752. 7962. 7934. 7769. 7532. 7264. 6999. 6756. 6538.
 1000. 2641. 7752. 7762. 7943. 7798. 7578. 7318. 7054. 6806. 6584.
 5000. 2641. 7752. 7962. 7955. 7845. 7665. 7433. 7171. 6914. 6680.0
 C

C MR = 0.0 2. 3. 4. 5. 6. 7. 8. 9. 10.
 PC COMBUSTION TEMPERATURE
 20. 149. 3235. 4325. 4955. 5291. 5457. 5520. 5531. 5511. 5475.
 40. 149. 3236. 4354. 5039. 5417. 5605. 5678. 5689. 5668. 5626.
 100. 149. 3237. 4383. 5140. 5578. 5804. 5894. 5909. 5880. 5830.
 300. 149. 3238. 4407. 5240. 5759. 6042. 6161. 6179. 6143. 6080.
 500. 149. 3238. 4415. 5279. 5838. 6151. 6285. 6307. 6267. 6197.
 1000. 149. 3238. 4424. 5325. 5936. 6296. 6454. 6482. 6436. 6354.
 5000. 149. 3238. 4435. 5398. 6120. 6600. 6842. 6887. 6819. 6705.
 C

C COEFFICIENTS FOR THROAT RADIUS CORRECTION CORRELATION

C (DELTA KL/DELTA RT) = A + B * LN(KL REF)

C A = -0.2791 B = 1.2005 RTEF = 2.289

C

END DATA

C

C PROPELLANTS: LIQUID OXYGEN - RP1

C

C

C

C ASSUMPTIONS:

C LOX TEMP= 90.18 DEGREES KELVIN

C RP-1 TEMP= 298.15 DEGREES KELVIN

C LOX ENTHALPY= -3093. CAL/MOL

C

C

C

Figure 6.3. Propellant Library (PROPLIB) (Sheet 12 of 32)

RF-1 ENTHALPY = -6200. CAL/MOL

ODK DATA CORRESPONDS TO THROAT RADIUS OF 2.289 IN.

SIZE OF VARIOUS DATA ARRAYS

ODE PC	ODE MR	ODE EPS	ODE PC	ODE MR	ODE EPS
8	10	17	5	10	8

ODE MIXTURE RATIO VALUES

C	MR	0.22	1.0	2.0	2.4	2.6	2.8	3.0	3.2	3.5	10.0
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EPS CHAMBER PRESSURE = 20.0

ODE SPECIFIC IMPULSE

1.	122.9	168.8	219.9	216.8	215.0	212.6	210.3	208.0	204.3	166.7
2.	146.9	198.6	261.6	259.3	257.4	254.6	251.8	249.1	245.4	198.1
4.	162.8	215.5	288.3	287.7	286.1	283.2	280.2	277.2	273.2	218.0
10.	179.0	238.9	313.2	314.0	315.5	312.6	309.4	306.2	301.7	236.5
20.	189.0	251.6	327.1	334.2	333.5	330.9	327.7	324.4	319.6	246.7
40.	197.4	262.7	338.1	348.9	348.7	346.7	343.6	340.2	335.0	254.8
100.	207.0	275.6	349.6	363.2	364.9	364.4	361.8	358.5	353.3	262.9
200.	213.3	284.2	356.7	371.8	374.7	375.5	373.8	370.6	365.0	267.6
300.	216.7	288.8	369.3	375.7	379.7	381.2	380.1	377.2	371.5	269.8
400.	219.0	292.0	362.6	378.6	382.9	384.9	384.3	381.6	375.9	271.1
500.	220.6	294.3	364.3	380.6	385.2	387.5	387.3	384.8	379.1	272.2
600.	222.0	296.2	365.7	382.3	387.1	389.6	389.8	387.5	381.8	273.0
800.	224.0	299.1	367.7	384.9	389.8	392.7	393.3	391.4	385.8	274.1
1000.	225.5	301.2	369.3	386.8	391.8	395.0	395.9	394.4	390.4	274.9
1500.	228.2	305.0	371.9	389.5	394.9	398.5	399.9	399.1	394.8	276.2
2000.	230.0	307.6	373.8	391.5	397.2	401.0	402.8	402.3	397.9	277.0
3000.	232.4	311.1	376.4	394.2	400.3	404.5	406.8	407.0	402.3	277.9

EPS CHAMBER PRESSURE = 40.0

ODE SPECIFIC IMPULSE

1.	123.3	169.6	221.4	214.2	217.1	214.7	212.3	210.0	206.7	167.5
2.	147.3	199.9	263.1	261.7	259.7	257.0	254.2	251.5	247.6	198.8
4.	163.3	220.0	289.5	290.3	288.5	285.6	282.6	279.7	275.4	218.5
10.	179.5	240.6	314.0	319.0	317.8	315.1	312.0	308.8	304.1	236.8
20.	189.5	253.4	327.8	336.0	335.7	333.4	330.2	326.9	322.0	247.0
40.	198.0	264.6	338.7	350.0	350.6	349.1	346.1	342.8	337.7	255.0
100.	207.6	277.5	350.1	363.8	366.4	366.5	364.3	361.0	355.7	263.1
200.	213.9	286.1	357.0	372.1	376.0	377.3	376.1	373.1	367.7	267.7
300.	217.3	290.7	360.6	376.5	380.9	382.8	382.3	379.6	374.1	269.9
400.	219.6	293.9	362.9	379.3	384.0	386.4	386.3	384.0	378.5	271.3
500.	221.2	296.2	364.6	381.3	386.3	388.9	389.2	387.2	381.7	272.3
600.	222.6	298.1	366.0	383.0	388.1	391.0	391.6	389.8	384.3	273.1
800.	224.6	301.0	368.1	385.5	390.8	394.0	395.0	393.7	388.3	274.2
1000.	226.1	303.2	369.6	387.1	392.7	396.2	397.5	396.5	391.3	275.0
1500.	228.8	306.9	372.3	389.9	395.8	399.6	401.4	401.0	396.2	276.2
2000.	230.6	309.5	374.1	392.0	397.9	402.0	404.1	404.2	399.6	277.0
3000.	233.9	312.9	376.8	394.8	401.0	405.4	408.0	408.7	404.5	278.0

EPS CHAMBER PRESSURE = 100.0 ODE SPECIFIC IMPULSE

1.	124.4	171.0	223.3	221.4	219.7	217.4	215.0	212.7	209.3	168.3
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Figure 6.3. Propellant Library (PROPLIB) (Sheet 13 of 32)

400.	146.2	248.2	339.0	343.8	341.6	340.2	338.7	335.6	332.4	265.5
500.	147.2	250.2	340.0	345.0	342.8	341.5	340.0	336.9	333.7	266.5
600.	148.2	251.8	340.8	346.0	343.8	342.5	341.0	337.9	334.7	267.2
800.	149.5	254.2	341.8	347.3	345.2	343.9	342.5	339.4	336.2	268.2

C
EPS CHAMBER PRESSURE = 300.
 40. 134.6 230.0 337.1 350.3 348.9 347.7 346.3 343.0 339.5 255.1
 100. 141.6 241.1 347.0 363.7 362.8 361.6 360.3 357.0 353.4 263.0
 200. 145.2 248.4 352.5 371.6 371.1 370.1 368.8 365.5 361.9 267.7
 300. 147.2 252.3 355.1 375.6 375.3 374.3 373.0 369.8 366.2 269.8
 400. 149.1 254.9 356.8 378.1 378.0 377.1 375.8 372.6 368.9 271.2
 500. 150.2 257.0 357.9 379.9 379.9 379.0 377.8 374.6 370.9 272.1
 600. 151.1 258.5 358.8 381.3 381.4 380.5 379.3 376.1 372.5 272.9
 800. 152.4 261.0 360.1 383.3 383.6 382.8 381.6 378.4 374.7 273.9

C
EPS CHAMBER PRESSURE = 500.
 40. 135.0 231.5 338.1 353.3 352.4 351.3 350.0 346.8 343.3 255.4
 100. 141.6 242.4 347.9 366.9 366.7 365.8 364.5 361.3 357.7 263.3
 200. 145.8 249.7 353.5 375.1 375.4 374.6 373.4 370.2 366.6 267.8
 300. 148.1 253.6 356.1 379.1 379.7 379.0 377.9 374.7 371.1 270.0
 400. 149.6 256.3 357.8 381.7 382.5 381.9 380.8 377.7 374.0 271.4
 500. 150.6 258.3 359.0 383.6 384.5 383.9 382.8 379.8 376.1 272.3
 600. 151.6 259.8 359.8 385.0 386.1 385.5 384.5 381.4 377.7 273.1
 800. 153.0 262.2 361.1 387.1 388.4 387.9 386.9 383.9 380.2 272.2

C
EPS CHAMBER PRESSURE = 1000.
 40. 135.7 233.3 338.2 356.2 356.2 355.4 354.2 351.1 347.6 255.6
 100. 142.2 244.3 348.6 370.0 370.9 370.4 369.3 366.3 362.8 263.4
 200. 146.5 251.6 354.2 378.3 379.9 379.6 378.6 375.7 372.1 268.0
 300. 148.8 255.5 356.8 382.4 384.4 384.2 383.4 380.5 376.9 270.2
 400. 150.2 258.1 358.5 385.0 387.3 387.2 386.4 383.6 380.0 271.5
 500. 151.4 260.1 359.6 386.9 389.4 389.4 388.6 385.9 382.2 272.5
 600. 152.3 261.7 360.5 388.4 391.1 391.1 390.4 387.6 384.0 273.3
 800. 153.7 264.1 361.9 390.5 393.5 393.6 392.9 390.2 386.6 274.3

C
EPS CHAMBER PRESSURE = 5000.
 40. 137.0 237.7 339.3 359.5 361.3 361.3 360.8 358.3 354.9 255.8
 100. 143.6 248.6 349.1 373.1 376.1 376.8 376.7 374.7 371.3 263.7
 200. 147.9 255.9 354.6 381.2 385.2 386.2 386.5 384.9 381.6 268.2
 300. 150.1 259.8 357.2 385.3 389.7 391.0 391.5 390.2 386.8 270.3
 400. 151.7 262.4 358.9 387.9 392.7 394.1 394.8 393.6 390.2 271.7
 500. 152.8 264.3 360.0 389.7 394.8 396.4 397.1 396.1 392.8 272.7
 600. 153.7 265.9 360.9 391.2 396.4 398.1 399.0 398.0 394.7 273.4
 800. 155.0 268.2 362.2 393.3 398.9 400.7 401.7 400.5 397.6 274.5

C
C MR = .22 1.0 2.0 2.4 2.6 2.8 3.0 3.2 3.5 10.
PC CHARACTERISTIC VELOCITY (FT/SEC)
 20. 2150. 4336. 5736. 5668. 5625. 5564. 5502. 5443. 5359. 4348.
 40. 2150. 4363. 5771. 5721. 5676. 5615. 5554. 5494. 5409. 4365.
 100. 2150. 4408. 5812. 5788. 5743. 5684. 5622. 5562. 5475. 4383.
 300. 2150. 4471. 5853. 5868. 5822. 5764. 5703. 5642. 5554. 4401.
 500. 2150. 4502. 5868. 5900. 5857. 5801. 5740. 5679. 5591. 4407.
 1000. 2150. 4545. 5884. 5940. 5904. 5850. 5790. 5729. 5639. 4415.
 2000. 2150. 4588. 5909. 5977. 5940. 5887. 5832. 5765. 5677. 4588.
 5000. 2150. 4645. 5910. 6020. 6002. 5958. 5902. 5841. 5749. 4427.

C
C MR = .22 1.0 2.0 2.4 2.6 2.8 3.0 3.2 3.5 10.
PC COMBUSTION TEMPERATURE
 20. 2140. 2505. 5374. 5594. 5632. 5646. 5646. 5639. 5619. 4736.
 40. 2140. 2524. 5495. 5752. 5795. 5812. 5813. 5806. 5785. 4808.

Figure 6.3. Propellant Library (PROPLIB) (Sheet 16 of 32)

C

100.	2140.	2566.	5651.	5965.	6019.	6040.	6044.	6037.	6011.	4896.
300.	2140.	2652.	5826.	6224.	6297.	6328.	6334.	6326.	6298.	4990.
500.	2140.	2706.	5899.	6344.	6428.	6464.	6473.	6466.	6434.	5028.
1000.	2140.	2793.	5989.	6506.	6608.	6653.	6666.	6659.	6625.	5075.
2000.	2140.	2895.	6067.	6663.	6785.	6843.	6861.	6856.	6822.	5116.
5000.	2140.	3050.	6150.	6859.	7019.	7098.	7124.	7122.	7086.	5162.

C

C COEFFICIENTS FOR THROAT RADIUS CORRECTION CORRELATION
(DELTA KL/DELTA RT) = A + B * LN(KL REF)

A = -1.1543 B = 1.7378 RTREF = 2.289

C

C

C

END DATA

C

C

C

C

C

C

PROPELLANTS: LIQUID OXYGEN - METHANE

C

C

C

C

C

ASSUMPTIONS:

C

	TEMP	ENTHALPY
LOX	90.18 K	-3090. CAL/MOL
CH4	111.64 K	-21370. CAL/MOL

ODK VALUES CORRESPOND TO THROAT RADIUS = 7.07 IN

C

C

C

C

C

SIZE OF VARIOUS DATA ARRAYS

ODE PC	ODE MR	ODE EPS	ODK PC	ODK MR	ODK EPS
7	10	17	7	10	17

C

C

C

ODE MIXTURE RATIO VALUES

C	MR	0.6	2.0	2.5	3.0	3.4	3.5	3.6	3.8	4.0	4.5
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C

EPS	CHAMBER PRESSURE = 20.0				ODE SPECIFIC IMPULSE						
1.	149.8	222.5	228.4	225.0	220.5	219.3	218.2	216.0	213.8	208.8	
2.	178.7	261.4	271.7	269.2	264.1	262.7	261.4	258.7	256.2	250.1	
4.	198.0	285.0	299.4	298.9	293.7	292.3	290.8	287.9	285.1	278.3	
10.	217.3	306.6	325.4	328.6	324.2	322.7	321.1	318.0	314.9	307.4	

C

C

C

Figure 6.3. Propellant Library (PROPLIB) (Sheet 17 of 32)

1000.	197.3	343.0	377.0	398.1	406.9	407.6	407.0	405.2	402.4	391.2
1500.	199.3	344.0	378.9	400.0	409.0	409.8	409.3	407.5	404.7	393.5
2000.	200.6	344.7	379.8	401.3	410.6	411.3	410.9	409.0	406.3	395.0
3000.	202.4	345.4	381.1	403.2	412.7	413.5	413.1	411.3	408.5	397.2

S CHAMBER PRESSURE = 5000.
 1. 111.7 224.0 235.4 236.8 236.7 236.3 235.6 233.9 232.0 226.1
 2. 153.2 262.4 277.9 280.2 280.1 275.6 278.8 277.0 274.8 267.8
 4. 147.3 285.4 304.3 307.3 307.1 306.6 305.9 304.1 301.9 294.2
 10. 181.4 305.9 328.7 339.1 342.1 342.0 341.0 338.6 335.8 327.0
 20. 169.9 316.8 342.2 353.7 356.8 356.7 355.8 353.6 350.8 341.6
 40. 177.2 325.0 352.7 366.2 371.0 371.2 370.6 368.9 366.3 356.3
 100. 185.7 332.9 362.2 379.1 386.0 386.6 386.5 385.4 383.1 372.2
 200. 190.1 337.1 369.1 386.7 395.0 395.9 396.2 395.6 393.6 382.0
 300. 192.7 339.1 372.0 390.4 399.5 400.6 401.1 400.8 398.9 387.0
 400. 194.8 340.4 373.8 392.8 402.5 403.7 404.3 404.2 402.4 390.3
 500. 196.1 341.2 375.0 394.5 404.6 405.8 406.6 406.6 404.9 392.6
 600. 198.8 341.9 376.0 395.8 406.2 407.6 408.4 408.6 406.9 394.4
 800. 198.1 342.8 377.6 397.7 408.6 410.1 411.0 411.4 409.8 397.2
 1000. 199.5 343.5 378.0 399.1 410.4 411.9 412.5 413.4 411.9 399.1
 1500. 201.4 344.5 379.9 401.0 412.5 414.1 415.2 415.7 414.2 401.4
 2000. 202.7 345.2 380.8 402.3 414.1 415.7 416.8 417.4 415.9 402.9
 3000. 204.3 345.9 382.1 404.2 416.2 417.9 419.0 419.7 418.2 405.2

C

C MR = 0.6 2.0, 2.5, 3.0, 3.4, 3.5, 3.6, 3.8, 4.0, 4.5

PC CHARACTERISTIC VELOCITY (FT/SEC)
 20. 3911. 5759. 5960. 5886. 5771. 5741. 5711. 5653. 5597. 5465.
 40. 3946. 5762. 5989. 5933. 5821. 5791. 5761. 5703. 5646. 5512.
 100. 3992. 5766. 6027. 5995. 5887. 5858. 5828. 5769. 5711. 5575.
 200. 4090. 5768. 6082. 6117. 6030. 6002. 5974. 5915. 5855. 5720.
 300. 4169. 5768. 6073. 6092. 5995. 5971. 5942. 5882. 5823. 5683.
 400. 4190. 5768. 6086. 6129. 6045. 6017. 5989. 5930. 5870. 5737.
 500. 4163. 5768. 6085. 6200. 6140. 6119. 6090. 6032. 5974. 5825.

C

C MR = 0.6 2.0, 2.5, 3.0, 3.4, 3.5, 3.6, 3.8, 4.0, 4.5

PC COMBUSTION TEMPERATURE (DEG - R)
 20. 1627. 4484. 5199. 5441. 5495. 5500. 5502. 5500. 5453. 5463.
 40. 1665. 4501. 5259. 5526. 5586. 5591. 5594. 5592. 5584. 5552.
 100. 1780. 4553. 5440. 5779. 5857. 5865. 5868. 5867. 5858. 5819.
 200. 1867. 4573. 5541. 5949. 6048. 6058. 6061. 6062. 6053. 6007.
 300. 1953. 4593. 5642. 6118. 6238. 6250. 6254. 6256. 6247. 6195.
 1000. 2033. 4603. 5712. 6260. 6404. 6418. 6425. 6429. 6418. 6361.
 5000. 2227. 4618. 5835. 6562. 6789. 6814. 6827. 6836. 6826. 6752.

C

C COEFFICIENTS FOR THROAT RADIUS CORRECTION CORRELATION

(DELTA KL/LELTA RT) = A + B * LN(KL REF)

A = -1.1576 B = 1.7368 RTREF = 7.07

C

C

C

END DATA

C

C

C

Figure 6.3. Propellant Library (PROPLIB) (Sheet 22 of 32)

C PROPELLANTS: LIQUID FLORINE - LIQUID HYDROGEN

C ASSUMPTIONS

	ENTHALPY	TEMP	STATE
F2	-3056. CAL/MOLE	84.7 K	LIQ
H2	-2154. CAL/MOLE	20.27 K	LIQ

C ODK VALUES FOR THROAT RADIUS = 2.289 INCH

C C-STAR & CHAMBER TEMP DATA EVALUATED AT ODE PC & ODE MR VALUES

C SIZE OF VARIOUS DATA ARRAYS

ODE PC	ODE MR	ODE EPS	ODK PC	ODK MR	ODK EPS
6	10	16	6	10	16

C ODE MIXTURE RATIO VALUES

MR= 1.0	2.0	4.0	6.0	8.0	10.0	12.0	14.0	16.0	20.0
---------	-----	-----	-----	-----	------	------	------	------	------

EPS	CHAMBER PRESSURE = 40.0	ODE SPECIFIC IMPULSE
1.	102.3	306.5
2.	117.0	353.9
4.	124.6	380.0
10.	130.9	401.7
20.	133.9	412.5
40.	136.0	420.3
70.	137.2	425.0
100.	137.9	427.4
150.	138.5	429.8
200.	138.9	431.2
300.	139.4	432.9
400.	139.6	434.0
600.	139.9	435.2
800.	140.1	436.0
1000.	140.2	436.5
3000.	140.4	438.5

EPS	CHAMBER PRESSURE = 100.0	ODE SPECIFIC IMPULSE
1.	102.3	306.5
2.	117.0	354.0
4.	124.6	380.0
10.	130.9	401.7
20.	133.9	412.5
40.	136.0	420.3
70.	137.2	425.0
100.	137.9	427.4
150.	138.5	429.8
200.	138.9	431.2
300.	139.4	432.9
400.	139.6	434.0

Figure 6.3. Propellant Library (PROPLIB) (Sheet 23 of 32)

10.	130.9	401.6	434.6	440.5	439.7	437.5	435.4	433.5	431.0	418.3
20.	133.9	412.5	447.4	454.8	454.9	453.4	451.8	450.5	448.9	435.5
40.	136.0	420.3	456.7	465.1	466.0	465.0	463.8	463.0	462.2	448.2
70.	137.2	424.9	462.3	471.3	472.8	472.1	471.2	470.6	470.3	456.1
100.	137.9	427.4	465.2	474.6	476.3	475.8	475.0	474.6	474.6	460.1
150.	138.5	429.6	468.0	477.7	479.6	479.3	478.7	478.4	478.7	464.0
200.	138.9	431.0	469.7	479.6	481.7	481.5	480.9	480.7	481.1	466.4
300.	139.4	432.5	471.8	481.9	484.2	484.1	483.6	483.5	484.1	469.3
400.	139.6	433.4	473.1	483.3	485.7	485.7	485.2	485.2	485.9	471.0
600.	139.9	434.5	474.6	485.0	487.6	487.6	487.2	487.3	488.2	473.1
800.	140.1	435.2	475.5	486.1	488.7	488.8	488.5	488.6	489.5	474.4
1000.	140.2	435.6	476.2	486.8	489.5	489.6	489.3	489.4	490.4	475.3
3000.	140.4	437.0	478.6	489.6	492.4	492.7	492.4	492.7	493.9	478.6
C										

EPS	CHAMBER PRESSURE = 500.0	ODK SPECIFIC IMPULSE
1.	102.3	306.4
2.	117.0	353.9
4.	124.6	380.0
10.	130.9	401.6
20.	133.9	412.5
40.	136.0	420.3
70.	137.2	425.0
100.	137.9	427.4
150.	138.5	429.6
200.	138.9	431.0
300.	139.4	432.5
400.	139.6	433.5
600.	139.9	434.5
800.	140.1	435.2
1000.	140.2	435.6
3000.	140.4	437.0

EPS	CHAMBER PRESSURE = 1000.0	ODK SPECIFIC IMPULSE
1.	102.3	306.4
2.	117.0	353.9
4.	124.6	380.0
10.	130.9	401.6
20.	133.9	412.5
40.	136.0	420.3
70.	137.2	425.0
100.	137.9	427.4
150.	138.5	429.6
200.	138.9	431.0
300.	139.4	432.5
400.	139.6	433.5
600.	139.9	434.5
800.	140.1	435.2
1000.	140.2	435.6
3000.	140.4	437.1

EPS	CHAMBER PRESSURE = 5000.0	ODK SPECIFIC IMPULSE
1.	102.3	306.5
2.	117.0	354.0
4.	124.6	380.0
10.	130.9	401.7
20.	133.9	412.5
40.	136.0	420.3
70.	137.2	425.0
100.	137.9	427.4
150.	138.5	429.8

Figure 6.3. Propellant Library (PROPLIB) (Sheet 26 of 32)

200.	138.9	431.2	472.2	487.6	495.0	498.8	500.8	501.8	502.3	485.8
300.	139.4	432.9	474.3	490.0	497.6	501.6	503.9	505.1	505.7	493.1
400.	139.6	434.0	475.6	491.4	499.2	503.4	505.7	507.1	507.8	495.1
600.	139.9	435.2	477.1	493.2	501.2	505.5	508.0	509.5	510.4	497.5
800.	140.1	436.0	478.1	494.3	502.4	506.8	509.4	511.0	512.0	499.0
1000.	140.2	436.5	478.7	495.1	503.2	507.8	510.4	512.0	513.1	500.1
3000.	140.4	438.5	481.2	497.9	506.4	511.2	514.1	515.9	517.2	504.0
C										
C MR =	0.1	2.0	4.0	6.0	8.0	10.0	12.0	14.0	16.0	20.0
PC	CHARACTERISTIC VELOCITY (FT/SEC)									
40.	2583.	7820.	8372.	8247.	8067.	7941.	7854.	7758.	7657.	7410.
100.	2583.	7820.	8390.	8322.	8165.	8046.	7962.	7877.	7770.	7525.
300.	2583.	7820.	8402.	8400.	8275.	8169.	8088.	8008.	7906.	7663.
500.	2583.	7820.	8406.	8431.	8322.	8223.	8146.	8067.	7969.	7727.
1000.	2583.	7820.	8409.	8468.	8381.	8293.	8221.	8147.	8053.	7814.
5000.	2583.	7820.	8412.	8527.	8495.	8438.	8382.	8321.	8240.	8008.
C										
C MR =	0.1	2.0	4.0	6.0	8.0	10.0	12.0	14.0	16.0	20.0
PC	COMBUSTION TEMPERATURE (DEG - R)									
40.	142.	3063.	4916.	5732.	6246.	6662.	7013.	7266.	7417.	7527.
100.	142.	3063.	5002.	5927.	6503.	6955.	7327.	7597.	7763.	7883.
300.	142.	3063.	5086.	6151.	6815.	7321.	7725.	8021.	8206.	8339.
500.	142.	3063.	5118.	6250.	6960.	7494.	7918.	8227.	8423.	8563.
1000.	142.	3063.	5154.	6376.	7153.	7732.	8184.	8515.	8727.	8877.
5000.	142.	3064.	5210.	6623.	7571.	8272.	8811.	9207.	9467.	9646.
C										

C COEFFICIENTS FOR ODK THROAT RADIUS CORRECTION CORRELATION
C ($\Delta KL/\Delta RT$) = $A + B * \ln(REF KL)$

A = -0.2791 B = 1.2005 RTREF = 2.289

C
END DATA

C
C
C
C
C
C
C
C
C
C
C
C
C
C
C
C

C PROPELLANT: LIQUID FLORINE - LIQUID HYDRAZINE

C ASSUMPTIONS: ENTHAPLY TEMP STATE
C F2 -3056. CAL MOLE 84.7 K LIQ
C N2H4 12054. CAL MOLE 298.16K LIQ

C MONO-PROPELLANT, MR=0.0, DATA FROM TRAM 72 RUNS
C ODK VALUES CORRESPOND TO A THROAT RADIUS OF 2.289 INCHES

Figure 6.3. Propellant Library (PROPLIB) (Sheet 27 of 32)

SIZE OF VARIOUS DATA ARRAYS

	ODE PC	ODE MR	ODE EPS	ODE PC	ODE MR	ODE EPS
	6	9	16	6	9	16

ODE MIXTURE RATIO VALUES

C MR	0.0	1.0	1.4	1.8	2.0	2.2	2.4	3.0	E.0
------	-----	-----	-----	-----	-----	-----	-----	-----	-----

EPS	CHAMBER PRESSURE = 40.0				ODE SPECIFIC IMPULSE				
1.	201.5	260.1	265.4	268.3	268.1	267.1	265.6	259.5	213.6
2.	232.4	307.8	314.7	318.8	319.2	318.3	316.6	308.7	245.2
4.	250.5	337.4	346.3	351.5	352.7	352.3	350.5	340.0	263.0
10.	268.0	363.6	376.2	383.1	385.1	385.8	384.4	367.1	280.1
20.	278.5	377.1	392.4	401.0	403.7	405.3	404.6	380.7	290.5
40.	287.5	387.0	404.4	414.8	418.2	420.6	420.6	390.6	299.5
70.	293.9	393.1	411.8	423.4	427.4	430.3	430.6	396.7	306.0
100.	297.6	396.2	415.7	427.9	432.2	435.4	435.9	400.2	309.8
150.	301.8	399.3	419.4	432.3	436.9	440.5	441.1	403.7	313.8
200.	304.3	401.1	421.7	435.0	439.8	443.6	444.3	406.1	316.6
300.	308.0	403.4	424.5	438.2	443.3	447.3	448.2	409.2	320.2
400.	310.2	404.8	426.2	440.2	445.4	449.6	450.6	411.3	322.6
600.	313.4	406.5	428.3	442.7	448.1	452.5	453.5	414.1	325.9
800.	315.6	407.5	429.6	444.2	449.7	454.2	455.3	415.9	328.1
1000.	317.2	408.2	430.5	445.2	450.8	455.4	456.6	417.3	329.7
3000.	324.5	410.9	433.8	449.2	455.0	460.0	461.5	422.9	336.9

EPS	CHAMBER PRESSURE = 100.0				ODE SPECIFIC IMPULSE				
1.	201.7	262.9	268.8	271.9	271.9	271.0	269.5	263.2	213.6
2.	232.9	310.4	318.2	322.7	323.3	322.6	321.0	312.5	245.4
4.	251.5	339.5	349.6	355.3	356.6	356.5	354.9	343.0	263.6
10.	269.5	365.0	378.7	386.4	388.7	389.7	388.6	368.9	281.2
20.	280.3	378.1	394.3	403.7	406.7	408.6	408.3	382.0	291.9
40.	289.5	387.8	405.8	416.8	420.6	432.2	432.4	391.6	301.1
70.	296.0	393.7	412.9	425.0	429.2	432.4	432.9	397.7	307.7
100.	299.8	396.7	416.7	429.3	433.8	437.3	437.9	401.1	311.5
150.	304.1	399.7	420.3	433.4	438.2	442.0	442.8	404.7	315.6
200.	306.6	401.5	422.5	436.0	441.0	444.9	445.8	407.1	318.3
300.	310.3	403.7	425.1	439.1	444.3	448.5	449.4	410.3	322.0
400.	312.6	405.0	426.8	441.0	446.3	450.7	451.7	412.4	324.4
600.	315.8	406.7	428.8	443.3	448.8	453.4	454.4	415.1	327.7
800.	318.0	407.7	430.0	444.8	450.4	455.0	456.2	417.0	329.9
1000.	319.6	408.4	430.8	445.8	451.4	456.1	457.4	418.3	331.5
3000.	327.0	411.0	434.1	449.5	455.4	460.4	462.0	423.6	338.5

EPS	CHAMBER PRESSURE = 300.0				ODE SPECIFIC IMPULSE				
1.	202.1	265.8	272.5	276.1	276.4	275.7	274.3	267.6	213.7
2.	235.9	313.1	322.0	327.1	328.0	327.6	326.1	316.7	245.7
4.	253.2	341.5	353.0	359.5	361.2	361.5	360.1	346.0	264.6
10.	271.9	366.3	381.3	389.9	392.5	394.0	393.3	370.8	282.8

Figure 6.3. Propellant Library (PROPLIB) (Sheet 28 of 32)

20.	283.0	379.1	396.2	406.4	409.8	412.1	412.1	383.4	293.8
40.	292.4	388.5	407.2	418.9	422.9	426.0	426.3	392.7	303.2
70.	295.0	394.2	414.1	426.6	431.1	434.6	435.2	398.8	309.9
100.	302.9	397.2	417.6	430.7	435.4	439.2	439.9	402.3	313.8
150.	307.2	400.1	421.1	434.6	439.6	443.6	444.5	405.9	317.9
200.	309.7	401.9	423.2	437.0	442.2	446.4	447.3	408.3	320.7
300.	313.5	404.0	425.7	440.0	445.3	449.7	450.7	411.5	324.3
400.	315.8	405.3	427.3	441.8	447.3	451.8	452.8	413.6	326.7
600.	319.0	406.9	429.2	444.0	449.6	454.3	455.4	416.3	330.0
800.	321.2	407.9	430.4	445.4	451.0	455.8	457.1	418.1	332.1
1000.	322.8	408.6	431.2	446.3	452.0	456.9	458.2	419.4	333.7
3000.	331.7	411.1	434.3	449.8	455.8	460.9	462.6	424.3	340.2

C	EPS	CHAMBER PRESSURE = 500.0				ODE	SPECIFIC	IMPULSE	
1.	202.5	267.0	274.2	278.0	278.4	277.8	276.5	269.5	213.8
2.	234.7	314.1	323.7	329.0	330.1	329.9	328.5	318.4	246.0
4.	254.3	342.3	354.5	361.3	363.2	363.7	362.4	347.1	265.1
10.	273.2	366.8	382.3	391.3	394.2	395.8	395.3	371.5	283.7
20.	284.4	379.5	397.0	407.5	411.1	413.6	413.7	383.9	294.8
40.	293.9	388.8	407.8	419.7	423.9	427.1	427.5	393.2	304.3
70.	300.6	394.4	414.5	427.3	431.9	435.5	436.2	399.3	311.0
100.	304.4	397.4	418.0	431.3	436.1	439.9	440.7	402.8	314.9
150.	308.7	400.2	421.7	435.1	440.2	444.3	445.2	406.5	319.1
200.	311.3	402.0	423.4	437.5	442.7	446.9	447.9	408.9	321.8
300.	315.1	404.1	426.0	440.4	445.8	450.2	451.2	412.1	325.4
400.	317.4	405.4	427.5	442.1	447.6	452.2	453.3	414.1	327.9
600.	320.6	407.2	429.4	444.3	449.9	454.6	455.9	416.9	331.1
800.	322.4	408.0	430.5	445.6	451.3	456.1	457.5	418.6	333.2
1000.	324.4	408.6	431.3	446.5	452.3	457.2	458.6	419.8	334.7
3000.	331.7	411.2	434.4	450.0	456.0	461.1	462.8	424.6	341.0

C	EPS	CHAMBER PRESSURE = 1000.0	ODE	SPECIFIC	IMPULSE
1.	203.2	268.5	276.3	280.5	281.1
2.	235.9	315.4	325.8	331.6	332.9
4.	255.9	343.2	356.2	363.6	365.7
10.	275.1	367.4	383.5	393.1	396.2
20.	286.5	379.9	397.9	408.9	412.7
40.	296.1	389.1	408.5	420.7	425.1
70.	302.8	394.7	415.0	428.1	432.8
100.	306.7	397.6	418.4	431.9	436.9
150.	311.0	400.4	421.8	435.7	440.9
200.	313.6	402.1	423.8	438.0	443.3
300.	317.3	404.2	426.2	440.8	446.3
400.	319.6	405.5	427.8	442.5	448.1
600.	322.9	407.1	429.6	444.6	450.3
800.	325.1	408.1	430.7	445.9	451.7
1000.	326.7	408.7	431.5	446.8	452.6
3000.	333.9	411.2	434.5	450.1	456.2

C	EPS	CHAMBER PRESSURE = 5000.0	ODE	SPECIFIC	IMPULSE
1.	206.1	271.1	280.6	285.7	286.8
2.	240.0	317.4	329.7	336.7	338.7
4.	260.7	344.7	359.4	368.1	370.8
10.	280.5	368.3	385.7	396.3	400.0
20.	292.1	380.6	399.4	411.4	415.6
40.	301.8	389.6	409.6	422.6	427.3
70.	308.6	395.1	415.9	429.5	434.6
100.	312.5	397.9	419.2	433.2	438.4
150.	316.8	400.7	422.4	436.8	442.1
200.	319.3	402.4	424.4	438.9	444.4

Figure 6.3. Propellant Library (PROPLIB) (Sheet 29 of 32)

500.	323.1	404.5	426.7	441.6	447.2	451.9	453.1	414.3	330.8
400.	325.4	405.7	428.2	443.2	448.9	453.7	455.0	416.4	333.1
600.	328.6	407.3	430.0	445.2	451.0	455.9	457.4	418.9	335.9
800.	330.7	408.2	431.1	446.4	452.3	457.3	458.8	420.4	337.7
1000.	332.3	408.8	431.8	447.3	453.2	458.2	459.8	421.5	339.0
3000.	339.3	411.3	434.7	450.5	456.6	461.8	463.5	425.7	343.9

C

ODK MIXTURE RATIOS

C/MP	0.0	1.0	1.4	1.8	2.0	2.2	2.4	3.0	5.0
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EPS	CHAMBER PRESSURE =	40.0							
1.	201.5	257.9	264.0	267.2	267.1	266.0	264.4	258.2	213.4
2.	232.4	300.8	308.8	314.0	314.2	313.0	310.9	302.4	245.2
4.	251.5	325.3	334.6	341.5	342.0	340.6	338.1	327.8	262.0
10.	268.0	346.3	356.7	365.3	366.1	364.3	361.4	349.3	275.3
20.	278.5	357.0	367.9	377.4	378.4	376.4	373.3	360.0	281.6
40.	287.5	364.7	376.0	386.1	387.3	385.2	381.8	367.7	286.0
70.	293.9	369.3	380.8	391.3	392.6	390.4	387.0	372.3	288.5
100.	297.8	371.7	383.3	394.1	395.4	393.1	389.6	374.7	289.8
150.	301.8	374.0	385.7	396.6	398.0	395.7	392.1	376.9	291.0
200.	304.3	375.4	387.2	398.2	399.6	397.3	393.7	378.3	291.7
300.	306.0	377.1	388.9	400.1	401.5	399.2	395.5	379.9	292.6
400.	310.2	378.1	390.0	401.2	402.7	400.3	396.6	380.9	293.1
600.	313.4	379.4	391.3	402.6	404.1	401.7	398.0	382.1	293.7
800.	315.6	380.1	392.1	403.5	404.9	402.5	398.8	382.8	294.1
1000.	317.2	380.7	392.6	404.0	405.5	403.1	399.3	383.3	294.4
3000.	324.5	382.6	354.7	406.2	407.7	405.3	401.4	385.1	295.3

C

EPS	CHAMBER PRESSURE =	100.0							
1.	201.7	262.0	268.3	271.5	271.6	270.7	269.2	262.8	213.6
2.	232.9	306.5	315.2	320.5	321.3	320.5	318.8	309.9	245.3
4.	251.5	332.4	342.8	349.8	351.4	350.9	348.8	337.6	262.5
10.	269.5	354.6	366.7	375.3	378.1	377.6	375.1	361.3	276.4
20.	282.3	366.0	378.9	388.5	392.0	391.4	388.7	373.3	283.0
40.	289.5	374.3	387.8	398.1	402.2	401.6	398.7	382.1	287.6
70.	296.0	379.3	393.3	403.9	408.4	407.8	404.7	387.3	290.3
100.	299.8	381.9	396.1	406.9	411.7	411.0	407.9	390.0	291.7
150.	304.1	384.4	398.8	406.8	414.8	414.0	410.9	392.6	292.9
200.	306.6	385.9	400.4	411.6	416.6	415.9	412.7	394.2	293.7
300.	310.3	387.8	402.4	413.7	418.9	418.2	414.9	396.0	294.6
400.	312.6	388.9	403.6	415.0	420.3	419.5	416.2	397.2	295.2
600.	315.8	390.3	405.0	416.6	422.0	421.2	417.9	398.5	295.8
800.	318.0	391.1	405.9	417.5	423.0	422.2	418.9	399.4	296.2
1000.	319.6	391.7	406.6	418.2	423.7	422.9	419.5	400.0	296.5
3000.	327.0	393.9	408.9	420.7	426.3	425.5	422.1	402.1	297.5

C

EPS	CHAMBER PRESSURE =	300.0							
1.	202.1	265.5	272.4	276.0	276.3	275.6	274.2	267.4	213.7
2.	233.9	311.6	321.1	326.4	327.5	327.1	325.6	316.0	245.7
4.	253.2	338.6	350.3	357.3	359.3	359.6	358.0	344.9	264.0
10.	271.9	362.0	375.8	384.5	387.5	388.8	387.1	369.6	280.0
20.	283.0	374.0	389.0	398.7	402.4	404.3	402.4	382.3	288.0
40.	292.4	382.8	398.7	409.2	413.3	415.8	413.8	391.4	293.6
70.	299.0	388.2	404.7	415.6	420.1	423.0	420.8	397.0	296.9
100.	302.9	391.0	407.8	419.0	423.6	426.7	424.5	399.9	298.6
150.	307.2	393.7	410.8	422.2	427.0	430.3	428.0	402.6	300.2
200.	309.7	395.3	412.6	424.2	429.1	432.5	430.2	404.3	301.1
300.	313.5	397.3	414.8	426.6	431.6	435.1	432.8	406.3	302.3
400.	315.8	398.6	416.2	428.0	433.1	436.8	434.4	407.5	303.0
600.	319.0	400.0	417.8	429.8	435.0	438.8	436.4	409.0	303.8

Figure 6.3. Propellant Library (PROPLIB) (Sheet 30 of 32)

800.	321.2	400.9	418.9	430.9	436.1	440.0	437.6	409.8	304.3
1000.	322.8	401.6	419.5	431.6	436.9	440.8	438.4	410.5	304.6
3000.	330.1	403.9	422.2	434.5	439.9	443.9	441.5	412.8	305.8

EPS	CHAMBER PRESSURE = 500.0			ODK SPECIFIC IMPULSE					
1.	202.5	266.9	274.1	277.9	278.3	277.8	276.4	269.4	213.8
2.	234.7	313.3	323.2	328.7	329.8	329.6	328.2	318.1	246.0
4.	254.3	340.6	352.8	359.9	362.0	362.6	361.2	346.7	264.9
10.	273.2	364.2	378.7	387.7	390.8	392.4	391.2	371.1	282.1
20.	284.4	376.4	392.2	402.2	405.9	408.4	407.1	383.5	291.0
40.	293.9	385.4	402.2	413.0	417.1	420.3	418.9	392.5	297.3
70.	300.6	390.8	408.4	419.6	424.0	427.7	426.3	398.0	301.1
100.	304.4	393.7	411.8	423.1	427.7	431.6	430.2	400.8	303.0
150.	318.7	396.4	414.6	426.4	431.2	435.3	433.9	403.5	304.9
200.	311.5	398.1	416.5	428.5	433.3	437.6	436.2	405.1	306.0
300.	315.1	400.1	418.8	431.0	435.9	440.4	439.0	407.1	307.3
400.	317.4	401.4	420.2	432.5	437.5	442.1	440.7	408.3	308.1
600.	320.6	402.9	421.9	434.3	439.5	444.2	442.8	409.7	309.0
800.	322.8	403.8	423.0	435.5	440.7	445.4	444.0	410.6	309.6
1000.	324.4	404.5	423.7	436.2	441.5	446.3	444.9	411.2	310.0
3000.	331.7	406.9	426.4	439.2	444.6	449.6	448.2	413.5	311.4

EPS	CHAMBER PRESSURE = 1000.0			ODK SPECIFIC IMPULSE					
1.	203.2	268.4	276.3	280.4	281.0	280.6	279.3	271.9	213.9
2.	235.9	315.0	325.6	331.4	332.8	332.8	331.4	320.3	246.6
4.	255.9	342.4	355.4	362.9	365.1	366.0	364.8	348.3	266.0
10.	275.1	366.2	381.7	391.0	394.3	396.3	395.6	372.1	284.4
20.	286.5	378.5	395.4	405.9	409.6	412.4	412.0	384.3	294.5
40.	296.1	387.5	405.6	416.9	421.1	424.5	424.3	393.1	301.9
70.	302.8	393.1	411.8	423.7	428.2	432.0	432.0	398.5	306.4
100.	306.7	395.9	415.1	427.3	432.0	436.0	436.1	401.3	308.7
150.	311.0	398.7	418.3	430.8	435.6	439.8	440.0	403.9	310.9
200.	313.6	400.4	420.2	432.9	437.8	442.2	442.4	405.5	312.3
300.	317.3	402.4	422.5	435.5	440.5	445.0	445.4	407.4	313.9
400.	319.6	403.7	424.0	437.0	442.2	446.8	447.2	408.6	314.9
600.	322.9	405.2	425.7	439.0	444.2	448.9	449.4	410.0	316.0
800.	325.1	406.2	426.8	440.1	445.4	450.2	450.7	410.9	316.7
1000.	326.7	406.8	427.6	440.9	446.3	451.1	451.7	411.5	317.2
3000.	333.9	409.3	430.4	444.0	449.5	454.5	455.2	413.8	319.0

EPS	CHAMBER PRESSURE = 5000.0			ODK SPECIFIC IMPULSE					
1.	206.1	271.1	280.6	285.7	286.8	286.8	285.8	276.6	214.9
2.	240.0	317.4	329.7	336.7	338.6	339.3	338.2	323.7	248.7
4.	260.7	344.6	359.3	368.0	370.7	372.2	371.6	350.6	265.1
10.	280.5	368.2	385.4	396.0	399.7	402.2	402.4	373.7	288.7
20.	292.1	380.4	399.1	410.8	415.0	418.2	418.9	385.6	300.1
40.	301.8	389.4	409.2	421.9	426.5	430.2	431.3	394.5	309.4
70.	308.6	394.9	415.5	428.7	433.7	437.7	439.1	400.0	315.3
100.	312.5	397.7	418.8	432.4	437.4	441.7	443.2	402.8	318.5
150.	316.8	400.5	421.9	435.9	441.1	445.5	447.2	405.6	321.6
200.	319.3	402.2	423.9	438.0	443.4	447.9	449.6	407.2	323.5
300.	323.1	404.2	426.2	440.6	446.1	450.7	452.6	409.3	325.8
400.	325.4	405.5	427.7	442.2	447.8	452.5	454.4	410.5	327.2
600.	328.6	407.0	429.4	444.2	449.8	454.7	456.7	412.0	328.9
800.	330.7	408.6	430.5	445.4	451.1	456.0	458.1	412.9	329.9
1000.	332.3	408.6	431.2	446.2	452.0	456.9	459.0	413.5	330.7
3000.	339.3	411.1	434.1	449.4	455.3	460.4	462.6	415.9	333.4

C MR = .001 1.0 1.4 1.8 2.0 2.2 2.4 3.0 5.0
FC CHARACTERISTIC VELOCITY (FT/SEC)

Figure 6.3. Propellant Library (PROPLIB) (Sheet 31 of 32)

C

40.	5125.	6756.	6950.	6988.	6990.	6966.	6927.	6764.	5419.
100.	5310.	6819.	6980.	7075.	7082.	7063.	7025.	6854.	5420.
300.	5146.	6885.	7070.	7176.	7190.	7176.	7141.	6956.	5422.
500.	5159.	6911.	7109.	7221.	7239.	7228.	7194.	7000.	5425.
1000.	5183.	6942.	7158.	7280.	7303.	7296.	7265.	7055.	5430.
5000.	5272.	6994.	7252.	7401.	7438.	7444.	7418.	7153.	5465.

C PC COMBUSTION TEMPERATURE (DEG - R)

40.	1767.	5988.	6618.	7081.	7216.	7299.	7344.	7335.	5644.
100.	1771.	6173.	6879.	7374.	7523.	7616.	7666.	7645.	5648.
300.	1780.	6431.	7197.	7740.	7910.	8017.	8074.	8032.	5653.
500.	1787.	6536.	7344.	7915.	8095.	8210.	8271.	8215.	5657.
1000.	1805.	6670.	7542.	8153.	8351.	8477.	8543.	8462.	5666.
5000.	1895.	6930.	7973.	8701.	8946.	9107.	9188.	9013.	5726.

C COEFFICIENTS FOR COK THROAT CORRECTION CORRELATION

$$(\Delta KL / \Delta RT) = A + B * \ln(RREF/KL)$$

$$A = -1.1543 \quad B = 1.7378 \quad RTREF = 2.289$$

C

END DATA

C

C

C

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Figure 6.3. Propellant Library (PROPLIB) (Sheet 32 of 32)